



# Optimal control theory, sub-Riemannian geometry and swimming of copepod

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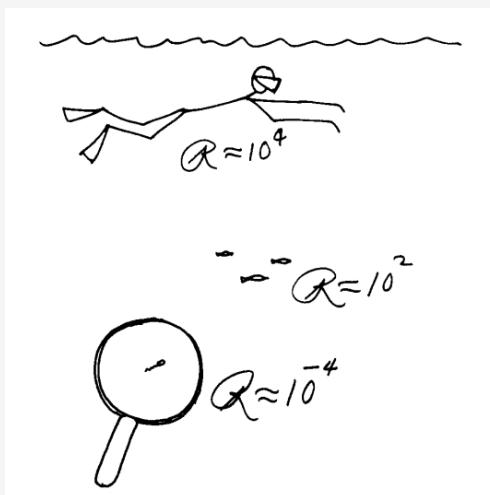
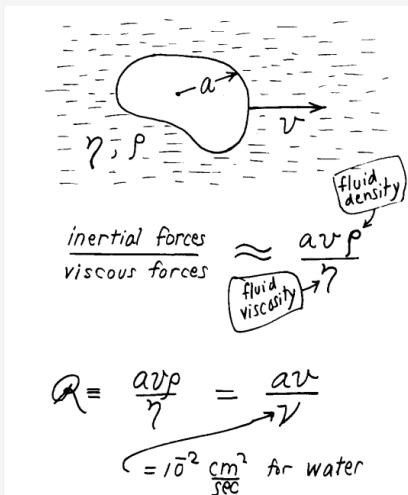
# **Optimal control theory, sub-Riemannian geometry and swimming of copepod**

Jérémie Rouot, LAAS-CNRS, Toulouse

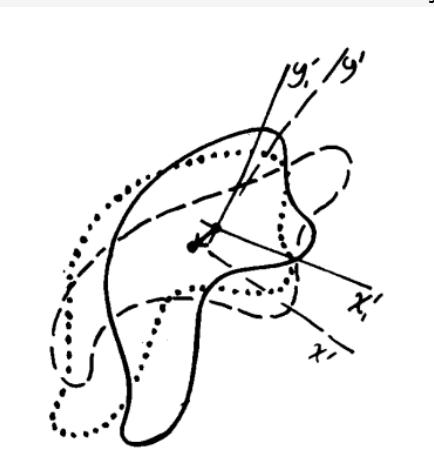
Congrès SMAI 2017  
8e Biennale Française des Mathématiques Appliquées et Industrielles

*La Tremblade*

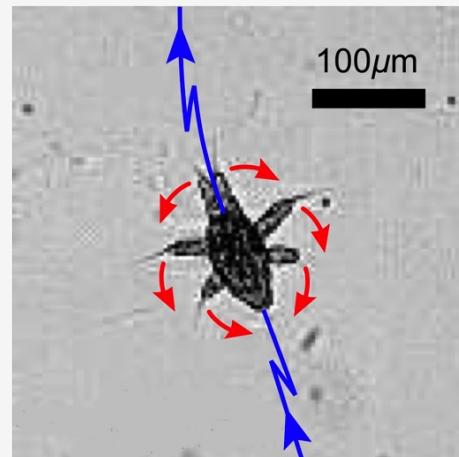
# Life at low Reynolds number - Purcell, 1977



Reynolds number

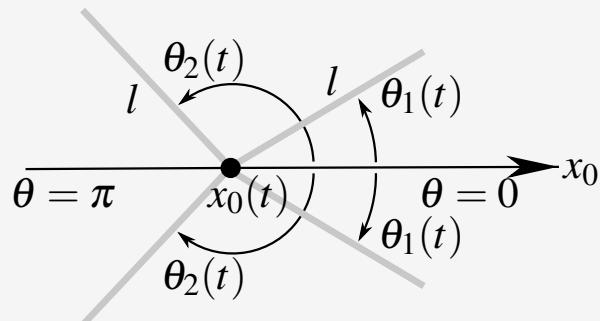


Shape deformations of a microswimmer



Zooplankton

## 2-link symmetric swimmer.



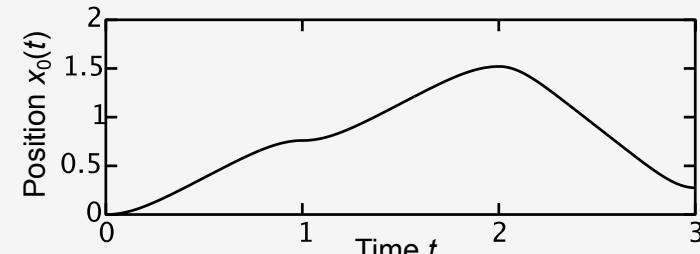
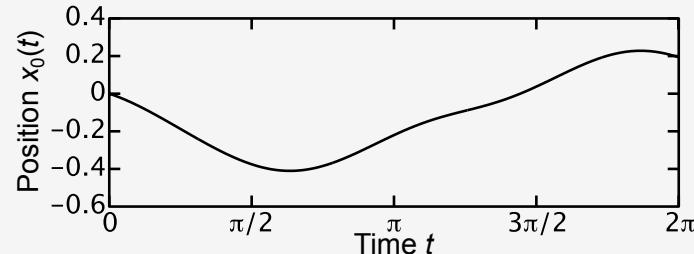
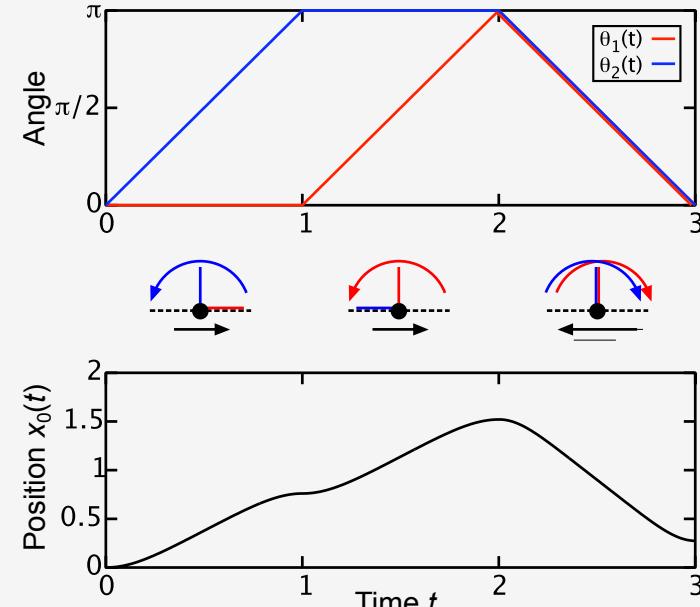
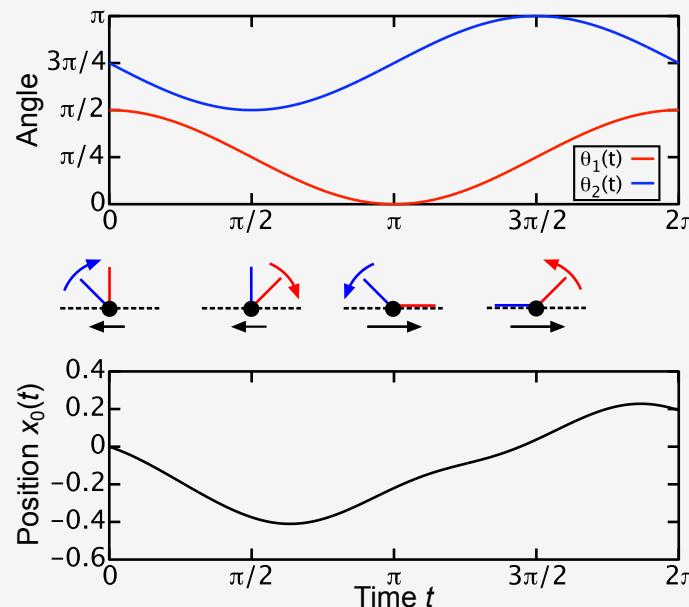
## Dynamic.

$$\dot{x}_0 = \frac{\sum_{i=1}^2 l^2 \dot{\theta}_i \sin(\theta_i)}{2 + \sum_{i=1}^2 \sin^2(\theta_i)}, \quad \dot{\theta}_i = u_i, \quad i = 1, 2 \quad (\text{state constraint : } 0 \leq \theta_1 \leq \theta_2 \leq \pi).$$

**Criterion.** min drag forces :  $\dot{q}S(q)\dot{q}^\top$ ,  $q = (\theta_1, \theta_2, x_0)$  and  $S$  is positive definite  
 $\implies$  quadratic form in  $(u_1, u_2)$ .

## Two types of geometric motions

**Definition 1.** A stroke is a periodic motion of the shape variables  $(\theta_1, \theta_2)$  associated with a **periodic control** producing a net displacement of the position variables after one period  $T$  (we can fix  $T = 2\pi$ ).



(left) Trigonometric controls. (right) Piecewise constant controls.

$$\mathcal{E}(q(\cdot)) = \textbf{Geometric Efficiency} = x_0(T)/l_{SR}(q)$$

**SR Length**  $l_{SR}$ .

$$l_{SR}(q) = \int_0^T \sqrt{L(q, u)} dt, \quad L(q, u) = a(q) u_1^2 + 2b(q) u_1 u_2 + c(q) u_2^2$$

$$\min_{u(\cdot)} l_{SR}(q) \Leftrightarrow \min_{u(\cdot)} \int_0^T L(q, u) dt$$

**Two steps.**

$$\max_{u(\cdot), x_0(T)} \mathcal{E} \Leftrightarrow \left( \begin{array}{l} \dot{q} = \sum_{i=1}^2 u_i F_i \leftarrow \min_{u(\cdot)} \int_0^T L(q, u) dt, \\ \min_{u(\cdot)} \int_0^T L(q, u) dt \quad \text{with } x_0(T) \text{ fixed, then} \quad \underbrace{\max_{x_0(T)} \mathcal{E}}_{\text{Transversality cond.}} \end{array} \right)$$

Compute points on the Sub-Riemannian sphere → provide candidate solutions for the maximum of efficiency problem.

## Pontryagin Maximum Principle

Introduce  $q^0$  be the state s.t. :  $\dot{q}^0 = L(q, u)$  and denote  $\tilde{q} = (q, q^0)$ ,  
 $c(\tilde{q}(0), \tilde{q}(T))$  is the cost function to minimize,  
 $B$  defines the boundary conditions :  $(\tilde{q}(0), \tilde{q}(T)) \in B$ .

**Necessary conditions.**  $(\tilde{q}, u)$  optimal  $\Rightarrow \exists \tilde{p} = (p, p^0) : [0, T] \rightarrow (\mathbb{R}^n \times \mathbb{R})$  abs. continuous and  $\lambda \geq 0$  cst. with  $(\tilde{p}, \lambda) \neq (0, 0)$  and s.t.

$$\dot{\tilde{q}} = \frac{\partial H}{\partial \tilde{p}}, \quad \dot{\tilde{p}} = -\frac{\partial H}{\partial \tilde{q}}, \quad \frac{\partial H}{\partial u} = 0$$

where  $H(\tilde{q}, \tilde{p}, u) = p \cdot \dot{q} + p^0 \dot{q}^0$ .

### Transversality Conditions

$$(\tilde{p}(0), -\tilde{p}(T)) - \lambda \left( \frac{\partial c}{\partial \tilde{q}(0)}(\tilde{q}(0), \tilde{q}(T)), \frac{\partial c}{\partial \tilde{q}(T)}(\tilde{q}(0), \tilde{q}(T)) \right) \in (T_{(\tilde{q}(0), \tilde{q}(T))} B)^\perp$$

**Definition 2.**  $(\tilde{q}, \tilde{p}, \lambda, u)$  is called a **normal extremal** if  $\lambda > 0$ , **abnormal** if  $\lambda = 0$ .

An abnormal trajectory  $q(\cdot)$  which is not the projection of a normal extremal is called strict.

## Pontryagin Maximum Principle : Copepod

$$\dot{q} = \sum_{i=1}^2 u_i F_i(q) \leftarrow \min_{u(\cdot)} q^0(T), \quad q = (\theta_1, \theta_2, x_0), \quad x_0(T) \text{ fixed} .$$

$$F_i = \frac{\sin(\theta_i)}{\Delta} \frac{\partial}{\partial x_0} + \frac{\partial}{\partial \theta_i}, \quad \Delta = 2 + \sin^2(\theta_1) + \sin^2(\theta_2)$$

**PMP :**

$$H(z, u) = u_1 H_1(z) + u_2 H_2(z) + p^0 L(q, u), \quad z = (q, p)$$

with  $H_i = p \cdot F_i$ ,  $i = 1, 2$ .

— normal case :  $p^0 = -1/2$

$$H_n = 1/2 (a(q) H_1^2 + 2b(q) H_1 H_2 + c(q) H_2^2)$$

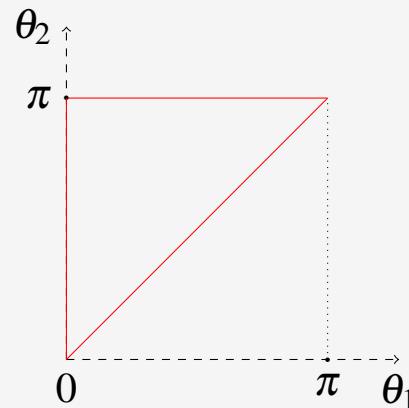
— abnormal case :  $p^0 = 0$  hence  $H_1 = H_2 = \{H_1, H_2\} = 0$ , then

$$u_1 \{\{H_1, H_2\}, H_1\} + u_2 \{\{H_1, H_2\}, H_2\} = 0.$$

**Proposition 3.** *The surface  $\Sigma : \{ q; \det(F_1(q), F_2(q), [F_1, F_2](q)) = 0 \}$  contained abnormal trajectories and is defined by*

- $\theta_i = 0$  or  $\pi$ , for  $i = 1, 2$ ,
- $\theta_1 = \theta_2$ .

*It is formed by the boundaries of the physical domain :  $\theta_i \in [0, \pi]$ ,  $i = 1, 2$ ,  $\theta_1 \leq \theta_2$ .*



: abnormal trajectories  
in the plane  $(\theta_1, \theta_2)$

## Boundary conditions

$$x_0(0) = 0, \quad x_0(T) = x_f, \quad \theta_i(0) = \theta_i(T), \quad i = 1, 2$$

## Transversality conditions

$$p_{\theta_i}(0) = p_{\theta_i}(T), \quad i = 1, 2$$

## Boundary value problem

$$\begin{cases} \dot{z} = \vec{H}_n(z) \\ x_0(0) = 0, \quad x_0(T) = x_f \text{ (fixed)}, \\ \theta_i(0) = \theta_i(T), \quad i = 1, 2 \\ p_{\theta_i}(0) = p_{\theta_i}(T), \quad i = 1, 2 \end{cases}$$

- HamPath, *indirect method* : based on Maximum Principle, Newton type algorithm (sensitive to initialization) and computation of **second order necessary optimality conditions** .
- Bocop, *direct method* : gives an initialization for the shooting algorithm of Ham-Path.

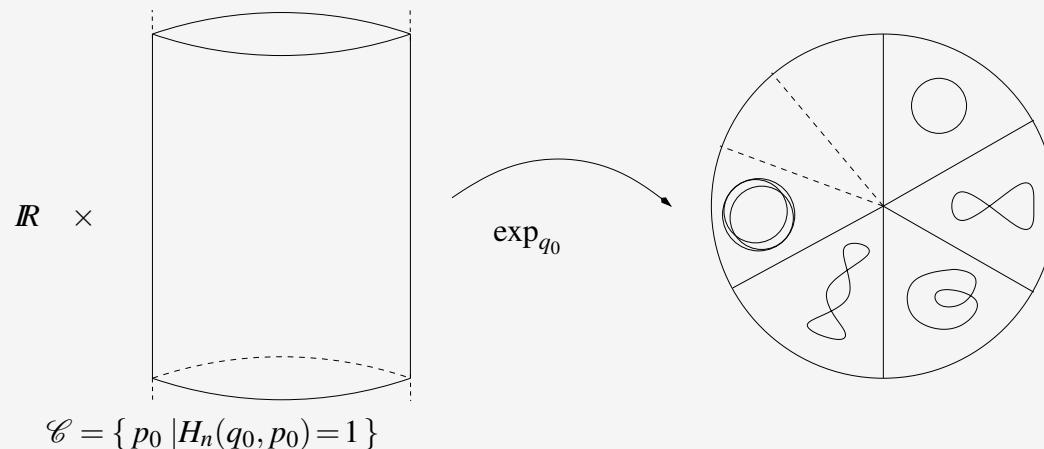
## Exponential mapping

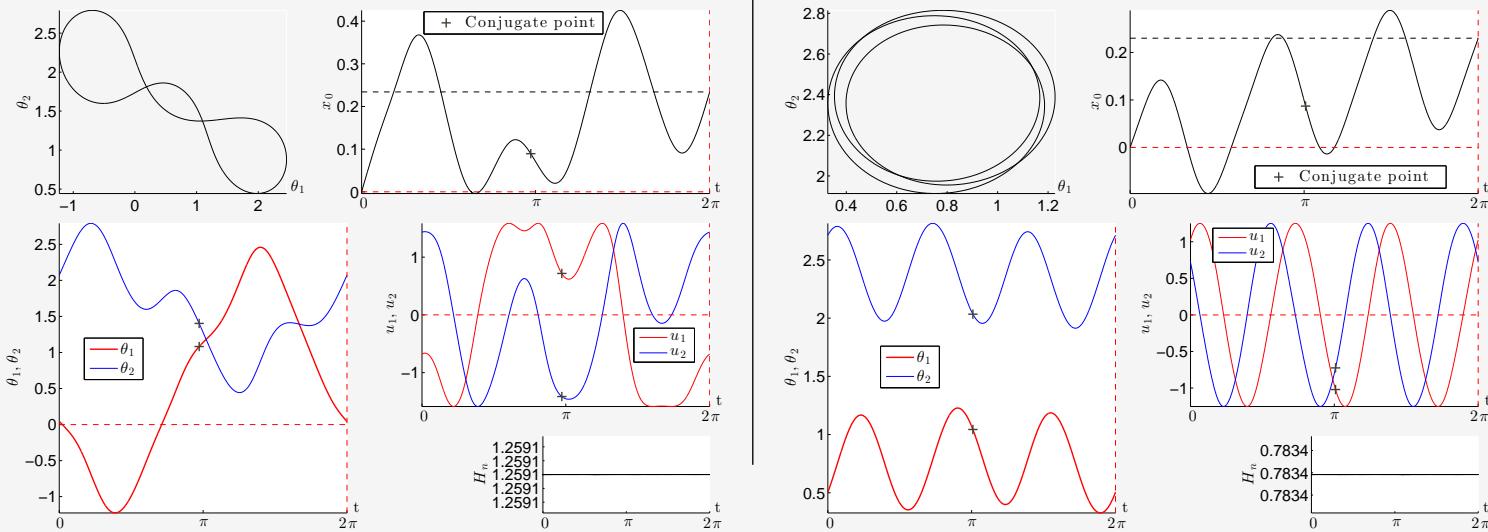
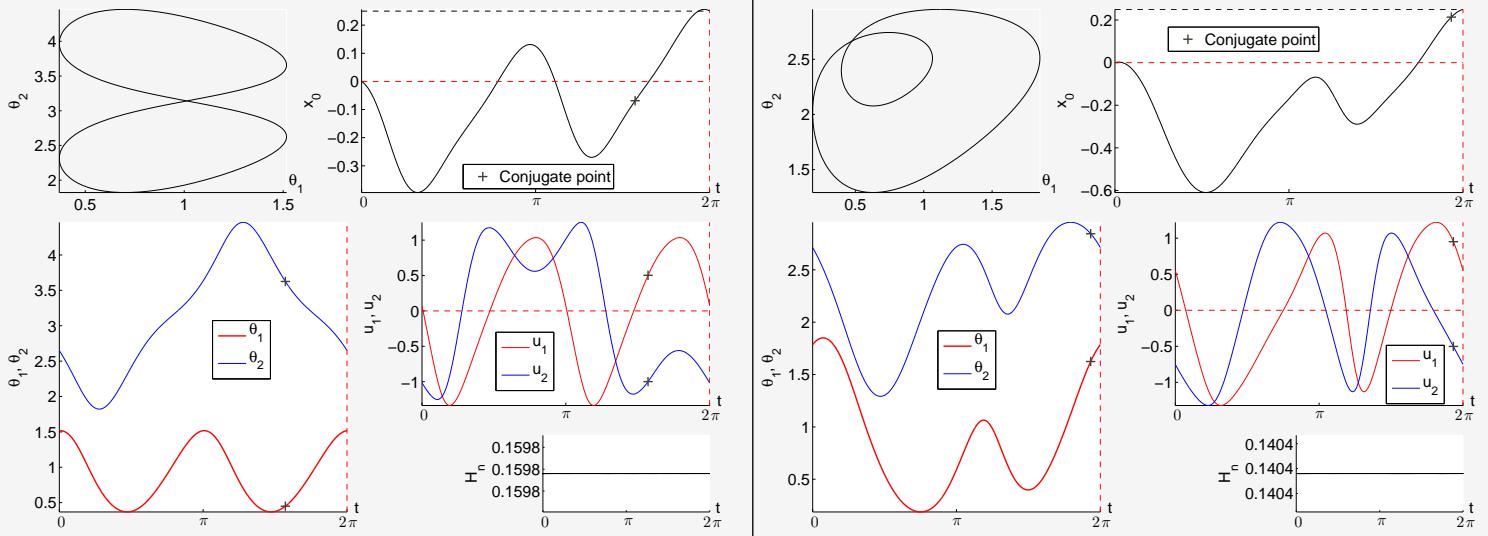
**First conjugate time  $t_c$**  : The first time  $t_c$  when the exponential mapping

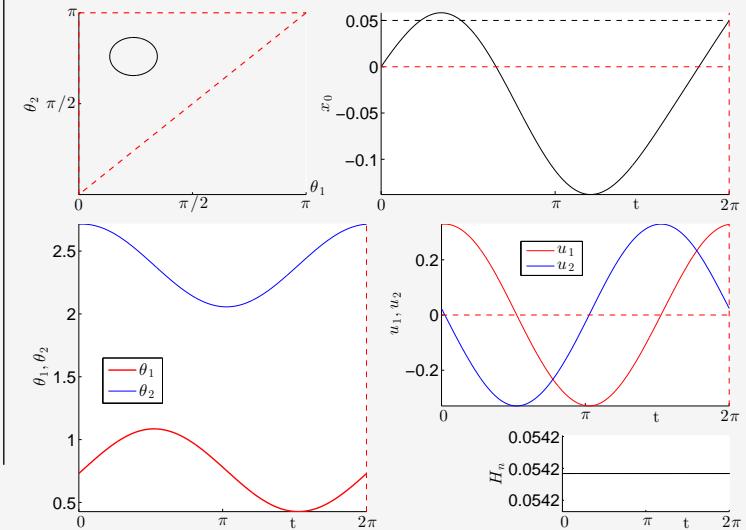
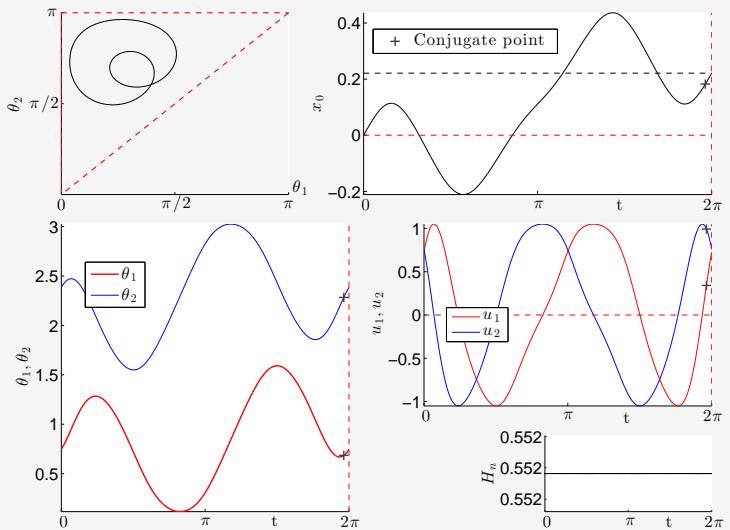
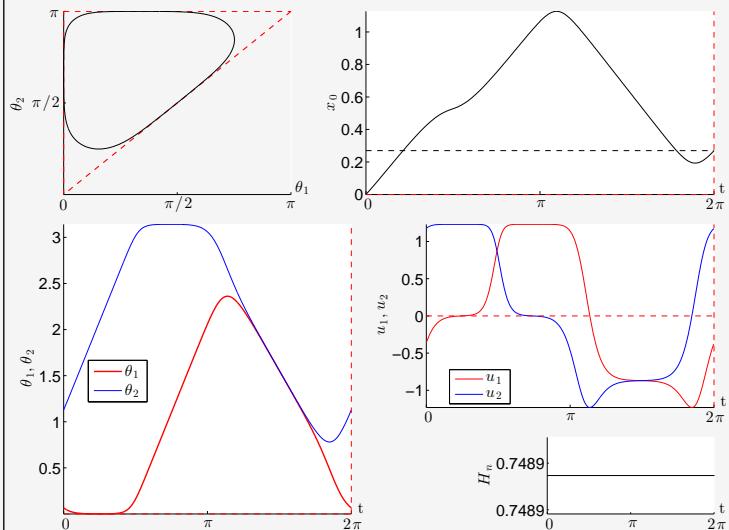
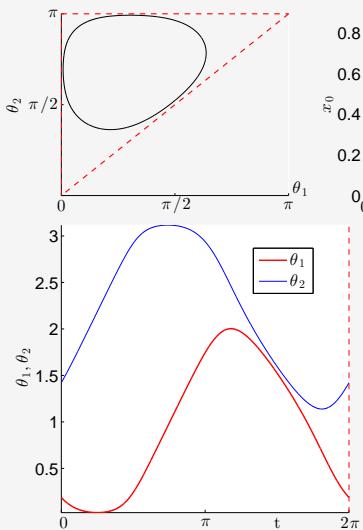
$$\exp_{q_0} : \mathbb{R} \times \mathcal{C} \rightarrow M, \quad (t, p_0) \mapsto q(t, q_0, p_0)$$

is not an immersion at  $(t_c, p_0)$ .

**Theorem 4.** Let  $q : [0, T] \longrightarrow \mathbb{R}^n$  be a strict normal stroke. If  $q(\cdot)$  has at least one conjugate point on  $]0, T[$ , then  $q(\cdot)$  is not a local minimizer for the  $L^\infty$  topology on the controls considering the optimal control problem with fixed extremities.



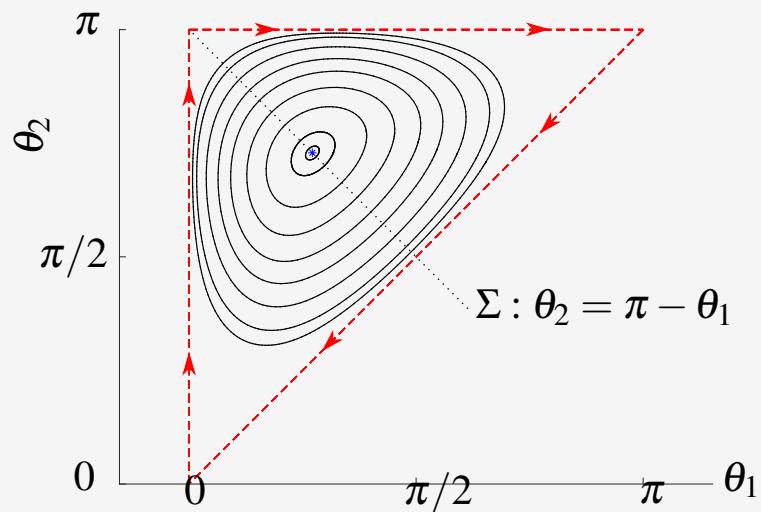




### Numerical fact :

Only the simple loops don't have conjugate points on  $]0, T[$ . They are the only candidates for optimality.

**Theorem 5.** *There is a one parameter family of simple loop strokes parameterized by the displacement  $x_0(T)$  or the energy level  $H_n(q_0, p_0)$ .*



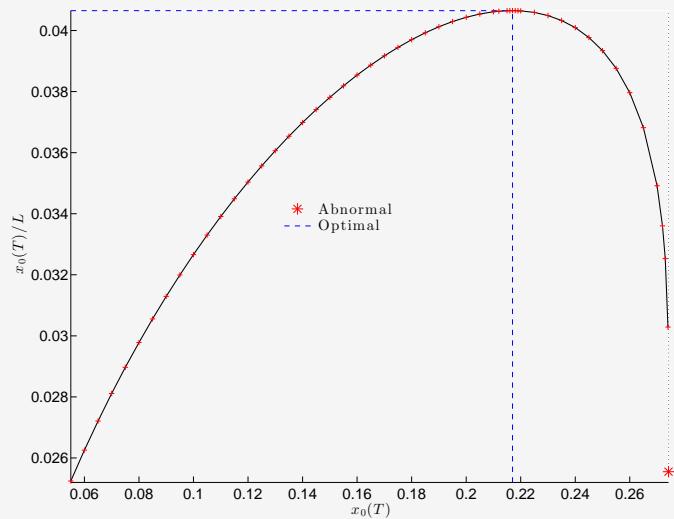
One parameter family of geodesic strokes.

Select on the point on the SR sphere with maximum of efficiency

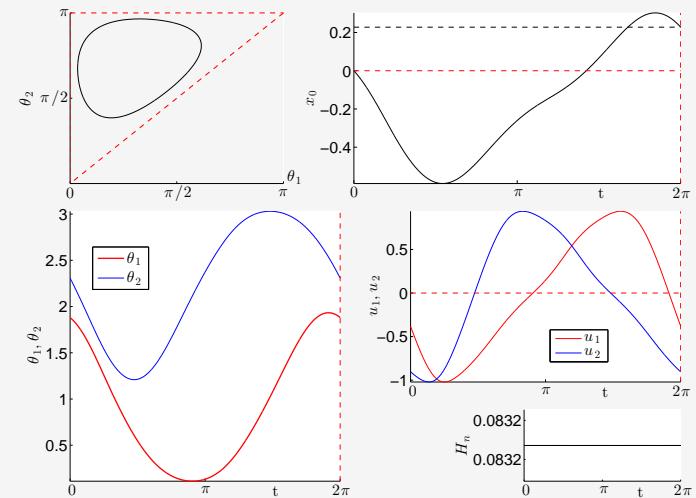
Geometric efficiency :  $\mathcal{E} = x_0(T)/l_{SR}(q)$ ,  $(x_0(T) \text{ free})$

### Transversality conditions

$$p_{x_0}(T) = q^0(T)/x_0(T), \quad p^0(T) = -1/2$$



Efficiency curve with continuation on  $x_0(T)$ .



Optimal normal stroke

**Theorem 6.** *The abnormal stroke is not minimizing for both costs (length with fixed displacement and efficiency).*

**SR problem**  $(D, g)$  where  $D = \text{span}\{F, G\}$  is a 2-dimensional distribution in  $\mathbb{R}^3$  and  $g$  is a SR metric.

**Normal form of order  $-1$**  Nilpotent model of order  $-1$ , the Brockett model :

$$\hat{F} = \frac{\partial}{\partial x} + y \frac{\partial}{\partial z}, \quad \hat{G} = \frac{\partial}{\partial y} - x \frac{\partial}{\partial z}$$

where (weight of  $x, y) = 1$  and (weight of  $z) = 2$  (privileged coordinates).

**Application to the Copepod**  $(x, y, z)$  are related to the physical coordinates  $(\theta_1, \theta_2, x_0)$  by change of coordinates  $(x = \theta_1, y = \theta_2)$ .

$\Rightarrow$  this model is **not generic** and  $z$  (always increasing) cannot be identified with the displacement  $x_0$ .

## Normal form of order 1

**Theorem 7** (Chakir, Gauthier, Kupka, 1996). *The generic model is given by the normal form of order 1*

$$F = \hat{F} + yQ(x,y)\frac{\partial}{\partial z}, \quad G = \hat{G} - xQ(x,y)\frac{\partial}{\partial z},$$

$Q$  quadratic in  $(x,y)$ .

**Application to the Copepod** At a contact point  $(\beta, \pi - \beta)$ ,  $\beta \in ]0, \pi/2[$ , truncating the Taylor expansion of  $F_1, F_2$ , we consider :

$$\begin{aligned} \hat{F}_1(x,y,z) &= \frac{\partial}{\partial x} + (a_{30}(\beta)x^3 + a_{21}(\beta)x^2y + a_{12}(\beta)xy^2 + a_{03}(\beta)y^3 + a_{20}(\beta)x^2 \\ &\quad + a_{11}(\beta)xy + a_{02}(\beta)y^2 + a_{10}(\beta)x + a_{01}(\beta)y + a_{00}(\beta))\frac{\partial}{\partial z} \\ \hat{F}_2(x,y,z) &= \frac{\partial}{\partial y} + (-a_{30}(\beta)y^3 - a_{21}(\beta)xy^2 - a_{12}(\beta)x^2y - a_{03}(\beta)x^3 + a_{20}(\beta)y^2 \\ &\quad + a_{11}(\beta)xy + a_{02}(\beta)x^2 - a_{10}(\beta)y - a_{01}(\beta)x + a_{00}(\beta))\frac{\partial}{\partial z}. \end{aligned}$$

**Gauge group**  $\mathcal{D}$  : set of formal diffeomorphisms preserving the origin,

$\mathcal{F}$  : set of formal power series in  $x, y, z$ .

- action of  $\varphi \in \mathcal{D}$ ,  $\varphi.(A, B) = (\varphi_*(A), \varphi_*(B))$ ,
- action of  $\alpha \in \mathcal{F}$ ,  $\alpha.(A, B) = (A \cos \alpha + B \sin \alpha, -A \sin \alpha + B \cos \alpha)$ .

Under the action of the gauge group,  $(\hat{F}_1, \hat{F}_2)$  can be put under the form given in Theorem 8 with

$$Q(x, y) = 1/8 \frac{(-11 \cos^6 \beta + 17 \cos^4 \beta - 8 \cos^2 \beta + 4) x^2}{(\cos^6 \beta - 5 \cos^4 \beta + 8 \cos^2 \beta - 4) \cos^2 \beta} \\ + 1/8 \frac{(5 \cos^8 \beta - 33 \cos^6 \beta + 2 \cos^4 \beta + 28 \cos^2 \beta - 8) y^2}{(\cos^6 \beta - 5 \cos^4 \beta + 8 \cos^2 \beta - 4) \cos^2 \beta}.$$

## Periodicity equations

$$\theta_i(0) = \theta_i(T), \quad \dot{\theta}_i(0) = \dot{\theta}_i(T), i = 1, 2.$$

## Admissible transformations

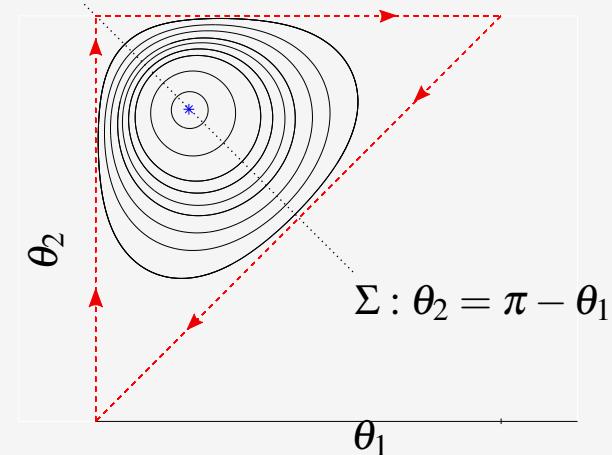
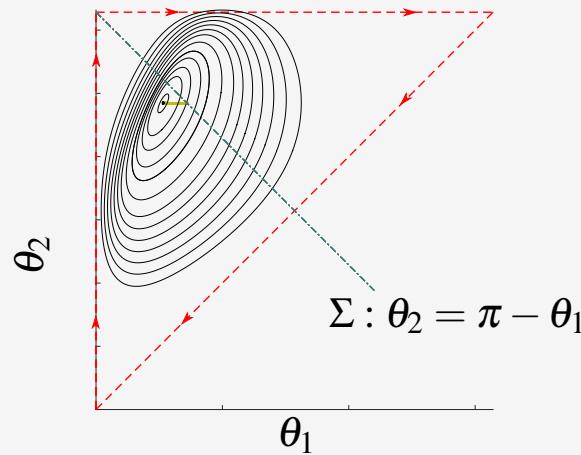
$$\mathcal{G} = \{\varphi \in \mathcal{D} \mid \varphi(\theta, x_0) = (\varphi_1(\theta), \varphi_2(\theta), \varphi_3(\theta, x_0))\}.$$

## Transformation mixing up shape variables (x,y) and the displacement z

$$\varphi(x, y, z) = (x + c_{011}(\beta)y z + c_{001}(\beta)z, y - c_{011}(\beta)x z + c_{001}(\beta)z, z + P(x, y, z, \beta)),$$

$$\Rightarrow c_{011}(\beta) = c_{001}(\beta) = 0.$$

**Theorem 8.** *The only stroke that can be computed with transformations of  $\mathcal{G}$  is reduced to the **center of the family** of simple loop strokes (obtained by the true system).*



One parameter family of simple loops corresponding to different metrics for the true system.

The center of family = SR invariant : related to the inverse optimal control problem.