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# AC Losses and Material Degradation Effects in a Superconducting Tape for SMES Applications

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**Abstract.** Superconducting Magnetic Energy Storage (SMES) systems are one potential application of superconductivity in electric grids. The main element of such systems is a coil, made from superconducting tape. Although SMES systems work in DC conditions, due to highly dynamic working regimes required for some applications, AC currents can appear in the coil. It is then of utmost importance to verify the magnitude of these AC currents and take into account AC losses generated on the tape in the design phase of such system. To assure a proper operation, it is also necessary to know tape characteristics during the device lifetime, which in normal operation conditions can be of decades. Continuous thermal cycles and mechanical stresses to which the tape is subjected can change its characteristics, changing important quantities like critical current ( $I_C$ ) and  $n$ -value. It is then also necessary to evaluate tape degradation due to these conditions. A study of AC losses will be here presented, for a short sample of BSCCO tape.  $I_C$  and  $n$ -value degradation due to consecutive thermal cycles will also be studied.

**Keywords:** Superconducting Magnetic Energy Storage, SMES, AC losses, HTS tape degradation.

## 1 Introduction

SMES systems are superconducting devices with several possible applications in electric grids and can contribute to the implementation of future's Smart Grids [1]. With such device it is possible to overcome several power quality issues, as voltage dips and swells, frequency oscillations or harmonic distortion [2]. This is possible because SMES systems store energy in a superconducting coil and can exchange active and reactive power, independently, with the electric grid where the system is

placed. The main component of the system is a coil, made from high temperature superconducting (HTS) tape. This particular work will be focused in first generation (1G) tape, built by BiSrCaCuO on its phase 2223 (BSCCO/Ag tape).

Although the coil operates in DC conditions, highly dynamic regimes to which it is subjected can lead to the appearance of an AC current. This means that in the project phase of an SMES system, it is necessary to take into account phenomena that usually occurs in AC conditions, like AC losses [3]. In fact, AC losses are one of the limiting factors for large-scale applications of superconductivity in power systems. For several years, AC losses have been an important object of study in superconductivity in both, single tape samples and coils. As a very small example one can see references [4–6]. The study of AC losses in BSCCO/Ag tapes in self-field conditions is then of utmost importance for applications that use this superconducting material, and must be addressed in the first steps of any project. This study is extremely important because in the design phase of an SMES cooling system, one has to consider the necessary power to extract from the system heat generated by those losses. Considering that there are several possible applications of superconductivity (and of SMES systems in particular), it is also necessary to verify the frequency dependence of such losses, in order to achieve an accurate value for total AC losses in the system [7].

Bearing in mind an envisaged application for SMES systems where a highly dynamic regime can introduce AC currents in the coil with frequencies up to few hundreds Hz, in this work, a study with a frequency range from 72 Hz to 576 Hz will be presented.

It is common to model high temperature superconductors using the power law [8]:

$$E = E_c \left( \frac{J}{J_c} \right)^n \quad (1)$$

Where  $E$  is electric field in the superconductor,  $E_c$  is the value of electric field in which the critical current density  $J_c$  is achieved (a usual criterion of  $E_c = 1 \mu V / cm$  is used to define critical current). Parameter  $n$  is a material property and defines the shape of the E-J curve.

Operating conditions of superconducting devices in power systems subject HTS tape to various kinds of stress or strain. These can change tape characteristics, which will change important quantities like its critical current ( $I_c$ ) or  $n$ -value. When subjected to bending and mechanical tension, the  $I_c$  value of a HTS tape will be degraded [9]. This fact should be taken into account in the design stage of the superconducting device, to assure a safe operation. To reduce mechanical vibrations in superconducting coils, it is common to impregnate HTS tape with epoxy. However, this impregnation may result in a higher tape heating, which can also decrease  $I_c$  [10].

In an SMES lifetime, the system can have many thermal cycles (cooling down and warming up the superconducting coil). These thermal cycles can also degrade the HTS tape, again leading to a lower  $I_c$  value [11] and possibly a different  $n$ -value. This effect will also be verified in this work.

## 2 Relationship to Collective Awareness Systems

Existing power grids are mainly unidirectional. However, in the electric grids of the future, energy is foreseen to flow up- and downstream. This “Smart Grid” concept involves both energy and information flows on the network [12]. This paradigm change transforms the power grid in a new grid, much more similar to information networks as internet. In the last years the concept of Internet of Things (IoT) in which every device is connected to the Web, is arising. Smart Grids represent a particular case of IoT, where reliability and security of supply are requirements of utmost importance, considering energy transmission and distribution. In this sense, power grids can become a Collective Awareness System, with distributed control and learning capabilities. Devices like SMES are foreseen to help the implementation of Smart Grids, thus being also part of these Collective Awareness Systems.

## 3 AC Losses in Superconducting Tapes

To verify the effects of AC losses in an SMES system it is first necessary to understand the origin of those losses and to classify them.

### 3.1 AC Losses Classification

Based on the physical mechanism that origins them and their frequency dependence, AC losses (power losses) in BSCCO/Ag tapes (and in HTS tapes in general) can be sorted into three different types [13]:

- *Superconducting hysteresis losses* ( $P_h$ ): linearly proportional to frequency, these appear due to variations in the superconductor magnetic state [14].
- *Eddy currents losses* ( $P_{ed}$ ): due to the existence of silver in the BSCCO/Ag tape, there are Eddy currents through that metal, which also generates losses. These are quadratically proportional to frequency and, as demonstrated by Ishii et al. [15], can be expressed as:

$$P_{ed} = \frac{2\pi^2 \mu_0^2 f^2 I_p^2 d^3}{\rho l} \text{ (W/m)} \quad (2)$$

where  $\mu_0$  is vacuum permeability,  $f$  is frequency,  $I_p$  is current amplitude through the tape,  $d$  is sheath thickness (for this tape: 36  $\mu\text{m}$ ),  $\rho$  is resistivity of silver (here set as  $3 \times 10^{-9} \Omega \cdot \text{m}$ ) and  $l$  is perimeter of the outer superconducting filament layer (in this case: 6.5 mm).

- *Resistive losses* ( $P_r$ ): at high applied-to-critical current ratios ( $i$ ), resistive losses appear in the superconductor. These are frequency independent and their value depends on the characteristics of the tape (mainly  $n$ -value). Usually they are negligible till  $i > 0.8$  [13].

Total AC losses in the superconducting tape are then the sum of those three components. By dividing the power loss per meter ( $P$ ) by frequency, one can achieve the energy loss per meter, per cycle ( $Q$ ) as follows.

$$Q_t = \frac{P_t}{f} = \frac{P_h}{f} + \frac{P_{ed}}{f} + \frac{P_r}{f} = Q_h + Q_{ed} + Q_r \quad (\text{J/m}) \quad (3)$$

At frequencies below 200 Hz hysteresis energy losses ( $Q_h$ ) are expected to have a main contribution. These are frequency independent. Eddy currents losses contribution for frequencies below this value are usually negligible, but they start to have a higher contribution to total losses with increasing frequencies. Resistive losses, as already stated, are frequency independent and depend on the used applied-to-critical current ratio. Their contribution to total losses is only visible for applied currents close to the tape  $I_C$ .

In this work, AC losses of a short sample of BSCCO/Ag tape, in which flows an AC current with frequencies ranging from 72 to 576 Hz, will be measured. The frequency dependence of these losses will be evaluated, especially concerning Eddy current losses, which are those most dependent of frequency.

To evaluate effects of thermal cycles in  $I_C$  and  $n$ -value, thus on operating conditions of the tape, after a first measurement of  $I_C$ , the sample is subjected to several of those cycles and critical current is measured again to obtain a comparison which can be very useful in real systems applications. By fitting all measured data to E-J power law (1) it will be possible to see if the  $n$ -value of the tape is also degraded.

#### 4 Experimental Measurements of AC Losses

To evaluate tape degradation, the  $I_C$  of an HTS tape sample was measured prior and after several dozens of thermal cycles. AC losses were measured and compared to the well-known Norris ellipse model [14]. To evaluate frequency dependence, both total measured losses and calculated losses by taking out Eddy current component will be presented. It is expected that, after taking out the component related to Eddy currents, AC losses show no frequency dependence. InnoST insulated tape was used and its characteristics are shown in table 1.

**Table 1.** Characteristics of the SC tape, according to supplier.

| Characteristic                                     | Value |
|--|-------|
| Critical current @ 77 K, self-field (A)            | 85    |
| Critical current density (SC) (A/mm <sup>2</sup> ) | 8500  |
| Minimum bending radius (mm)                        | 30    |
| Width (mm)   | 4.2   |
| Thickness (mm)                                     | 0.25  |

#### 4.1 Experimental Setup

To measure  $I_C$  (DC critical current) and AC losses, a four-point configuration was used. Figure 1 depicts the used sample with voltage taps 4 cm apart. AC losses were measured using an electrical method with a lock-in amplifier as main measuring device and a Rogowski coil. All measurements were made at liquid nitrogen (LN) temperature (77 K).

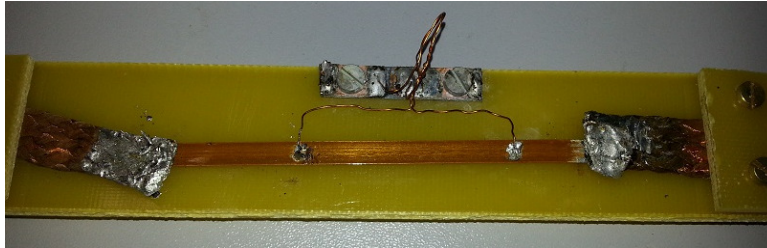


Fig. 1. HTS tape sample for measurements of critical current and AC losses.

#### 4.2 Measurements of Critical Current

DC critical current was measured for three different tape conditions:

- Unused sample (*case A*);
- After 25 thermal cycles (*case B*);
- After a total of 50 thermal cycles (*case C*).

For every thermal cycle the tape was cooled down by putting the tape directly into LN and then warmed up to room temperature (warm up by natural heating, just by taking the sample out of LN). All results are shown in figure 2.

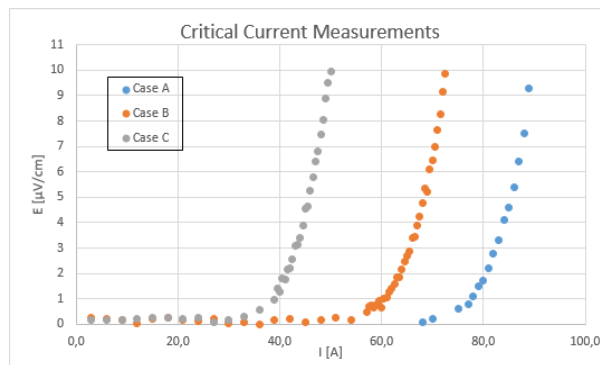


Fig. 2. Critical current measurements.

To evaluate critical current and  $n$ -value degradation, experimental results obtained for the three previous cases were used to achieve fitting E-J curves, by using Matlab<sup>®</sup> cftool. Results are shown in table 2.

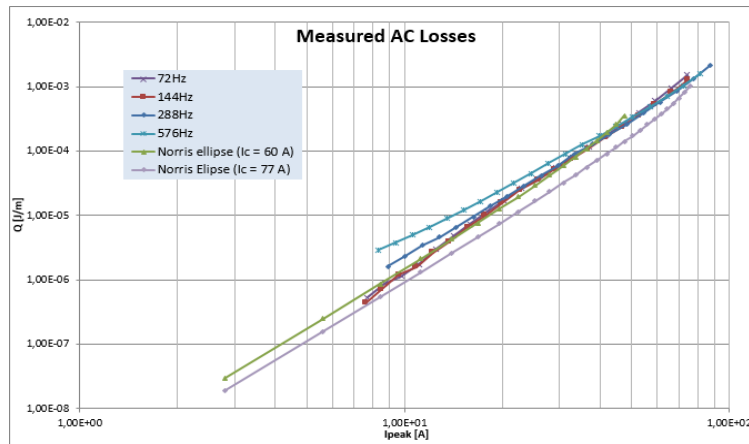
**Table 2.**  $I_c$  and  $n$ -value degradation due to thermal cycles.

| Number of cycles | Critical current [A] | $n$ -value |
|------------------|----------------------|------------|
| 0                | 77.02                | 15.35      |
| 25               | 59.6                 | 11.73      |
| 50               | 37.9                 | 8.44       |

As can be seen from results contained in table 2, the number of thermal cycles to which a superconducting tape is exposed degrade important characteristics like its critical current and  $n$ -value.

### 4.3 Measurements of AC Losses

AC losses were measured for four different values of frequency: 72 Hz, 144 Hz, 288 Hz, and 576 Hz. Figure 3 contains results for measurements made with the tape in situation B (after 25 thermal cycles). In this figure, Norris ellipse model is also shown for two values of critical current: 77 A and 60 A.

**Fig. 3** Measured (total) AC losses

Results contained in figure 3 suggest that values tend to approach Norris ellipse model (for  $I_c = 60$  A), for lower frequencies (72 Hz and 144 Hz) and for current values close to the critical current (for all frequencies). For small current amplitudes and when the current flowing through the tape has higher frequencies (288 Hz and 576 Hz) AC losses seem to be frequency dependent, increasing with frequency. Eddy current losses should be responsible for this behavior. However, when the current increases resistive losses start to appear in the tape, making Eddy current losses negligible to the total losses value. So for currents whose peak is close to the critical current of the tape, there is no frequency dependence because resistive losses, which

became the most important component in total losses (together with hysteresis losses) are frequency independent. As can be seen by the two Norris ellipse models depicted in the figure, for the same value of applied current, losses are higher if the tape has less critical current. This is an obvious result, since it means that for the same operating current, the tape is closer to its critical current if this value is lower. This also shows that AC losses in tapes with degraded critical current can still be modeled using Norris ellipse model, if the model is calculated considering the new value of critical current of that tape.

To verify if the frequency dependent behavior for small current amplitudes is due to Eddy current losses, this component was calculated using expressions (2), (3) and subtracted from the total value of losses. The results obtained are shown in figure 4.

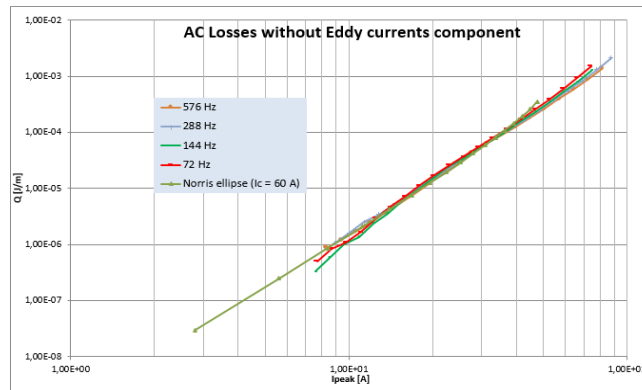


Fig. 4 AC losses after subtracting Eddy current losses component.

As can be seen in figure 4, AC losses show a non-frequency dependent behavior, if Eddy current losses are not considered. Norris ellipse model for a critical current of 60 A is also shown in this figure, for easier comparison with the previous one.

## 5 Conclusions

Critical current and  $n$ -value degradation due to thermal cycles in an HTS BSCCO/Ag tape was studied. As shown by experimental results obtained, these important quantities in a superconducting tape are effectively degraded if the tape is subjected to a certain number of thermal cycles. In fact, by subjecting the tape to a total of 50 cycles, there is a reduction of 50% of critical current value and the  $n$ -value changes from 15.35 to 8.44. This phenomena is of extreme importance for superconducting devices like SMES, where operating current is calculated based on critical current of the tape. This means that during the lifetime of the device, due to tape degradation, the required power to extract heat losses is expected to increase (for the same operating current) and this aspect cannot be neglected in the design phase of an SMES project.



AC losses of a short sample of degraded BSCCO/Ag tape, in which there are currents flowing in a band of frequencies ranging from 72 Hz to 576 Hz were also measured. Results indicate that AC losses in HTS degraded tapes can still be modeled using Norris ellipse model, if the critical current of the model is set to the effective critical current of the tape after degradation. AC losses seem to behave as frequency independent for the measured frequencies, if Eddy current losses are subtracted from the total value. As expected, Eddy current losses are frequency dependent and can be neglected for frequencies below 200 Hz.

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