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A Global Illumination Solution for General Reflectance Distributions

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Abstract

A general light transfer simulation algorithm for environments composed of materials with arbitrary reflectance functions is presented. This algorithm removes the previous practical restriction to ideal specular and/or ideal diffuse environments, and supports complex physically based reflectance distributions. This is accomplished by extending previous two-pass ray-casting radiosity approaches to handle non-uniform intensity distributions, and resolving all possible energy transfers between sample points. An implementation is described based on a spherical harmonic decomposition for encoding both bidirectional reflectance distribution functions for materials, and directional intensity distributions for illuminated surfaces. The method compares favorably with experimental measurements.


Additional Keywords and Phrases: global illumination, BRDF, specular reflection, directional-diffuse, progressive radiosity, spherical harmonics.

1 Introduction

The simulation of global illumination is one of the major requirements for realistic image synthesis. Global illumination effects produced by multiple surface reflections are significant in all but the simplest environments. For instance, indirect lighting and color bleeding, or the transfer of color by reflection, can be observed in almost all indoor scenes. This paper presents a completely general algorithm designed to solve the global illumination problem for arbitrarily complex reflectance models.

Solution techniques for the simulation of complex light transfer mechanisms, where every point in the environment can potentially act as an illuminator for all other points, have thus far been quite limited. Two major paths have been explored. Light can be followed as it leaves the light sources and is propagated and reflected throughout the environment. For example, this approach is used by progressive refinement radiosity algorithms, and can be characterized as view-independent shading [3]. Conversely, standard ray tracing [20] and its derivatives usually start from the eye and follow light paths in the reverse direction. It is therefore strongly view-dependent.

These approaches work well for certain types of reflective behaviors, such as ideal diffuse (radiosity), ideal specular (ray tracing), or combinations of these [18, 17, 9]. The actual reflectance distributions of most surfaces are far more complicated, exhibiting some directionality which must be taken into account for accurate simulation.

The approach presented here extends the progressive radiosity method to include arbitrary reflectance distributions. While previous algorithms incorporating general reflectances have relied upon a discrete set of directions [11, 1, 13], no such restriction is introduced here. This is accomplished by using continuous functions to encode the directional dependence of intensity distributions.

In the next section we discuss the applicability of view-independent and view-dependent approaches to the case of general reflectance distributions and introduce a classification of reflectance types into ideal diffuse, ideal specular and directional diffuse components. The third section is devoted to the presentation of a complete algorithm to solve the general problem. Two specific issues are then detailed: treatment of ideal specular reflection in Section 4, and storage of directional diffuse contributions in Section 5.

2 Algorithmic choices for a general solution

The goal of this research is to develop a method for the simulation of global illumination that is general enough to provide accurate solutions for scenes incorporating any reflectance distribution. The problems encountered in devising a completely general algorithm are reviewed below, together with some of their design implications.

2.1 General reflectance distributions

The reflective properties of a surface are generally described by means of a bidirectional reflectance distribution function (BRDF), which is defined as the ratio of the reflected radiance in a given outgoing direction to the incoming energy flux (per unit area) in another direction. A similar quantity is defined for transmission. For the sake of clarity, we will refer only to reflection in this paper, although the algorithm is equally applicable to transmission. The two well-understood limiting cases are ideal diffuse and ideal specular reflection.

- An ideal diffuse reflector has a constant BRDF, that is, the scattered intensity is the same in all directions. Diffuse reflection can thus be fully described by a single scalar value.
• An ideal specular reflector has a Dirac delta function as its BRDF, where the only direction in which there is non-zero scattering is the mirrored direction. The relevant quantity to describe specular reflection is the ratio of the outgoing intensity in the specular direction to the incoming intensity, or specular reflectance.

Most materials have BRDFs that are not this simple, exhibiting a more elaborate directionality. Recent work on light reflection models has shown that different physical processes contribute to different parts of a BRDF [8], and the term directional diffuse has been introduced to describe the general BRDF excluding its ideal specular component. (Figure 1).

Figure 1: Different components of a general BRDF.

The directional diffuse component of a BRDF is a function of many variables, including surface finish (roughness), wavelength, and the electrical properties of the material. This produces a great variety of behaviors, all of which must be correctly simulated. The algorithm presented below is capable of incorporating both arbitrary directional diffuse and ideal specular reflection into a global solution.

The method presented below combines elements of both strategies into a two-pass algorithm. The first pass computes a view-independent solution for the directional diffuse distribution of light, including the effect of intermediate specular reflections, and the second pass supplies the view-dependent ideal specular effects. This partitioning of reflectance behaviors resembles earlier two-pass approaches, but now accounts for all possible transport chains and incorporates arbitrary reflectance distributions, not only the extreme cases of ideal diffuse and ideal specular.

In the following discussion we use the vocabulary of radiosity-style algorithms for two reasons. One reason is the energy consistency of the radiosity method: a physical consideration necessary to obtain accurate simulations. The second reason is the appeal of the progressive refinement paradigm [3], where useful intermediate results can be obtained early in the computation.

The notion of radiosity is extended to include the directional diffuse part of the light reflected at a given point. Because it does not include specularly reflected light, this intensity distribution is fairly smooth and thus can be stored at reasonable cost (See section 5). The ideal specular distribution of light is sharply discontinuous and is too costly to store on the surfaces; it is properly computed "on the fly" to resolve specular to directional diffuse transfers.

By using ray-casting, which has proven to be an effective sampling method to evaluate light transfers, all sample points in the environment are considered [19]. Furthermore, the use of ray casting imposes no restriction on the geometry of the environment and allows every illuminator to be sampled adaptively.

The algorithm proceeds by successive steps similar to progressive radiosity "shots", but directional intensity distributions are continuously maintained on the surfaces instead of scalar radiosity values. The ideal specular contributions to the energy transfers are propagated immediately so they need never be stored.

2.2 View-independence vs. view-dependence

View-independent methods in general require the storage of illumination information on the surfaces, both for the purpose of the illumination computation and for use by a final view-dependent display algorithm. In the case of diffuse surfaces, storing a single radiosity value per wavelength channel at each sample point is sufficient, resulting in reasonable storage demands. In the same spirit, Immel et al. stored the directional information regarding the reflected intensity at each point, using a discrete set of directions [11]. If, however, the distribution of emitted or reflected light is sharply directional, as is the case with specular surfaces, storage becomes unmanageable if accuracy is to be maintained.

On the view-dependent side, distribution ray tracing [5] uses brute force, firing many reflection rays to simulate complex BRDFs, while path tracing [12] follows many paths through the scene to obtain a statistically reliable estimate. Here again, the property that made standard ray tracing [20] computationally tractable disappears (namely the restriction to ideal specular reflection that limits the number of rays), as rays must be fired towards all potential illuminators.

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2.3 Energy transfers for non-diffuse surfaces

Traditional radiosity methods assume an ideal diffuse behavior on all the surfaces, and express the transfers between surfaces by means of a form factor [7]. For the general case the amount of light reflected from a point can be expressed as follows.

Let us denote by $I(T_1, \vec{u})$ the intensity (or radiance), expressed in Watts per unit solid angle per unit projected area leaving a surface at point $T_1$, in the direction of the unit vector $\vec{u}$ (Figure 2). The energy $d^2E$ emitted by a differential surface area $dA_1$ around $T_1$ in the direction $\vec{u}$ and falling on a differential surface $dA_2$ around point $T_2$ is given by:

$$
\frac{d^2E}{dA_1} = I(T_1, \vec{u}) \left( \cos\theta_1 \cos\theta_2 \right) \frac{dA_2 \cos\theta_2}{r^2} \left( \frac{dA_1 \cos\theta_1}{r^2} \right)
$$

(1)

where $\vec{u} = -\hat{\vec{u}}$ is the unit vector pointing from $T_2$ to $T_1$.

This energy is scattered by the surface at $T_2$ in all directions. By definition of the BRDF $\rho_2$ at $T_2$, the intensity leaving $T_2$ in the direction $\vec{w}$, due to the incident light from $dA_1$, is given by:

$$
\frac{dI(T_2, \vec{w})}{dA_2} = \rho_2(\vec{v}, \vec{w}) \frac{d^2E}{dA_1}
$$

(3)
To evaluate the total intensity leaving $T_2$ in direction $\vec{u}'$, due to the reflection of light originating from a finite area $A_1$, Equation (2) must be integrated across $A_1$ giving:

$$I(T_2, \vec{u}') = \int_{A_1} I(T_1, \vec{u}) \frac{\cos \theta_1 \cos \theta_2}{r^2} \rho_2(\vec{v}, \vec{u}') dA_1$$  \hspace{1cm} (4)

Equation (4) represents the effect of the light emitted by a particular surface on the light that is scattered around a point on another surface. It describes the elementary shooting operation of the radiosity method. The traditional radiosity method simplifies Equation (4) in two ways: first, the BRDF $\rho$ is assumed to be diffuse, which makes it a constant independent of both $\vec{v}$ and $\vec{u}'$, and can thus be moved out of the integral. The diffuse assumption also makes $I(T_1, \vec{u})$ independent of $\vec{u}$. Second, the radiosity $\pi I(T_1)$ is assumed to be constant across the surface of the patch. The intensity term can thus be moved out of the integral, which then becomes purely geometric and is called the differential form factor.

If more general BRDFs are considered for the surface at $T_1$, however, the entire integrand must be considered. The next section explains how a form factor computation algorithm is adapted for that purpose.

3 General solution for arbitrary reflectances

A detailed description of the algorithm is presented below. The first pass, or solution pass, is very similar to progressive radiosity, and the implementation is a straightforward modification of an existing radiosity program. The second pass employs a simple ray tracer to retrieve the directional intensity information stored on the surfaces.

A central assumption of the method is that a directional intensity distribution $I(\vec{u})$ can be stored and accessed at each vertex of the environment. We discuss this topic further in section 5, where an efficient storage scheme is presented.

The method is explained here in terms of a meshed environment, composed of patches and elements [4], but it could be applied to radiosity textures [9] as well, if directional distributions are stored in the texture. The second (view-dependent) pass is described first, as it is a straightforward application of ray tracing.

3.1 Second pass

Once the view-independent solution has been computed in the first pass, a simple ray tracing pass is used to supply the view-dependent portion and create the final image. When rays encounter surfaces with a directional diffuse component, the intensity leaving a surface is retrieved from the directional distributions computed and stored in the first pass. The intensity contributed by ideal specular reflection is obtained by recursively following reflected rays as in conventional ray tracing. Note that a specular reflectance function is used to attenuate the reflected rays instead of a simple "specular coefficient". This allows a precise treatment of specular reflection, where roughness effects as well as Fresnel reflection are properly accounted for [8].

3.2 First pass

The first phase of the computation is an extension of progressive radiosity, but directional distributions are used throughout the algorithm in place of diffuse radiosities. The basic shooting operation now uses the directional intensity distribution emitted by the shooting patch to update the directional intensity distributions of the receiving vertices according to Equation (4).

This equation can be rewritten as a function of the intensity distributions rather than scalar values. If $\rho_2(\vec{v}, \cdot)$ denotes the BRDF for an incoming direction $\vec{v}$ as a function of the outgoing direction, and $I(T, \cdot)$ denotes the intensity distribution at point $T$, then the effect of shooting from $T_1$ to $T_2$ is

$$I(T_2, \cdot) = \int_{A_1} I(T_1, \vec{u}) \frac{\cos \theta_1 \cos \theta_2}{r^2} \rho_2(\vec{v}', \cdot) dA_1$$  \hspace{1cm} (5)

The algorithm presented below follows Equation (5) and decomposes the integral into a discrete sum. This is similar to the form factor computation algorithm of Wallace et al. [19], but modified to sum complete directional intensity distributions.

Approximation of the integral

To obtain the reflected intensity distribution given by (5), we follow the computation of the area-to-differential-area form factor used in [19].

Patch $A_1$ is broken into a number of smaller pieces according to any given sampling scheme, and a contribution (a scalar form-factor in the diffuse radiosity case, a directional distribution in our case) is computed for each piece. A variety of sampling strategies is available, and this formulation is independent of the particular scheme chosen. For $N$ samples, the total integral is expressed as:

$$I(T_2, \cdot) = \sum_{i=1}^{N} \delta I_i(T_2, \cdot)$$  \hspace{1cm} (6)

Given sample $i$, with area $A_i$ centered at $T_i$, the associated contribution to the integral in (4) could be crudely approximated by assuming the integrand constant, yielding:

$$\delta I_i(T_2, \cdot) = I(T_i, \vec{u}_i) \frac{\cos \theta_1 \cos \theta_2}{r^2} \rho_2(\vec{v}', \cdot) \delta A_i$$  \hspace{1cm} (7)

To avoid possible singularities when $T_1$ and $T_2$ are close together, we treat piece $i$ as a finite area, and use the approximation of a disk-shaped area as in [19]. This amounts to assuming that the emitted intensity does not vary significantly over the area of the piece, which is a common assumption of the radiosity formulation. The contribution of piece $i$ is then:

$$\delta I_i(T_2, \cdot) = I(T_i, \vec{u}_i) \cos \theta_1 \cos \theta_2 \frac{\pi \delta A_i}{\delta A_i + \pi r_i^2} \rho_2(\vec{v}', \cdot)$$  \hspace{1cm} (8)

Introducing the incident energy flux (Watts per unit area) incident on point $T_2$ from piece $i$

$$\delta \Phi_i = I(\vec{u}_i) \cos \theta_1 \cos \theta_2 \frac{\pi \delta A_i}{\delta A_i + \pi r_i^2} = I(\vec{u}_i) \delta F_i$$  \hspace{1cm} (9)

Equation (5) can be conveniently rewritten as:

$$I(T_2, \cdot) = \sum_{i=1}^{N} \delta \Phi_i \rho_2(\vec{v}', \cdot)$$  \hspace{1cm} (10)

It is apparent from equation (10) that $I$ is simply a weighted sum of the BRDF at $T_2$ over a set of incident directions. Each energy flux term, $\delta \Phi_i$, is the product of the intensity leaving a sample point on the shooting patch in the direction of the receiving vertex and the delta-form-factor for that sample point.
Do until convergence
Select Shooting Patch \( P_i \)
Call Shoot(\( P_i, S_{\text{generic}} \) )
End Do

Function Shoot(\( P_i, S \) ) {
For each Receiving Vertex \( V_j \)
For each Sample Point \( T_s \) on \( P_i \)
  Evaluate occlusion \( c = S(T_s, V_j) \)
  If \( (c \neq 0) \) Then
    Obtain the incoming energy flux on \( V_j \)
    Evaluate intensity \( I_s \) leaving \( T_s \) toward \( V_j \),
    using intensity distribution of patch \( P_i \);
    Compute \( \delta F \) = "delta-form-factor" between \( T_s \) and \( V_j \);
    Compute incident energy flux \( \Phi = c \cdot \delta F \cdot I_s \);
    Construct reflected intensity distribution
    Compute incident angles in local axes at \( V_j \);
    Retrieve BRDF \( \rho \) of surface at \( V_j \) for the incident angle;
    Create intensity distribution \( \Delta I = \Phi \cdot \rho \)
    in local axes according to incident direction;
    Add \( \Delta I \) to accumulated and unshot intensity
    distributions \( I \) and \( U \) at \( V_j \);
  End If
End For
End For

For each surface \( A \) flagged as specular
  Construct reflected patch \( P_i' \)
  Chain occlusion functions : \( S' = S \circ S_A \)
End For

Figure 3: Algorithm for first pass. Step D is explained in section 4

Discussion of the algorithm

The shooting operation that propagates the accumulated energy of
a patch into the environment is presented as a pseudocode subroutine (called SHOOT) in Figure 3. Given a shooting patch \( P_i \) and
a receiving sample point (vertex \( V_j \)), the following operations are
needed to update the directional intensity distribution of the vertex:

Sample points are selected on the shooting patch according to a
sampling algorithm. Our implementation uses an adaptive sampling
technique where the number and location of the sample points
depend on the results obtained from previous samples [19]. For each
sample point, a contribution is added to the reflected intensity dis-
tribution of the vertex.

The first task of the algorithm is to compute the incident energy
flux on the vertex, which is used to weight the BRDF as in equation
(10). This involves a visibility determination accomplished by the
occlusion function \( S \). In the simple cases where no ideal specular
reflection is present, this function simply returns 0 or 1
to encode occlusion between the sample point and the vertex. The
more complex cases are explained in Section 4. If the two points
can "see" each other, the intensity leaving the shooting patch is
obtained from the stored directional distribution of the patch, and
a delta-form-factor \( \delta F \) (geometric attenuation term) is computed
(Figure 3-A). The desired energy flux is the product of the intensity,
the delta-form-factor and the attenuation given by the occlusion
function (Figure 4).

Figure 4: Computation of the energy flux.

The second step is to compute the contribution of the current sam-
ple point to the intensity distribution (Figure 3-B). We start by ob-
taining a directional distribution representing \( p_{\text{incident}}(\theta, \phi) \), that is, the
BRDF for the given incident direction. This is retrieved by means
of the storage method described in section 5. The BRDF is then
scaled by the energy flux value \( \delta F \cdot I_s \), which results in the distribu-
tion of reflected intensity \( \Delta I \) due to the current sample point. If an
isotropic BRDF is used, the directional distribution depends only on
the incident elevation angle \( \theta \), and is obtained in a canonical coor-
dinate system ; it must be rotated to be properly aligned with the in-
cident azimuth angle \( \phi \) in the local coordinate system of the receiver
(Figure 5). Finally this contribution is added to the unshot intensity
distribution and the accumulated intensity distribution, much as in
traditional progressive radiosity (Figure 6).

Figure 5: Orientation of the BRDF. (1) : obtaining the BRDF ac-
ccording to \( \theta \). (2) : rotating the BRDF according to \( \phi \).

Previous work has shown that a complete treatment of light trans-
fers requires exchanges incorporating different modes of reflection.
Our shooting operation also includes a complete treatment of ideal
specular reflection, so that the effect of specular reflection on the
intensity distributions is completely evaluated, but no "specular intensity" is stored (see section 2). Section 4 explains this part of the algorithm in more detail.

4 Ideal specular transfers

As explained in Section 2, specularly reflected light is not stored in the directional distributions on the specular reflector. Instead it is immediately propagated to other surfaces where part of it will be stored in a directional distribution, and part may again be specularly reflected to other surfaces.

Our implementation is an adaptation of the "image method" [16] to the ray-traced form factor idea: if the specular surfaces are planar, one can simply reflect the shooting patch across the surface, and shoot light from this "virtual patch" to all receiving vertices (Figure 7). Note that the direction for each shot is chosen deterministically based on the position of a vertex; this is not a Monte Carlo sampling technique.

This method has several important benefits:

- Multiple specular reflections can be implemented by recursively creating virtual patches. It should be noted that since the shooting patch is the only one that need be reflected, there is no explosion of the complexity of the scene.

The current implementation is limited to planar specular surfaces. If more complex geometries are needed for the specular surfaces, it is no longer simple to construct a modified patch from which to shoot. Instead, specular rays can be fired from each receiving vertex lying on a specular surface, in a manner similar to [17]. However, the distribution of specular rays then depends on the mesh of vertices on the specular surface, with no guarantee that all vertices in the environment will receive their share of the specularly reflected light. A major benefit of the ray-casting approach to radiosity is then lost. Furthermore, rays must be properly weighted, taking surface curvature into account, to ensure a physically correct energy transfer.

4.1 Algorithm

The pseudo-code algorithm in Figure 3 contains two parts involving specular reflection (note that the treatment of specular reflection within the first pass occurs entirely within the shooting operation).

In the general loop that considers all receiving vertices in turn, specular surfaces are flagged whenever one of their vertices receives some energy from the shooting patch (Figure 3-C). Entire surfaces (planar patches) are flagged regardless of their subdivision into patches or elements, or their number of vertices.

Once all the vertices have had their directional intensity distributions updated with respect to the shooting patch, the specular reflectors are then considered in turn (Figure 3-D). For each specular surface, a new patch is created and the occlusion testing function is modified in preparation for a recursive call to the shooting procedure SHOOT.

The new patch is obtained by reflecting the original shooting patch and its attached coordinate system across the specular surface A. The new, virtual patch possesses the same intensity distributions as the original shooting patch except that they are reflected by virtue of the reflected coordinate system.

A shot from the virtual patch $P'$ affects only those vertices in the environments that can "see" the original shooting patch in the specular surface. This is easily accomplished by sampling the virtual patch as a normal shooting patch, but using a modified occlusion testing routine between the receiving vertex and the sample point. Figure 8 depicts the extended occlusion test.

An occlusion function (called $S_A$ in Figure 3, and described as pseudo-code in Figure 9) is first called: this function first looks for an intersection between the specular surface A and the ray linking the receiving vertex $V_i$ and a sample point on the virtual patch $T_S$. If no intersection is found, there can be no light reflected in that direction, and the function returns. Next, if an intersection point $T_S$ is found, a normal occlusion test is performed between $V_i$ and $T_S$. If the two points are visible to one another, the specular reflectance of the specular surface is computed for the appropriate reflection angle $r_S$.

If $S_A$ returns a non-zero value, the only remaining operation consists in determining the occlusion between $T_S$ and a sample point on the original shooting patch, that is, the reflected image of $T_S$ (Figure 8). This is accomplished by calling whatever occlusion function was in use at the current level of recursion: if we are dealing with a first specular reflection, the generic occlusion testing routine $S_{generic}$ is used. At deeper levels of recursion, a composite function obtained by previous chaining operations is used.
The entire operation can be described as chaining together the current occlusion testing function with the occlusion routine for the current specular surface. Note that once point \( \tau_S \) has been found on the specular surface, the order in which the two occlusion tests are carried out is arbitrary. However, since the occlusion test between \( \tau_S \) and \( V_j \) is generally a simpler test, it is performed first.

\[
I_k(\theta, \phi) = \sum_{i=1}^{n} \Phi_i \rho_k(\theta_i, \theta, \phi + \Delta \phi_i)
\]

Here \( \Phi_i \), \( \theta_i \), and \( \Delta \phi_i \) are the energy flux, angle of incidence, and azimuthal angle of the \( i \)th contribution respectively. Here we have expressed the BRDF parameters as angles with respect to a fixed local coordinate system at vertex \( k \) (Figure 5). The vertical axis of this coordinate system corresponds to the surface normal at that vertex though the other axes are arbitrary.

We therefore require a representation that is general enough to account for this variation while also accommodating the steps in Figure 3-B. High-order continuity is also a requirement, since a discrete description, such as the global cube [11], can result in severe aliasing problems. Furthermore, derivative discontinuities in the intensity distributions can cause artifacts such as Mach-banding on the illuminated surfaces, even if a perfectly accurate transfer of light is computed.

In the following sections we describe an approach based on spherical harmonics which meets these requirements. Using this mechanism we can compactly and accurately represent arbitrary BRDFs and their associated intensity distributions and efficiently perform all of the operations required for shooting and incremental creation. It is therefore a nearly ideal mechanism for storing the intensity distributions for this global illumination algorithm.

### 5.1 Approximation using Spherical Harmonics

Spherical harmonics form an orthogonal basis for the space of functions defined over the unit sphere [6]. This infinite collection of basis functions is typically denoted by \( Y_{l,m}(\theta, \phi) \) where \( 0 \leq l < \infty \) and \(-l \leq m \leq l \). In direct analogy with Fourier series in one dimension, any square-integrable function, \( f(\theta, \phi) \), can be represented by an infinite series of the form

\[
f(\theta, \phi) = \sum_{l=0}^{\infty} \sum_{m=-l}^{l} C_{l,m} Y_{l,m}(\theta, \phi)
\]

where the coefficients are given by

\[
C_{l,m} = \int_{0}^{2\pi} \int_{0}^{\pi} f(\theta, \phi) Y_{l,m}(\theta, \phi) \sin(\theta) \, d\theta \, d\phi.
\]
To construct such a representation for the intensity distributions we begin by approximating the BRDFs in terms of spherical harmonics. In previous work, Cabral et al. have used a similar approximation for the purpose of simulating diffuse and glossy reflections of the environment [2]. In the present work the dependence of the BRDF on the angle of incidence is accounted for by representing each spherical harmonic coefficient as a function of $\theta^\prime$. That is, for every BRDF we construct a collection of scalar functions, $B_{l,m}(\cdot)$, such that

$$
\rho(\theta^\prime, \theta, \phi) \cos \theta \approx \sum_{l=0}^{N} \sum_{m=-l}^{l} B_{l,m}(\theta^\prime) Y_{l,m}(\theta, \phi)
$$

(14)

In this way we can model the behavior of a BRDF over the entire range of incident angles. In our implementation the $B_{l,m}$ functions are stored as one-dimensional cubic splines; one for each spherical harmonic in the BRDF approximation. The $\cos \theta$ factor is included at this stage because it reduces evaluation time and tends to reduce ringing in the approximation. Figure 10 shows several of these curves for slightly rough aluminum. Additional details on this approximation can be found in Appendix A.

Figure 10: Seven spherical harmonic coefficients for the BRDF of slightly rough aluminum plotted as functions of the incident angle.

### 5.2 Operations on Spherical Harmonic Coefficients

Given a BRDF approximation of the form in equation (14) we can construct a corresponding intensity distribution using Equation (11). For every intensity contribution we first evaluate the BRDF at the given angle of incidence, $\theta^\prime$, by computing the spherical harmonic coefficients of the resulting directional distribution. This consists of evaluating an interpolating spline, $B_{l,m}(\cdot)$, for each coefficient.

Next, we scale the distribution by multiplying each of these coefficients by the energy flux. The third step, rotating the distribution about the vertical axis, is made simple by the following property of spherical harmonics (shown in real form).

$$
\begin{bmatrix}
Y_{l,m}(\theta, \phi + \alpha) \\
Y_{l,-m}(\theta, \phi + \alpha)
\end{bmatrix}
= 
\begin{bmatrix}
\cos(m \alpha) & -\sin(m \alpha) \\
\sin(m \alpha) & \cos(m \alpha)
\end{bmatrix}
\begin{bmatrix}
Y_{l,m}(\theta, \phi) \\
Y_{l,-m}(\theta, \phi)
\end{bmatrix}
$$

This property follows immediately from the definition of spherical harmonics given in Appendix A. Rotation about this axis is particularly straightforward, and the usual symmetry of the BRDFs with respect to the incident plane simplifies it even further. Because negatively subscripted spherical harmonics are odd functions with respect to $\phi$, we are guaranteed that all such coefficients will vanish in the BRDF approximation. These coefficients reappear in the intensity distributions, however, because the symmetry is destroyed when the BRDFs undergo arbitrary rotations. This can be seen in step 3 of figure 11.

### 6 Results

Solutions have been computed for several test environments to demonstrate the feasibility of the simulation for arbitrary reflectance distributions. The resulting pictures exhibit all the expected visual effects produced by directional diffuse as well as ideal specular energy transfers.

Figure 12 shows a side by side comparison of a simulated environment with a scanned physical environment. The scanned picture was obtained by scanning through three colored filters, where each channel is spectrally integrated over a large range of wavelengths. Thus, the comparison with a simulation computed with three well-defined monochromatic channels can only be qualitative (for example the general color tone is noticeably different). However, important features such as the structure of the shadow on the left, or the illumination of the ceiling via specular reflection from the top of the wall box, appear to be very similar. A related research project is un-
In figure 13, the tall box is covered with perfectly smooth aluminum, making it a first surface mirror. In figure 14 the surface has been roughened slightly. Note that ideal specular effects are still very strong, both in the reflected image on the box, and in the upper left corner of the environment, where light is reflected by the top of the tall box. The directional nature of the diffused light can also be seen on the front face of the tall box. In figure 15, the box is made somewhat rougher, and more of the light is being reflected in a directional diffuse manner. Note that the specular reflection is stronger on the left face of the box than it is on the front face because of the different incident angles for rays reaching the eye. This is a result of the model used to predict the specular reflectance [8] and is observed on real materials. Figure 16 shows an aluminum box that is rougher still, and the ideal specular component of the reflectance has almost disappeared. Note that there is still a concentration of light in the upper left corner of the scene, because light reflected by the top face of the box has a definite directional character. Figures 17 and 18 show the results of the algorithm run on more complex scenes. In figure 17 the aluminum bowl and cupboard doors are directional diffuse reflectors, and in figure 18 the telephone, the drawer handles and the blackboard frame are made of different varieties of aluminum.

Figure 13: First-surface mirror
Figure 14: Smooth Aluminum box #1
Figure 15: Smooth Aluminum box #2
Figure 16: Rough Aluminum
Figure 17: Kitchen with directional diffuse cupboards and mixing bowl. Note the highlights on the cupboards.
Figure 18: Desk with aluminum phone and drawer handles. Note the caustics on the back wall.
Conclusions

A way to develop precise radiometric measurement procedures so that accurate quantitative comparisons can be made [10].

Figures 13 to 16 show simulations of a simple environment with varying surface properties. The tall box is made of aluminum with increasing roughness throughout the sequence. Figures 17 and 18 demonstrate the method applied to complex scenes (consisting of 34400 and 30200 elements, respectively). The realistic picture required an average time of 5 minutes per radiosity shot, on an Apollo DN10000 computer with 64 Megabytes of main memory.

In all these simulations, between 80 and 133 coefficients were used to approximate the BRDFs, resulting in intensity distributions of 148 to 254 coefficients. The number of coefficients in the latter increases due to loss of symmetry as described in section 5.2. The number of coefficients was determined for each material in order to achieve a given precision in the approximation of the BRDF over the entire range of incidence angles. Ideal diffuse surfaces require only one coefficient, and in general the more directional the BRDF, the more coefficients are required to account for the higher frequencies in the shape.

In all cases the intensity distributions have been stored using fewer than 1 Kilobyte at each vertex, while the error in the approximation was kept to a few percent. For any fixed number of coefficients, however, the approximation will generally begin to degrade as the BRDF becomes increasingly directional. Fortunately, according to physical optics, this will be somewhat compensated by the fact that the ideal specular component, which is handled separately, begins to dominate in this case [8]. Therefore, even for nearly-perfect mirrors, we can maintain a reasonable accuracy in terms of energy balance without increasing storage.

7 Conclusions and future directions

An algorithm for the simulation of global illumination with arbitrary reflectance behaviors was presented. A general treatment of ideal specular to directional diffuse transfers was introduced, allowing all chains of reflection to be effectively simulated. An efficient method using spherical harmonics to store the directional diffuse intensity distributions has been demonstrated, which permits a given accuracy to be maintained with a fixed amount of storage per vertex throughout the simulation.

Other features could be added easily to the system. An extension to anisotropic reflectance models would require an extra level of interpolation to obtain the BRDF, since it would depend on both incident angles (elevation and azimuth). This can be accomplished by using a two-dimensional spline function instead of the current one-dimensional spline function for the spherical harmonics coefficients.

Polarization effects that are predicted by general reflectance models [8] could also be incorporated into the system very naturally, by using the complex formulation of spherical harmonics.

This method suffers from several limitations inherited from the progressive radiosity method. For example, the intensity distribution is assumed to be uniform across a patch at shooting time, even though more detailed information might already be available from the subdivision of the patch into elements. Better sampling strategies are also needed. However, we believe that the formulation of the global illumination problem in terms of directional distributions attached to the surfaces, combined with a physically consistent treatment of ideal specular reflection, allows a truly general solution to be computed for arbitrary reflectance distributions.

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References


Appendix A: More on spherical harmonics

In real form, the normalized spherical harmonics are defined by

\[ Y_{l,m}(\theta, \phi) = \begin{cases} 
N_{l,m} P_{l,m}(\cos \theta) \cos(m\phi) & \text{if } m > 0 \\
N_{l,0} P_{l,0}(\cos \theta) \sqrt{2} & \text{if } m = 0 \\
N_{l,m} P_{l,|m|}(\cos \theta) \sin(|m|\phi) & \text{if } m < 0 
\end{cases} \] (15)

where the normalizing constants, \( N_{l,m} \), are given by

\[ N_{l,m} = \sqrt{\frac{2l + 1}{2\pi} \frac{(l - |m|)!}{(l + |m|)!}} \] (16)

and the \( P_{l,m}(x) \) factors are associated Legendre polynomials. The latter can be evaluated with the recurrence relations

\[ P_{l+1,m}(x) = xP_{l,m}(x) - (l+1)P_{l-1,m}(x) \]

beginning with \( P_{0,0}(x) = 1 \) [15]. Applying these in conjunction with recurrence relations for generating \( \sin(\phi), \sin(2\phi), \ldots, \sin(m\phi) \) and \( \cos(\phi), \cos(2\phi), \ldots, \cos(m\phi) \), it is possible to evaluate spherical harmonic expansions using approximately 10 floating point operations per coefficient and no trigonometric function evaluations whatsoever.

Evaluation of the spherical harmonic functions is required for two purposes: shooting from an intensity distribution and creating the initial BRDF approximations. The former is a straightforward application of Equation 12 while the latter is more complicated and is performed once per distinct BRDF. To approximate an isotropic BRDF for all incident angles, we first compute

\[ b_{l,m} = \int_0^{\pi} \int_0^{2\pi} \rho(\theta, \phi) Y_{l,m}(\theta, \phi) \sin(\theta) d\theta d\phi \] (17)

for \( j = 0, 1, \ldots, q \) where \( 0 = \theta_0^j \leq \theta_1^j \leq \cdots \leq \theta_q^j = \pi/2 \). Then the functions \( B_{l,m} \) can be approximated by cubic interpolating splines through the the points \( (\theta_0^j, b_{l,0}^j), (\theta_1^j, b_{l,1}^j), \ldots, (\theta_q^j, b_{l,q}^j) \). For each distinct BRDF, \( \rho \), we select \( q \) as well as a specific set of spherical harmonic coefficients to achieve the desired accuracy of approximation over all incident angles. The value of \( q \) affects the accuracy of the interpolation but does not otherwise influence the intensity distributions. In contrast, the number of coefficients used in the BRDF approximation directly determines the storage required for the intensity distributions. It is therefore important to keep this number reasonably small.

If the BRDF that we wish to approximate is only defined on the upper hemisphere, as with an opaque material, we extend the function to the lower hemisphere before computing the approximation. We do this in such a way that the complete BRDF satisfies

\[ \rho(\theta^*, \phi) = -\rho(\theta^*, \pi - \phi), \] (18)

This introduces a vertical symmetry which has the advantage of eliminating all spherical harmonics for which \( l + m \) is even. It also maintains \( C^1 \) continuity between the upper and lower hemispheres when the function is zero at the equator, a condition that is guaranteed if the \( \cos \theta \) factor is included as described in section 5.1.