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Benchmarking sep-CMA-ES on the BBOB-2009 Function Testbed

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ABSTRACT

A partly time and space linear CMA-ES is benchmarked on the BBOB-2009 noiseless function testbed. This algorithm with a multistart strategy with increasing population size solves 17 functions out of 24 in 20-D.

Categories and Subject Descriptors

G.1.6 [Numerical Analysis]: Optimization—*global optimization, unconstrained optimization*; F.2.1 [Analysis of Algorithms and Problem Complexity]: Numerical Algorithms and Problems

General Terms

Algorithms

Keywords

Benchmarking, Black-box optimization, Evolutionary computation, Covariance matrix adaptation, Evolution strategy

1. INTRODUCTION

The sep-CMA-ES algorithm introduced in [7] is a variant of the covariance matrix adaptation evolution strategy (CMA-ES) [5] that is linear in time and space. This property combined with a faster learning rate makes sep-CMA-ES appropriate for separable function and larger dimensions. A mixed strategy of using sep-CMA-ES and CMA-ES is proposed here and benchmarked on a noiseless function testbed.

2. ALGORITHM PRESENTATION

In its design, the sep-CMA-ES differs from the CMA-ES by two aspects: first, the covariance matrix is constrained to be diagonal at each of its update, second, the learning rate is increased by a factor of $\frac{n+3/2}{3}$, where n is the dimension of the search space¹. These modifications result

¹Please note that the factor for the learning rate is smaller than the one in [7].

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in an algorithm that trades model complexity with a time and space scaling that is better than the original CMA-ES. The $(\mu/\mu_w, \lambda)$ -sep-CMA-ES has been shown to outperform $(\mu/\mu_w, \lambda)$ -CMA-ES on separable functions.

We propose here what would be the best of two worlds: to use sep-CMA-ES for the first few iterations and then switch to CMA-ES. At the time of the switch, all parameters are retained except for the learning rate that is decreased back to its default value. This implies the diagonal covariance matrix acquired using sep-CMA-ES is directly used by CMA-ES. This mixed strategy is therefore expected to be faster than CMA-ES on separable functions. Ongoing work has also shown that for some test functions the first iterations using sep-CMA-ES would not disadvantage the latter use of CMA-ES in any way. In other terms, the cost of initially using sep-CMA-ES would not induce a penalty in the cost of solving the function with CMA-ES afterwards. The author admits some functions could induce such a penalty.

As for the multistart strategy, we use the increasing population size IPOP-CMA-ES [1]. Though this approach has shown its limits [6], independent restart may improve the probability of the algorithm reaching a given target function value.

3. EXPERIMENTAL PROCEDURE

The Matlab implementation of the CMA-ES (version 3.23beta) is used². We use the $(\mu/\mu_w, \lambda)$ -IPOP-CMA-ES variant with an initial default population size $\lambda = 4 + \lfloor 3 \ln(n) \rfloor$ increasing twice at each restart. Except the learning rate, all other algorithm parameters are set to their default values. The covariance matrix is constrained to be diagonal only for the first $1 + 100n/\sqrt{\lambda}$ iterations of the *first start*. A maximum of 8 independent restarts is conducted. Restarts occur after $100 + 300n\sqrt{n/\lambda}$ iterations or if any of the default stopping criterion is met. The initial stepsize has been set to 2 and the starting point has been chosen uniformly in $[-4, 4]^n$. The maximum number of function evaluations was set to 10^4 times the dimension. No parameter tuning was done, the CrE [3] is computed to zero.

4. RESULTS AND DISCUSSION

Results from experiments according to [3] on the benchmark functions given in [2, 4] are presented in Figures 1 and 2 and in Table 1. The algorithm solves 17 out of the 24 functions in 20-D. The algorithm performs well on uni-

²Latest version available here: <http://www.lri.fr/~hansen/cmaesintro.html>

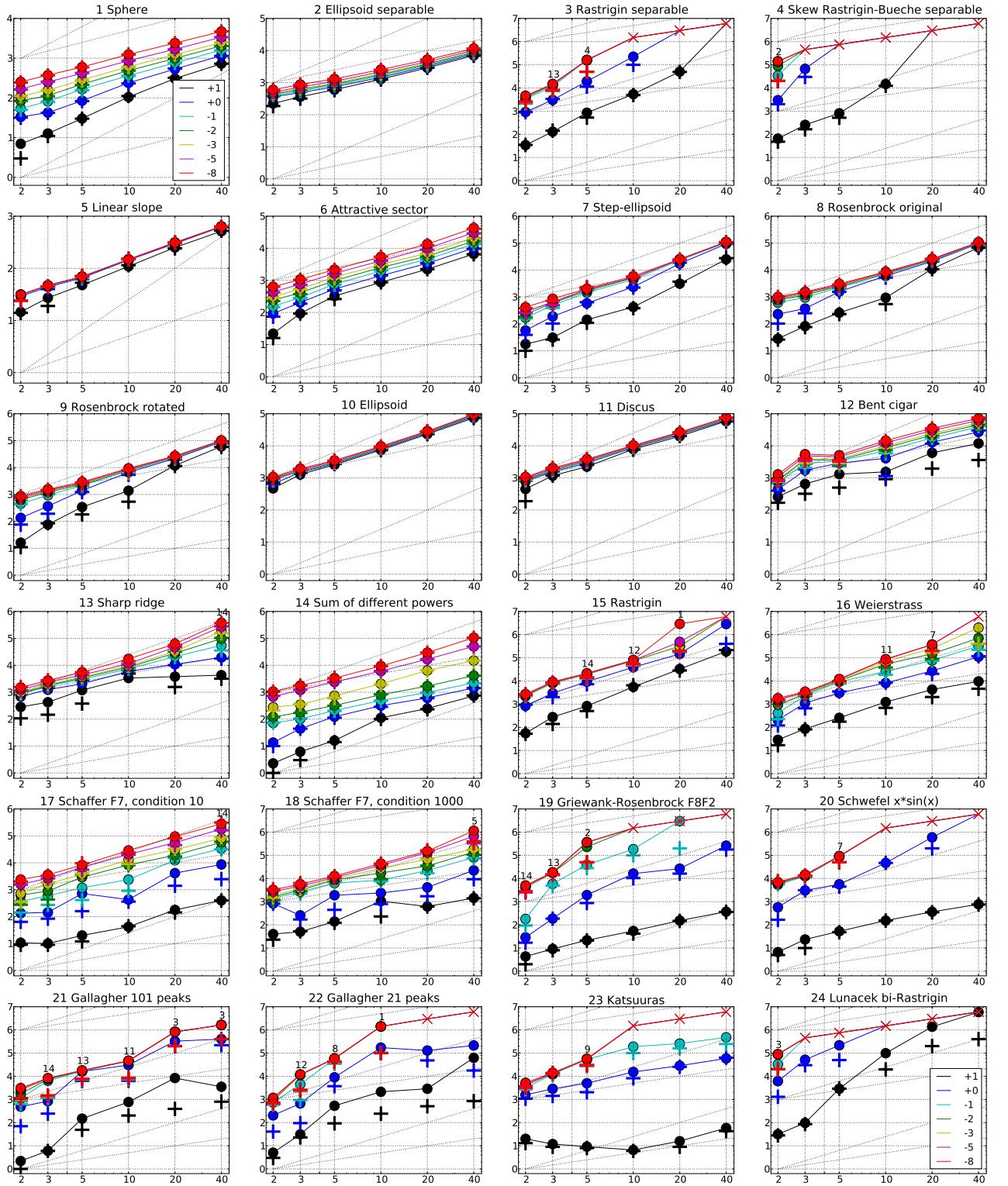


Figure 1: Expected Running Time (ERT, ●) to reach $f_{\text{opt}} + \Delta f$ and median number of function evaluations of successful trials (+), shown for $\Delta f = 10, 1, 10^{-1}, 10^{-2}, 10^{-3}, 10^{-5}, 10^{-8}$ (the exponent is given in the legend of f_1 and f_{24}) versus dimension in log-log presentation. The $\text{ERT}(\Delta f)$ equals to $\#\text{FEs}(\Delta f)$ divided by the number of successful trials, where a trial is successful if $f_{\text{opt}} + \Delta f$ was surpassed during the trial. The $\#\text{FEs}(\Delta f)$ are the total number of function evaluations while $f_{\text{opt}} + \Delta f$ was not surpassed during the trial from all respective trials (successful and unsuccessful), and f_{opt} denotes the optimal function value. Crosses (×) indicate the total number of function evaluations $\#\text{FEs}(-\infty)$. Numbers above ERT-symbols indicate the number of successful trials. Annotated numbers on the ordinate are decimal logarithms. Additional grid lines show linear and quadratic scaling.

<i>f</i> 1 in 5-D, N=15, mFE=738	<i>f</i> 1 in 20-D, N=15, mFE=2594	<i>f</i> 2 in 5-D, N=15, mFE=1554	<i>f</i> 2 in 20-D, N=15, mFE=5750	
Δf	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	
10	15 3.0e1 2.3e1 3.7e1 3.0e1	15 3.1e2 2.9e2 3.2e2 3.1e2	15 6.0e2 5.5e2 6.5e2 6.0e2	15 2.9e3 2.8e3 3.0e3 2.9e3
1	15 8.5e1 7.8e1 9.2e1 8.5e1	15 5.3e2 5.1e2 5.5e2 5.3e2	15 7.4e2 7.0e2 7.8e2 7.4e2	15 3.2e3 3.1e3 3.3e3 3.2e3
1e-1	15 1.7e2 1.5e2 1.8e2 1.7e2	15 7.6e2 7.4e2 7.8e2 7.6e2	15 8.3e2 7.9e2 8.6e2 8.3e2	15 3.5e3 3.4e3 3.6e3 3.5e3
1e-3	15 2.8e2 2.7e2 3.0e2 2.8e2	15 1.2e3 1.2e3 1.3e3 1.2e3	15 9.7e2 9.4e2 1.0e3 9.7e2	15 4.0e3 3.9e3 4.1e3 4.0e3
1e-5	15 4.2e2 4.0e2 4.3e2 4.2e2	15 1.7e3 1.6e3 1.7e3 1.7e3	15 1.1e3 1.1e3 1.1e3 1.1e3	15 4.5e3 4.4e3 4.6e3 4.5e3
1e-8	15 6.0e2 5.8e2 6.2e2 6.0e2	15 2.4e3 2.4e3 2.4e3 2.4e3	15 1.3e3 1.3e3 1.3e3 1.3e3	15 5.2e3 5.1e3 5.3e3 5.2e3
<i>f</i> 3 in 5-D, N=15, mFE=50422	<i>f</i> 3 in 20-D, N=15, mFE=200352	<i>f</i> 4 in 5-D, N=15, mFE=50430	<i>f</i> 4 in 20-D, N=15, mFE=200376	
Δf	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	
10	15 8.6e2 5.9e2 1.1e3 5.1e4	15 8.6e2 4.2e4 6.0e4 5.1e4	10 15 8.1e2 5.7e2 1.1e3 8.1e2	0 14e+0 13e+0 16e+0 1.1e5
1	13 1.9e4 1.3e4 2.7e4 1.5e4	0 60e-1 40e-1 70e-1 1.1e5	0 37e-1 30e-1 40e-1 1.8e4	.
1e-1	4 1.6e5 9.6e4 3.4e5 3.7e4	.	.	.
1e-3	4 1.6e5 9.8e4 3.5e5 3.8e4	.	.	.
1e-5	4 1.6e5 9.9e4 3.3e5 3.8e4	.	.	.
1e-8	4 1.6e5 1.0e5 3.4e5 3.9e4	.	.	.
<i>f</i> 5 in 5-D, N=15, mFE=106	<i>f</i> 5 in 20-D, N=15, mFE=410	<i>f</i> 6 in 5-D, N=15, mFE=2650	<i>f</i> 6 in 20-D, N=15, mFE=24422	
Δf	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	
10	15 4.8e1 4.2e1 5.4e1 4.8e1	15 2.5e2 2.3e2 2.7e2 2.5e2	10 15 3.2e2 2.6e2 3.9e2 3.2e2	15 2.2e3 2.1e3 2.3e3 2.2e3
1	15 6.6e1 6.0e1 7.2e1 6.6e1	15 3.0e2 2.8e2 3.2e2 3.0e2	15 5.3e2 4.7e2 6.1e2 5.3e2	15 3.4e3 3.2e3 3.5e3 3.4e3
1e-1	15 6.8e1 6.2e1 7.4e1 6.8e1	15 3.1e2 2.9e2 3.3e2 3.1e2	15 7.5e2 6.8e2 8.3e2 7.5e2	15 4.6e3 4.4e3 4.7e3 4.6e3
1e-3	15 6.9e1 6.4e1 7.5e1 6.9e1	15 3.1e2 2.9e2 3.3e2 3.1e2	15 1.3e3 1.2e3 1.3e3 1.3e3	15 7.0e3 6.8e3 7.2e3 7.0e3
1e-5	15 6.9e1 6.4e1 7.5e1 6.9e1	15 3.1e2 2.9e2 3.3e2 3.1e2	15 1.7e3 1.6e3 1.7e3 1.7e3	15 1.0e4 9.3e3 1.1e4 1.0e4
1e-8	15 6.9e1 6.4e1 7.5e1 6.9e1	15 3.1e2 2.9e2 3.3e2 3.1e2	15 2.2e3 2.1e3 2.2e3 2.2e3	15 1.4e4 1.3e4 1.5e4 1.4e4
<i>f</i> 7 in 5-D, N=15, mFE=3288	<i>f</i> 7 in 20-D, N=15, mFE=46966	<i>f</i> 8 in 5-D, N=15, mFE=5788	<i>f</i> 8 in 20-D, N=15, mFE=28922	
Δf	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	
10	15 1.4e2 1.2e2 1.7e2 1.4e2	15 3.1e3 2.6e3 3.6e3 3.1e3	10 15 2.6e2 2.1e2 3.1e2 2.6e2	15 1.1e4 1.1e4 1.1e4 1.1e4
1	15 5.8e2 5.0e2 6.6e2 5.8e2	15 1.7e4 1.5e4 2.0e4 1.7e4	15 1.6e3 1.3e3 1.9e3 1.6e3	15 2.1e4 2.1e4 2.1e4 2.1e4
1e-1	15 1.4e3 1.2e3 1.7e3 1.4e3	15 2.3e4 2.0e4 2.6e4 2.3e4	15 2.3e3 2.1e3 2.5e3 2.3e3	15 2.3e4 2.2e4 2.3e4 2.3e4
1e-3	15 1.9e3 1.6e3 2.1e3 1.9e3	15 2.5e4 2.2e4 2.8e4 2.5e4	15 2.7e3 2.5e3 2.9e3 2.7e3	15 2.4e4 2.4e4 2.5e4 2.4e4
1e-5	15 1.9e3 1.6e3 2.1e3 1.9e3	15 2.5e4 2.2e4 2.8e4 2.5e4	15 2.8e3 2.6e3 3.1e3 2.8e3	15 2.5e4 2.5e4 2.6e4 2.5e4
1e-8	15 2.0e3 1.8e3 2.3e3 2.0e3	15 2.5e2 2.2e2 2.9e4 2.5e4	15 3.1e3 2.9e3 3.3e3 3.1e3	15 2.6e4 2.6e4 2.7e4 2.6e4
<i>f</i> 9 in 5-D, N=15, mFE=4914	<i>f</i> 9 in 20-D, N=15, mFE=55924	<i>f</i> 10 in 5-D, N=15, mFE=4042	<i>f</i> 10 in 20-D, N=15, mFE=30386	
Δf	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	
10	15 3.4e2 1.9e2 4.9e2 3.4e2	15 1.2e4 1.1e4 1.2e4 1.2e4	10 15 2.6e3 2.5e3 2.7e3 2.6e3	15 2.3e4 2.2e4 2.4e4 2.3e4
1	15 1.4e3 1.2e3 1.6e3 1.4e3	15 2.2e4 1.9e4 2.4e4 2.2e4	15 2.8e3 2.7e3 2.9e3 2.8e3	15 2.5e4 2.4e4 2.6e4 2.5e4
1e-1	15 2.1e3 2.0e3 2.3e3 2.1e3	15 2.4e4 2.1e4 2.6e4 2.4e4	15 2.9e3 2.8e3 3.0e3 2.9e3	15 2.6e4 2.6e4 2.7e4 2.6e4
1e-3	15 2.5e3 2.3e3 2.7e3 2.5e3	15 2.5e4 2.3e4 2.7e4 2.5e4	15 3.1e3 3.0e3 3.2e3 3.1e3	15 2.7e4 2.7e4 2.8e4 2.7e4
1e-5	15 2.7e3 2.5e3 2.8e3 2.7e3	15 2.6e4 2.4e4 2.8e4 2.6e4	15 3.3e3 3.2e3 3.3e3 3.3e3	15 2.8e4 2.7e4 2.8e4 2.8e4
1e-8	15 2.9e3 2.8e3 3.1e3 2.9e3	15 2.7e4 2.5e4 2.9e4 2.7e4	15 3.5e3 3.4e3 3.6e3 3.5e3	15 2.9e4 2.8e4 2.9e4 2.9e4
<i>f</i> 11 in 5-D, N=15, mFE=4226	<i>f</i> 11 in 20-D, N=15, mFE=31418	<i>f</i> 12 in 5-D, N=15, mFE=9042	<i>f</i> 12 in 20-D, N=15, mFE=58382	
Δf	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	
10	15 2.2e3 1.9e3 2.5e3 2.2e3	15 2.0e4 1.9e4 2.0e4 2.0e4	10 15 3.6e3 4.0e3 8.2e3 6.1e3	15 2.3e4 2.2e4 2.4e4 2.3e4
1	15 2.9e3 2.8e3 3.0e3 2.9e3	15 2.2e4 2.2e4 2.3e4 2.2e4	15 2.9e3 2.6e3 3.2e3 2.9e3	15 2.5e4 2.4e4 2.6e4 2.5e4
1e-1	15 3.2e3 3.1e3 3.3e3 3.2e3	15 2.3e4 2.3e4 2.4e4 2.3e4	15 3.4e3 2.9e3 3.8e3 3.4e3	15 2.8e4 2.7e4 2.8e4 2.7e4
1e-3	15 3.4e3 3.4e3 3.5e3 3.4e3	15 2.5e4 2.4e4 2.5e4 2.5e4	15 3.9e3 3.4e3 4.6e3 3.9e3	15 3.0e4 2.7e4 3.3e4 3.0e4
1e-5	15 3.6e3 3.5e3 3.7e3 3.6e3	15 2.6e4 2.5e4 2.6e4 2.6e4	15 4.5e3 3.8e3 5.2e3 4.5e3	15 3.5e4 3.2e4 3.8e4 3.5e4
1e-8	15 3.8e3 3.8e3 3.9e3 3.8e3	15 2.7e4 2.6e4 2.7e4 2.7e4	15 5.1e3 4.3e3 5.9e3 5.1e3	15 3.0e4 2.9e4 3.0e4 3.0e4
<i>f</i> 13 in 5-D, N=15, mFE=6308	<i>f</i> 13 in 20-D, N=15, mFE=10488	<i>f</i> 14 in 5-D, N=15, mFE=3634	<i>f</i> 14 in 20-D, N=15, mFE=31850	
Δf	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	
10	15 1.2e3 8.5e2 1.6e3 1.2e3	15 3.8e3 2.6e3 5.0e3 3.8e3	10 15 1.6e2 1.2e1 2.0e1 1.6e1	15 2.5e2 2.3e2 2.7e2 2.5e2
1	15 2.1e3 7.7e3 2.4e3 2.1e3	15 1.1e4 8.4e3 1.3e4 1.1e4	15 1.2e2 1.1e2 1.4e2 1.2e2	15 6.1e2 5.8e2 6.5e2 6.1e2
1e-1	15 3.0e3 2.8e3 3.2e3 3.0e3	15 2.1e4 1.7e4 2.5e4 2.1e4	15 2.1e2 1.9e2 2.3e2 2.1e2	15 9.8e2 9.4e2 1.0e3 9.8e2
1e-3	15 3.7e3 3.6e3 3.8e3 3.7e3	15 3.3e4 2.9e4 3.6e4 3.3e4	15 7.4e2 6.3e2 8.5e2 7.4e2	15 6.4e3 6.1e3 6.7e3 6.4e3
1e-5	15 4.4e3 4.3e3 4.5e3 4.4e3	15 4.7e4 4.4e4 5.0e4 4.7e4	15 2.4e3 2.3e3 2.5e3 2.4e3	15 1.7e4 1.6e4 1.7e4 1.7e4
1e-8	15 5.5e3 5.4e3 5.7e3 5.5e3	15 6.2e4 5.7e4 6.8e4 6.2e4	15 3.3e3 3.3e3 3.4e3 3.3e3	15 3.0e4 2.9e4 3.0e4 3.0e4
<i>f</i> 15 in 5-D, N=15, mFE=50430	<i>f</i> 15 in 20-D, N=15, mFE=200340	<i>f</i> 16 in 5-D, N=15, mFE=32578	<i>f</i> 16 in 20-D, N=15, mFE=200340	
Δf	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	
10	15 8.3e2 5.1e2 1.2e3 8.3e2	15 3.3e4 2.8e4 3.8e4 3.3e4	10 15 4.3e3 2.3e3 6.3e3 4.3e3	15 6.2e2 2.0e2 2.6e2 6.2e2
1	15 9.3e3 7.7e3 1.1e4 9.3e3	15 1.5e5 1.3e5 1.6e5 1.5e5	15 2.9e3 2.6e3 3.2e3 2.9e3	15 1.3e4 9.9e3 1.6e4 1.3e4
1e-1	14 1.9e4 1.5e4 2.4e4 1.8e4	9 3.1e5 2.4e5 4.5e5 1.8e5	15 3.4e3 2.9e3 3.8e3 3.4e3	15 1.8e4 1.4e4 2.1e4 1.8e4
1e-3	14 2.0e4 1.6e4 2.5e4 1.9e4	9 3.2e5 2.5e5 4.3e5 1.9e5	15 3.9e3 3.4e3 4.6e3 3.9e3	15 2.5e4 2.2e4 2.8e4 2.5e4
1e-5	14 2.1e4 1.6e4 2.6e4 1.9e4	6 4.9e5 3.5e5 7.5e5 2.0e5	15 4.5e3 3.8e3 5.2e3 4.5e3	15 3.0e4 2.7e4 3.3e4 3.0e4
1e-8	14 2.2e4 1.7e4 2.7e4 2.0e4	1 2.9e6 1.6e6 >3e6 >3e6	15 5.1e3 4.3e3 5.9e3 5.1e3	15 3.5e4 3.2e4 3.8e4 3.5e4
<i>f</i> 17 in 5-D, N=15, mFE=12542	<i>f</i> 17 in 20-D, N=15, mFE=159622	<i>f</i> 18 in 5-D, N=15, mFE=21008	<i>f</i> 18 in 20-D, N=15, mFE=171622	
Δf	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	
10	15 2.0e1 1.4e1 2.5e1 2.0e1	15 1.8e2 1.5e2 2.1e2 1.8e2	10 15 1.4e2 1.1e2 1.6e2 1.4e2	15 6.2e2 5.7e2 6.7e2 6.2e2
1	15 7.2e2 1.8e2 1.3e3 7.2e2	15 4.1e3 1.4e3 6.9e3 4.1e3	15 1.9e3 1.0e3 2.9e3 1.9e3	15 4.1e3 2.0e3 6.1e3 4.1e3
1e-1	15 1.2e3 6.8e2 1.7e3 1.2e3	15 2.4e4 1.9e4 3.5e4 2.4e4	15 6.3e3 5.1e3 7.6e3 6.3e3	15 2.2e4 1.9e4 2.5e4 2.2e4
1e-3	15 3.8e3 3.2e3 4.5e3 3.8e3	15 3.1e4 2.7e4 3.5e4 3.1e4	15 9.6e3 8.2e3 1.1e4 9.6e3	15 6.8e4 5.8e4 7.8e4 6.8e4
1e-5	15 6.9e3 5.8e3 7.9e3 6.9e3	15 5.6e4 5.0e4 6.2e4 5.6e4	15 1.1e4 9.6e3 1.2e4 1.1e4	15 1.3e5 1.2e5 1.4e5 1.3e5
1e-8	15 8.3e3 7.1e3 9.3e3 8.3e3	15 9.5e4 8.4e4 1.1e5 9.5e4	15 1.3e4 1.2e4 1.4e4 1.3e4	15 1.5e5 1.4e5 1.6e5 1.5e5
<i>f</i> 19 in 5-D, N=15, mFE=50122	<i>f</i> 19 in 20-D, N=15, mFE=200096	<i>f</i> 20 in 5-D, N=15, mFE=50502	<i>f</i> 20 in 20-D, N=15, mFE=200316	
Δf	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	
10	15 2.2e1 1.8e1 2.6e1 2.2e1	15 1.5e2 1.3e2 1.8e2 1.5e2	10 15 5.3e1 4.4e1 6.1e1 5.3e1	15 3.6e2 3.4e2 3.9e2 3.6e2
1	15 1.9e3 9.5e2 3.0e3 1.9e3	15 2.7e4 1.8e4 3.6e4 2.7e4	15 5.6e3 3.8e3 7.4e3 5.6e3	5 6.0e5 4.2e5 1.0e6 2.0e5
1e-1	13 3.9e4 3.1e4 5.0e4 3.0e4	1 3.0e6 1.5e6 >3e6 >3e6	15 8.9e4 6.2e4 1.4e5 3.7e4	0 11e-1 9.1e-2 12e-1 1.3e5
1e-3	2 3.6e5 1.9e5 >7e5 5.0e4	0 29e-2 18e-2 51e-2 2.0e5	15 9.1e4 6.4e4 1.5e5 3.8e4	.
1e-5	2 3.6e5 1.9e5 >7e5 5.0e4	.	15 9.2e4 6.5e4 1.5e5 3.8e4	.
1e-8	2 3.7e5 1.9e5 >7e5 5.0e4	.	15 9.4e4 6.6e4 1.4e5 3.9e4	.
<i>f</i> 21 in 5-D, N=15, mFE=50246	<i>f</i> 21 in 20-D, N=15, mFE=200714	<i>f</i> 22 in 5-D, N=15, mFE=50672	<i>f</i> 22 in 20-D, N=15, mFE=200762	
Δf	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	# ERT 10% 90% RT _{succ}	
10	15 1.5e2 4.5e2 2.6e2 1.5e2	15 8.4e3 1.6e3 1.6e4 8.4e3	10 15 5.3e2 2.4e2 8.4e2 5.3e2	15 2.9e3 1.5e3 4.4e3 2.9e3
1	15 1.6e4 9.7e3 2.3e4 1.4e4	6 3.3e5 2.2e5 5.5e5 1.5e5	15 2.9e3 4.8e3 1.4e4 8.8e4	10 1.3e5 8.4e4 1.9e5 8.7e4
1e-1	13 1.7e4 1.0e4 2.3e4 1.5e4	3 8.2e5 4.6e5 6.6e5 1.4e5	15 5.6e4 3.8e4 9.0e3 2.8e4	0 69e-2 69e-2 51e-1 1.3e4
1e-3	13 1.7e4 1.1e4 2.5e4 1.5e4	3 8.2e5 4.6e5 6.5e6 1.4e5	15 8.5e4 3.9e4 9.3e4 2.8e4	.
1e-5	13 1.7e4 1.1e4 2.5e4 1.5e4	3 8.2e5 4.6e5 6.5e6 1.4e5	15 8.5e4 3.9e4 9.2e4 2.8e4	.
1e-8	13 1.8e4 1.1e4 2.6e4 1.6e4	3 8.2e5 4.6e5 6.5e6 1.4e5	15 8.5e4 3.9e4 9.4e4 2.8e4	.
<i>f</i> 23 in 5-D, N=15, mFE=50064	<i>f</i>			

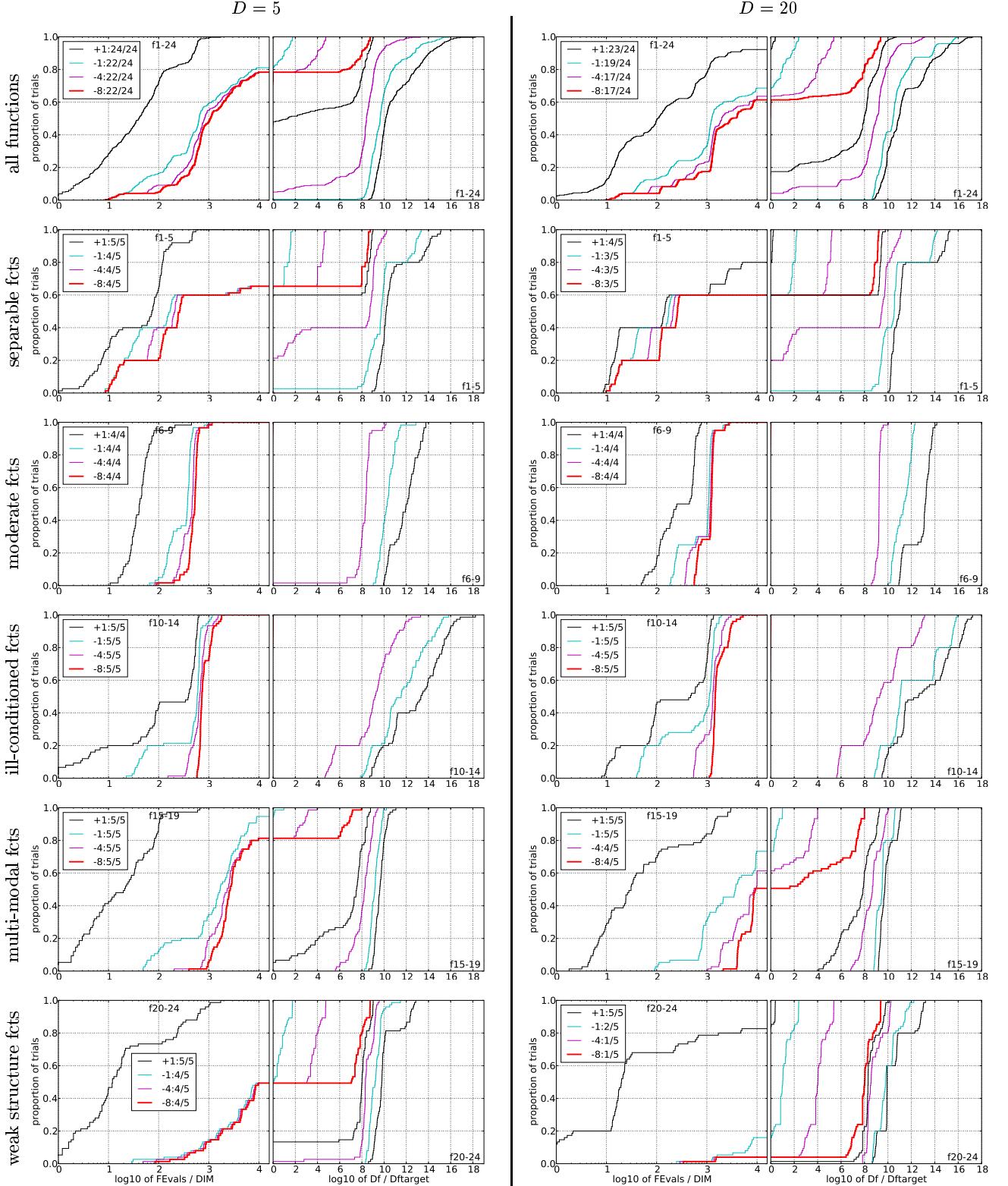


Figure 2: Empirical cumulative distribution functions (ECDFs), plotting the fraction of trials versus running time (left subplots) or versus Δf (right subplots). The thick red line represents the best achieved results. Left subplots: ECDF of the running time (number of function evaluations), divided by search space dimension D , to fall below $f_{\text{opt}} + \Delta f$ with $\Delta f = 10^k$, where k is the first value in the legend. Right subplots: ECDF of the best achieved Δf divided by 10^k (upper left lines in continuation of the left subplot), and best achieved Δf divided by 10^{-8} for running times of $D, 10D, 100D \dots$ function evaluations (from right to left cycling black-cyan-magenta). Top row: all results from all functions; second row: separable functions; third row: misc. moderate functions; fourth row: ill-conditioned functions; fifth row: multi-modal functions with adequate structure; last row: multi-modal functions with weak structure. The legends indicate the number of functions that were solved in at least one trial. FEval denotes number of function evaluations, D and DIM denote search space dimension, and Δf and Df denote the difference to the optimal function value.

modal separable functions as expected. Its performances on multimodal functions, even separable ones such as f_3 and f_4 , are limited though. Whereas for multimodal functions increasing the maximum number of function evaluations is likely to improve the performances of the algorithm, this should not be the case for f_{24} . For the timing experiment, the proposed algorithm was run on f_8 and restarted until at least 30 seconds have passed (according to Figure 2 in [3]). The experiments were conducted with an Intel Core 2 6700 processor (2.66GHz) with Matlab R2008a on Linux 2.6.24.7. The results were 15, 13, 11, 9.7, 9.9, and 13×10^{-5} seconds per function evaluations in dimension 2, 3, 5, 10, 20, and 40 respectively.

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