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Olivier Bernard[1]**, Georges Bastin**[2]

[1]INRIA-COMORE, BP93, 06902 Sophia-Antipolis Cedex, France, e-mail: `olivier.bernard@inria.fr`
[2]UCL-CESAME, av. G. Lemaître 4-6, 1348 Louvain-La-Neuve, Belgium, e-mail: `bastin@auto.ucl.ac.be`

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Abstract In this paper we propose a methodology to determine the structure of the pseudo-stoichiometric coefficient matrix K in a mass balance based model and to identify its coefficients from a set of available data. The first stage consists in estimating the number of reactions that must be taken into account to represent the main mass transfer within the bioreactor. This provides the dimension of K. Then we propose a method to directly determine the structure of the matrix (*i.e.* mainly its zeros and the signs of its coefficients). These methods are illustrated with simulations of a process of lipase production from olive oil by *Candida rugosa*.

1 Introduction and motivation

Macroscopic modelling provides simple dynamical models which have proved of great interest in bioengineering for the design of on-line algorithms for bioreactor monitoring, control and optimisation [1,2]. In such works, the dynamical behaviour of a stirred tank bioreactor is often described by the following general macroscopic mass-balance model:

$$\frac{d\xi(t)}{dt} = K\, r(t) + v(t), \qquad (1)$$

In this model, the vector $\xi = (\xi_1, \xi_2, \ldots, \xi_n)^T$ is made-up of the concentrations of the various species inside the liquid medium. The term $v(t)$ represents the net balance between inflows, outflows and dilution effects. The term $K\, r(t)$ represents the biological and biochemical conversions in the reactor (per unit of time) according to some underlying reaction network. The $(n \times p)$ matrix K is a constant pseudo-stoichiometric matrix. $r(t) = (r_1(t), r_2(t), \ldots, r_p(t))^T$ is a vector of reaction rates (or conversion rates). It is supposed to depend on the state ξ and on external environmental factors such as temperature, light or pressure, etc

The pseudo-stoichiometric (PS) matrix K is associated to a macroscopic reaction network that lumps together the many intracellular metabolic reactions of the various involved microbial species. The reaction network summarises then the main mass transfer throughout the bioreactor by a few reactions involving mainly extracellular compounds and biomasses without describing into all details the intracellular behaviour. Each column of the matrix corresponds to a chemical or biological reaction of the underlying macroscopic reaction network. The coefficients $k_{ij}\ \ j = 1, \ldots, p$ are associated with the jth reaction. A positive k_{ij} means that the ith species ξ_i is a product of the jth reaction, while a negative k_{ij} means that ξ_i is a substrate of the jth reaction. If $k_{ij} = 0$ the species ξ_i is not involved in the jth reaction.

In this paper, we are concerned with modelling situations where the on-line concentrations ξ_i of the involved species are measured but the structure of the reaction network is *a priori* questionable and therefore the matrix K is partially unknown. The objective, as in [5], is to provide guidelines to the user for the identification of the structure of a macroscopic reaction network and the determination of the PS matrix K from the available data. Note that the method can also be applied to simplify a known detailed intracellular metabolic network and provide a simpler reaction network that represents the main mass transfers throughout the system and directly connect initial substrates to final products. In such a case the concentrations ξ_i would result from simulations of a model based on the detailed known reaction network and matrix K is to be found from these "data".

The usual approach dedicated to the determination of reaction networks relies on the linearisation of the dynamics around a reference solution [9,7] and identification of the local jacobian matrix. This approaches are then suitable for data close to steady state. Here, in the spirit of [6,3], we use linear algebraic properties to exploit the structure of the bioprocesses (Equation (1))
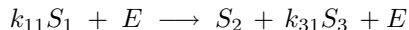
and our arguments do not rely on any linearisation. As a consequence we are not limited to steady state data and we can exploit all the available measurements, even when associated to transient states.
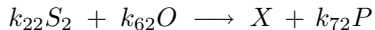
The problem is illustrated with the following example.

Example: Let us consider the example of a competitive growth on two substrates [12] which could represent, for instance, the production of lipase from olive oil by *Candida rugosa*. Here the microorganism is supposed to grow on two substrates that are produced by the hydrolysis of a primary complex organic substrate.

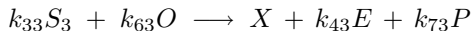The following 3-step reaction network has been assumed in the literature [6]:

- Hydrolysis:

$$k_{11}S_1 + E \longrightarrow S_2 + k_{31}S_3 + E$$

- Growth on S_2:

$$k_{22}S_2 + k_{62}O \longrightarrow X + k_{72}P$$

- Growth on S_3:

$$k_{33}S_3 + k_{63}O \longrightarrow X + k_{43}E + k_{73}P$$

where S_1 is the primary substrate (olive oil, made of several compounds, mainly triglycerides), S_2 (glycerol) and S_3 (fatty acids) are the secondary substrates. E is the enzyme (lipase), X the biomass (*Candida rugosa*), O the dissolved oxygen and P the dissolved carbon dioxide.

The associated PS matrix is:

$$K = \begin{pmatrix} -k_{11} & 0 & 0 \\ 1 & -k_{22} & 0 \\ k_{31} & 0 & -k_{33} \\ 0 & 0 & k_{43} \\ 0 & 1 & 1 \\ 0 & -k_{62} & -k_{63} \\ 0 & k_{72} & k_{73} \end{pmatrix}$$

$$\triangle$$

with $k_{ij} > 0$.

We shall assume that this reaction network is unknown to the user and has to be discovered from data of the species concentrations. Here the data will be simulated by a model but of course in practice the data are obtained from experiments.

Generally, the choice of a reaction network and its associated PS matrix K results from modelling assumptions. Sometimes however, a complete description of the reaction network is *a priori* not available. This can be a consequence of a lack of phenomenological knowledge on some of the involved mechanisms, letting a part of the reaction network questionable. The problem can also arise when it is desired to reduce a complicated given reaction network to a much simpler model. This situation especially occurs for models describing wastewater treatment processes involving a bacterial consortium made of

a broad range of bacterial species degrading a mixture of organic substrates. For example, more than 140 bacterial species have been found [8] in an anaerobic digestion wastewater treatment plant.

We first propose a method to determine the size of matrix K ı.e. the number of independent reactions that are distinguishable from the available data. Then we show how the structure of matrix K can be estimated, using the *a priori* available knowledge on the process. By structure we mean the sign and the location of the non-zero entries of matrix K. In addition, the method can also provide an estimate of the parameters k_{ij} if the available knowledge is sufficient.

2 Determination of the number of reactions

2.1 Introduction

In this section, we intend to determine the minimum number of reactions which are needed in order to explain the observed behaviour of the process, without any prior knowledge on the underlying reaction network. We assume that the vectors $\xi(t)$ of species concentrations and $v(t)$ of inflow/outflow balances are measured during some time interval and exhibit significant variations with time. We assume also that the number of measured variables is larger than the number of reactions: $n > p$. The PS matrix K and the vector of reaction/conversion rates $r(t)$ are unknown.

2.2 Theoretical determination of $\dim(\mathcal{I}m(K))$

The model equation (1) can be viewed as a linear dynamical system with state ξ and inputs $r(t)$ and $v(t)$ (although we know obviously that r and v may be state dependent). If we take the Laplace transform of this equation, we get:

$$s\Xi(s) = KR(s) + V(s) \qquad (2)$$

where $\Xi(s)$, $R(s)$ and $V(s)$ are the Laplace transforms of $\xi(t)$, $r(t)$ and $v(t)$ respectively. A linear filter or smoother with transfer function $G(s)$ can then be used in order to clean the data (noise reduction, decrease of autocorrelations etc ...):

$$U(s) = KW(s) \text{ with } U(s) = G(s)[s\Xi(s) - V(s)]$$

and $W(s) = G(s)R(s)$. Or, in the time domain:

$$u(t) = Kw(t) \qquad (3)$$

with $u(t)$ and $w(t)$ the inverse Laplace transforms of $U(s)$ and $W(s)$ respectively. The vector $u(t)$ can be computed directly from the data by appropriate filtering/smoothing techniques possibly involving delay operators.

For example, the moving average is a very simple filter that can be applied to (1), and provides an expression of the form (3) with (T denotes the considered moving average window):

$$u(t) = \frac{1}{T}\left[\xi(t) - \xi(t - T) - \int_{t-T}^{t} v(\tau)d\tau\right] \quad (4)$$

and

$$w(t) = \frac{1}{T}\left[\int_{t-T}^{t} r(\tau)d\tau\right]$$

Now the question of the dimension of matrix K can be formulated as follows: what is the dimension of the image of K ? In other words, what is the dimension of the space where $u(t)$ lives ? Note that we assume K to be a full rank matrix. Otherwise, it would mean that the same dynamical behaviour could be obtained with a matrix K of lower dimension, by defining other appropriate reaction rates. The determination of the dimension of the $u(t)$ space is a classical problem in statistical analysis. It corresponds to the principal component analysis (see e.g. [11]) that determines the dimension of the vector space spanned by the vectors k_i which are the rows of K. To reach this objective, we consider the $n \times N$ matrix U obtained from a set of N estimates of $u(t)$:

$$U = (u(t_1), \ldots, u(t_N))$$

We will also consider the associated matrix of reaction rates, which is unknown:

$$W = (w(t_1), \ldots, w(t_N))$$

We assume that matrix W is full rank. It means that the reactions are independent (none of the reaction rates can be written as a linear combination of the others). We consider more time instants t_i than state variables: $N > n$.

Property 1 *For a matrix K of rank p, if W has full rank, then the $n \times n$ matrix $M = UU^T = KWW^TK^T$ has rank p. Since it is a symmetric matrix, it can be written:*

$$M = P^T \Sigma P$$

where P is an orthogonal matrix ($P^T P = I$) and

$$\Sigma = \begin{pmatrix} \sigma_1 & 0 & & \cdots & & 0 \\ 0 & \sigma_2 & 0 & & & 0 \\ \vdots & & \ddots & & & \\ & & & \sigma_p & & \\ & & & & 0 & \\ & & & & & \ddots & \vdots \\ 0 & & \cdots & & & 0 \end{pmatrix}$$

with $\sigma_{i-1} \geq \sigma_i > 0$ for $i \in \{2, ..., p\}$.

Moreover, the eigenvectors associated with the σ_i generate an orthonormal basis of $\mathcal{I}mK$.

This property is a direct application of the singular decomposition theorem [10] since rank $(M) =$ rank $(KW) =$ rank $(K) =$ rank $(\Sigma) = p$.

Now from a theoretical point of view, it is clear that the number of reactions can be determined by counting the number of non zero singular values of UU^T.

2.3 Practical implementation

In practice, the ideal case presented above is perturbed for three main reasons:

- The reaction network that we are looking for is a first approximation of chemical or biochemical reactions which can be very complex. The "true" matrix K is probably much larger. The reactions that are fast or of low magnitude can be considered as perturbations of a dominant low dimensional reaction network that we are actually trying to estimate
- The measurements are corrupted by noise. This noise can be very important, especially for the measurement of biological quantities for which reliable sensors are not available.
- In order to compute $u(t)$ we need a numerical implementation of the filter $G(s)$. Moreover an interpolation is often required to estimate the values of $\xi(t_i)$ and $v(t_i)$ at the same time instants t_i. These processes generate additional perturbations.

2.3.1 Data normalisation In order to avoid conditioning problems and to give the same weighting to all the variables, the data vectors $u(t_i)$ are normalised as follows:

$$\tilde{u}_i(t_j) = \frac{u_i(t_j) - a(u_i)}{\sqrt{N}s(u_i)}$$

where $a(u_i)$ is the average value of the $u_i(t_k)$ for $k \in \{1..N\}$, and $s(u_i)$ their standard deviation.

2.3.2 Practical determination of the number of reactions In practice, for the reasons we have mentioned above, it is well known that there are no zero eigenvalues for the matrix $M = UU^T$.

The question is then to determine the number of eigenvectors that must be taken into account in order to produce a reasonable approximation of the data $u(t)$. To answer that question, let us remark that the eigenvalues σ_i of M correspond to the variance associated with the corresponding eigenvector (inertia axis) [11].

The method then consists in selecting the p first principal axis which represent a total variance larger than a fixed confidence threshold.

For instance, in the next example, we will consider a threshold (depending on the information available on noise measurements) at 95% of the variance. This leads to the selection of 3 axis, and therefore $p = 3$.

Remark: if rank $(M) = n$ it means that $rank(K) \geq n$. In such a case we cannot estimate p and measurements of additional variables are requested in order to apply the method presented here.

Parameter	Value	Unit
c_0	0.5	g/l.day^{-1}
c_1	3	day^{-1}
c_2	1	g/l
c_3	0.2	g/l
c_4	20	g.day$^{-1}l^{-1}$
c_5	1	g/l
c_6	0.2	g/l
c_7	2	g^2/l^2
c_8	2	g/l
c_9	0.2	g/l
c_{10}	5	day^{-1}
c_{11}	15	g/l
c_{12}	5	day^{-1}
c_{13}	0.5	g/l

Table 1 Parameters values.

2.3.3 Example: competitive growth on two substrates We come back to the example which has been introduced above. Consistently with Equation (1), the model for the state

$$\xi = (S_1, S_2, S_3, E, X, 0, P)^t$$

involving 3 main reactions can thus be written:

$$\frac{d\xi}{dt} = K \begin{pmatrix} r_1 \\ r_2 \\ r_3 \end{pmatrix} + v(t)$$

where

$$v(t) = D(\xi_{in} - \xi) - Q(\xi)$$

with $\xi_{in} = (S_{1in}, S_{2in}, S_{3in}, 0, 0, 0, 0)^t$ the vector of influent concentrations and $Q(\xi) = (0, 0, 0, 0, 0, qo_2(O), qco_2(P))^t$ the vector of gaseous flow rates.

The matrix K was chosen as follows:

$$K = \begin{pmatrix} -3 & 0 & 0 \\ 1 & -5 & 0 \\ 0.3 & 0 & -0.5 \\ 0 & 0 & 0.2 \\ 0 & 1 & 1 \\ 0 & -2 & -1 \\ 0 & 0.3 & 1.5 \end{pmatrix}$$

For the simulation purpose, we assume that the kinetics of the three reactions are given by the following expressions. They have not been selected on a realistic basis, but more in order to illustrate our approach on a broad variety of kinetics:

$$r_1(S_1, E) = c_0 \frac{S_1}{S_1 + c_8} \frac{E}{E + c_9} X$$

$$r_2(S_2, O, X) = c_1 \frac{S_2}{S_2 + c_2} \frac{O}{O + c_3} X$$

$$r_3(S_2, S_3, O) = c_4 \frac{S_3}{(S_3 + c_5)(S_2 + c_6)} \frac{O^2}{O^2 + c_7} X;$$

The transfer between liquid and gaseous phase is represented by the classical Henry's law:

$$qco_2(P) = c_{10}(P - c_{11}) \text{ and } qo_2(O) = c_{12}(O - c_{13})$$

The values of the coefficients c_i can be found in Table 1.

Initial condition	Value	Unit
$S_1(0)$	10	g/l
$S_2(0)$	0	g/l
$S_3(0)$	5	g/l
$E(0)$	5	g/l
$X(0)$	15	g/l
$O(0)$	0	g/l
$P(0)$	0	g/l

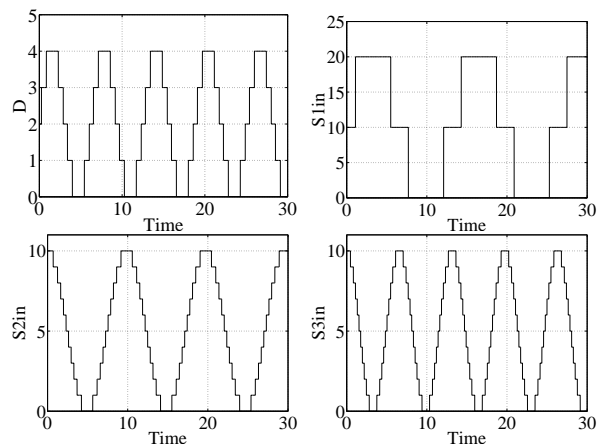**Table 2** Initial conditions used for the simulation.

Fig. 1 Values of dilution rate, S_{1in}, S_{2in} and S_{3in} used for the simulation.

A 30 day run of the model has been performed using the initial conditions provided in Table 2. The collected data have been corrupted with a white noise of high magnitude (30% of the standard deviation of each component) and sampled. Finally 380 data points are available.

The data (after sampling) are presented in Figure 2. The state variables S_2, S_3, E, X, P, O and of the gaseous flow rates q_{O_2} and q_{CO_2} have been measured. We assume here that the state variable S_1 was not recorded in order to illustrate the fact that our approach is applicable

even if the full set of state variables is not available for measurement. Moreover the dilution rate and the substrate inflow rate (see Figure 1) have been selected in order to guarantee that the system is sufficiently excited and therefore that the recorded signals will have a sufficiently informative content to expect good identification results.
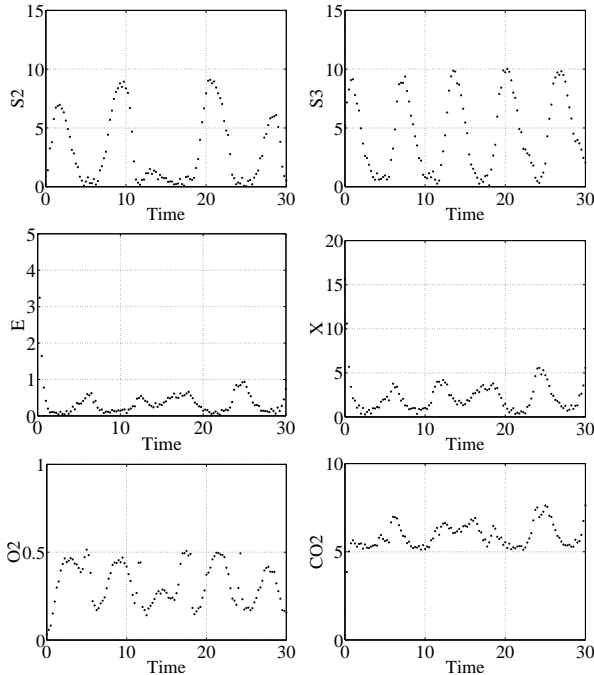

Fig. 2 Experiment simulated from the kinetic modelling corrupted with an additive white noise.

The vectors $u(t_i)$ are then computed by applying a simple moving average from these data and subsequently normalised as explained before. Finally, the eigenvectors of UU^T are computed.
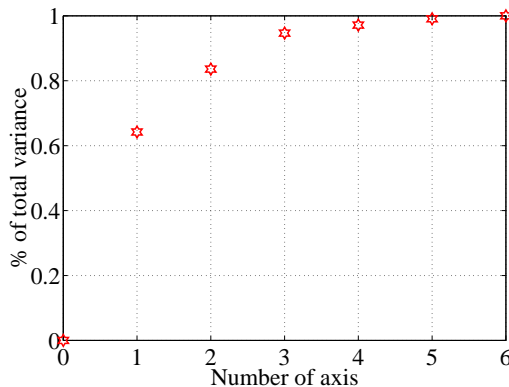

Fig. 3 Total variance explained with respect to the number of reactions for the production of lipase from olive oil by *Candida rugosa*.

Figure 3 represents the cumulated variance associated with the number of considered inertia axis. For instance, we can see that two reactions are sufficient to explain 82% of the observed variance. Since three reactions explain 95% of the total variance, it seems reasonable in this example to use 3 reactions for the model.

The reader is referred to [4] for an application to real data, for growth and vanillin production by cultures of the fungus *Pycnoporus cinnabarinus* in bioreactors.

3 Estimation of the pseudo-stoichiometric matrix K

Since we have a value for the number of involved reactions, we are in a position to start the estimation of the (totally or partially) unknown matrix K.

3.1 Determination of $\mathcal{I}mK$

Let us use Property 1 which states that $\mathcal{I}mK$ is spanned by the eigenvectors ρ_i associated with the non zero eigenvalues of UU^T. Now, from the experimental data collected through the matrix UU^T we get p eigenvectors ρ_i that span K. It means that each column k_i of K is a linear combination of the ρ_i. In other terms, there exists a $p \times p$ matrix G such that

$$K = \rho G$$

where the columns of matrix ρ are the eigenvectors ρ_j. In other words, the family of possible PS matrices K is parameterised by G.

Remark: In general, since the reaction rates are unknown, matrix G (and therefore matrix K) is not identifiable: this can be easily understood on a very simple example. If $r_1(\xi)$ and $r_2(\xi)$ are two reaction rates, the term $Kr(\xi)$ can be written:

$$Kr(\xi) = k_1 r_1(\xi) + k_2 r_2(\xi)$$
$$= \tfrac{k_1+k_2}{2}(r_1(\xi) + r_2(\xi)) + \tfrac{k_1-k_2}{2}(r_1(\xi) - r_2(\xi))$$

And therefore both matrices $K = [k_1 \ k_2]$ and $\tilde{K} = [\tfrac{k_1+k_2}{2} \ \tfrac{k_1-k_2}{2}]$ can produce the same result. The reaction rates associated with the second matrix are then: $\tilde{r}_1(\xi) = r_1(\xi) + r_2(\xi)$ and $\tilde{r}_2(\xi) = r_1(\xi) - r_2(\xi)$.

3.2 Additional hypotheses

In order to make matrix G (and K) uniquely identifiable, we need to introduce additional structural constraints. At this stage, all the *a priori* knowledge on the reaction network should be considered to improve the estimation process.

3.2.1 Normalisation First, we shall impose (without loss of generality) that each reaction rate is normalised with respect to one species, and therefore that each column of matrix K contains one +1 or one -1. This induces obviously additional constraints on the possible matrices G. Note that sometimes we may not know the sign of the element: the two possible cases must then be considered.

3.2.2 Physical assumptions One can impose the conservation of elementary mass balances. For example if one wants the carbon to be conserved in the model, if c_i is the carbon content of one unit of the state ξ_i, it means that we should have for each of the p reactions ($j \in \{1, \ldots, p\}$):

$$\sum_{i=1}^{n} c_i k_{ij} = 0 \qquad (5)$$

Note however that for macroscopic mass balance where the state variables represent a collection of compounds, the carbon content of the variable can be undetermined. However it can be bounded: $c_i^- \leq c_i \leq c_i^+$. Then equation (5) becomes an inequality.

An inequality can also be obtained if we assume that some of the products are not measured, for example if we have a loss of carbon through unmeasured products, we get:

$$\sum_{i=1}^{n} c_i k_{ij} \geq 0$$

3.2.3 Biological and biochemical assumptions When additional constraints are still necessary, we use biochemical assumptions.

When only a subset of the components are present in the reaction at the initial time, the production or not of new components with consumption or not of substrates is an indicator of the variables that are necessary for the reaction. It is clear for example that the first reaction will involve only the substrates which were present at the beginning of the fermentation.

We can for example deduce from this analysis that a specific component is not involved in one of the p reactions and therefore impose a zero in matrix K.

3.2.4 Other assumptions One can also try to find a matrix K involving the minimum number of components in each reaction (*i.e.* containing the maximum number of zeros). If these hypotheses are not sufficient, several matrices K can then be identified, parameterised by some parameter, and their biochemical meaning must then be assessed.

3.3 Validation

The main result provided by the previous analysis is the determination of the variables which are substrates or products in the reactions or, in other words, the obtained signs of the entries of K.

Another expected result can be the determination of the variables which are not involved in a reaction, corresponding to zero elements in the matrix K. However it is actually very unlikely that the analysis will provide estimates of the elements of K which are exactly zero. The idea consist then in replacing the very small elements by zeros, and to validate the corresponding reaction network using the techniques presented in [3,4]. These methods are based on the 5 following steps (see [4] for more details):

1. Determination of the vectors which are in the left Kernel of K, *i.e.* the vectors $\lambda \in \mathbf{R}^n$ such that:

$$\lambda^t K = 0 \qquad (6)$$

2. Determination of the associated regression, which is directly deduced by left multiplying Equation (3) by λ^t. Using Equation (6) it gives:

$$\sum \lambda_i u_i(t) = 0 \qquad (7)$$

3. Verification that the $u_i(t)$ involved in (7) are not related by any other linear relation associated to another left Kernel vector λ (soundness of λ)
4. Computation of the $u_i(t)$ from the available data and test of the significance of regression (7).
5. Test of the positivity of the PS coefficients identified in the previous step.

This validation procedure will be illustrated in the example study.

3.4 Example (continued)

3.4.1 Statement of the problem and considered data We shall now illustrate the proposed approach with the simulation study of lipase production from olive oil. From the previous study of the number of reactions, we know that 3 reactions should be considered.

We assume here that the first reaction is known, and therefore we only focus on the two other reactions. We are thus in the process of estimating the submatrix $\bar{K}$ extracted from K by removing the first line and the first column.

A set of noisy data of the state variables S_2, S_3, E, X, P, O and of the gaseous flow rates q_{O_2} and q_{CO_2} is produced by simulation as described in Section 2. The goal is to determine the 6×2 matrix $\bar{K}$ from this data set. More specifically, a question that we want to address is to determine, from the data, which of the two reactions produces the enzyme E.

$\bar{K}$	identified $\bar{K}$	identified $\bar{K}$ after validation
$\begin{pmatrix} -5 & 0 \\ 0 & -0.5 \\ 0 & 0.2 \\ 1 & 1 \\ -2 & -1 \\ 0.3 & 1.5 \end{pmatrix}$	$\begin{pmatrix} -3.54 & 0 \\ 0 & -0.51 \\ 0.01 & 0.22 \\ 1 & 1 \\ -1.34 & -0.87 \\ 0.18 & 1.51 \end{pmatrix}$	$\begin{pmatrix} -4.54 & 0 \\ 0 & -0.50 \\ 0 & 0.19 \\ 1 & 1 \\ -1.33 & -0.72 \\ 0.34 & 1.24 \end{pmatrix}$

Table 3 True coefficients of matrix $\bar{K}$ and identified values.

3.4.2 Estimation of $\bar{K}$ Now, using a moving average, we can compute the quantities U_i associated with the 6 state variables. Next we compute the matrix $M = U^T U$. The eigenvectors ρ_i associated with the two largest eigenvalues are then the basis of $\mathcal{I}m K$. Since G is a 2×2 matrix, the columns $\bar{k}_1$ and $\bar{k}_2$ of $\bar{K}$ can be written:

$$\bar{k}_1 = \alpha_{11}\rho_1 + \alpha_{12}\rho_2 \text{ and } \bar{k}_2 = \alpha_{21}\rho_1 + \alpha_{22}\rho_2 \quad (8)$$

Now we proceed in two successive steps:

i. Normalisation.
The PS coefficients associated with the biomass growth are normalised : $\bar{k}_{41} = 1$ and $\bar{k}_{42} = 1$. We get then:

$$\begin{aligned} \bar{k}_{41} = 1 = \alpha_{11}\rho_{41} + \alpha_{12}\rho_{42} \\ \bar{k}_{42} = 1 = \alpha_{21}\rho_{41} + \alpha_{22}\rho_{42} \end{aligned} \quad (9)$$

Using Equations (8) and (9) with the obtained values of ρ_1 and ρ_2, we can now write matrix $\bar{K}$ parametrised by α_{11} and α_{22} as follows:

$$\bar{K} = \begin{pmatrix} -1.42\alpha_{11} - 2.65 & -1.2\alpha_{22} + 1.12 \\ 0.2\alpha_{11} - 0.13 & 0.17\alpha_{22} - 0.67 \\ -0.08\alpha_{11} + 0.062 & -0.071\alpha_{22} + 0.28 \\ 1 & 1 \\ -0.19\alpha_{11} - 1.2 & -0.16\alpha_{22} - 0.72 \\ -0.53\alpha_{11} + 0.51 & -0.45\alpha_{22} + 1.93 \end{pmatrix}$$

ii. Biological hypotheses.
Now to determine uniquely matrix $\bar{K}$ two additional assumptions must be introduced.

Hypothesis: *A reaction still takes place when only S_2 [resp. S_3] is present at the initial time, and no S_3 [resp. S_2] is produced.*

In other words this means that S_2 is the only substrate of one reaction and that S_3 is the only substrate of the other one. Thus we will impose $\bar{k}_{12} = 0$ and $\bar{k}_{21} = 0$.

These additional constraints allows us to compute α_{11} (0.621) and α_{22} (0.93).

Finally we end up with an estimate of matrix $\bar{K}$ (see Table 3). It is worth noting that the identified matrix $\bar{K}$ is close to the true one. The value of the (theoretically zero) coefficient $\bar{k}_{13}$ is 0.01 which can be neglected with respect to the other coefficients of $\bar{K}$. Hence, the

unknown part of the structure of matrix $\bar{K}$ has been recognised. Moreover the estimates of the non-zero entries of the matrix $\bar{K}$ are quite accurate.

3.4.3 Validation Here we will validate the identified structure for K with respect to the available data. As it was shown in the previous step, the following structure for matrix K has been identified:

$$\bar{K} = \begin{pmatrix} -\bar{k}_{11} & 0 \\ 0 & -\bar{k}_{22} \\ 0 & \bar{k}_{32} \\ 1 & 1 \\ -\bar{k}_{51} & -\bar{k}_{52} \\ \bar{k}_{61} & \bar{k}_{62} \end{pmatrix}$$

Now the kernel of K^T is spanned by the following 4 vectors:

$$\bar{\lambda}^1 = \begin{pmatrix} 0 \\ \frac{\bar{k}_{32}}{\bar{k}_{22}} \\ 1 \\ 0 \\ 0 \\ 0 \end{pmatrix}, \quad \bar{\lambda}^2 = \begin{pmatrix} \frac{\bar{k}_{52}-\bar{k}_{51}}{\bar{k}_{11}} \\ 0 \\ 0 \\ \bar{k}_{52} \\ 1 \\ 0 \end{pmatrix},$$

$$\bar{\lambda}^3 = \begin{pmatrix} -\frac{\bar{k}_{32}}{\bar{k}_{11}} \\ 0 \\ 1 \\ -\bar{k}_{32} \\ 0 \\ 0 \end{pmatrix}, \quad \bar{\lambda}^4 = \begin{pmatrix} \frac{\bar{k}_{61}-\bar{k}_{62}}{\bar{k}_{11}} \\ 0 \\ 0 \\ -\bar{k}_{62} \\ 0 \\ 1 \end{pmatrix}$$

The associated regressions are the following:

$$\mathcal{R}_1 : \frac{\bar{k}_{32}}{\bar{k}_{22}} u_3(t) + u_4(t) = 0$$

$$\mathcal{R}_2 : \frac{\bar{k}_{52}-\bar{k}_{51}}{\bar{k}_{11}} u_2(t) + \bar{k}_{52} u_5(t) + u_6(t) = 0$$

$$\mathcal{R}_3 : -\frac{\bar{k}_{32}}{\bar{k}_{11}} u_2(t) + u_4(t) - \bar{k}_{32} u_5(t) = 0$$

$$\mathcal{R}_4 : \frac{\bar{k}_{61}-\bar{k}_{62}}{\bar{k}_{11}} u_2(t) - \bar{k}_{62} u_5(t) + u_7(t) = 0$$

(10)

Note that these regressions are sound [4] in the sense that they do not involve a set of components that are related together by another linear relationship.

The numerical results obtained from the considered regressions are presented in Table 4. It results that all the regressions (10) are highly significant, showing that the estimated reaction network is validated.

Moreover, the following quantities are estimated in Table 4:

$$\{ \frac{\bar{k}_{32}}{\bar{k}_{22}}, \frac{\bar{k}_{52} - \bar{k}_{51}}{\bar{k}_{11}}, \bar{k}_{52}, \frac{\bar{k}_{32}}{\bar{k}_{11}}, \bar{k}_{32}, \frac{\bar{k}_{61} - \bar{k}_{62}}{\bar{k}_{11}}, \bar{k}_{62} \}$$

It is easy to compute the values of $\bar{k}_{11}$ to $\bar{k}_{62}$ from this set, leading to the estimate of matrix $\bar{K}$ proposed

in Table 3. The final step consists in verifying that the estimates of the PS coefficients are all positive. This concludes the validation procedure.

	Significance	Unknown	Value	Interval
$\mathcal{R}_1$	YES	$\frac{k_{32}}{\bar{k}_{22}}$	2.36	[2.06 2.66]
$\mathcal{R}_2$	YES	$\frac{k_{52}-k_{51}}{\bar{k}_{11}}$	-0.14	[-0.18 0.09]
		$\bar{k}_{52}$	0.72	[0.66 0.77]
$\mathcal{R}_3$	YES	$\frac{k_{32}}{\bar{k}_{11}}$	-0.04	[-0.05 -0.03]
		$-\bar{k}_{32}$	-0.2	[-0.21 -0.18]
$\mathcal{R}_4$	YES	$\frac{k_{61}-k_{62}}{\bar{k}_{11}}$	-0.35	[-0.42 -0.29]
		$-\bar{k}_{62}$	-1.25	[-1.33 -1.16]

Table 4 Significance (threshold 5%) of the regressions (10) and parameter values.

4 Conclusion

Determining a macroscopic reaction network for a bioprocesses is a difficult issue mainly because of the complexity inherent to biological systems. This problem is fundamentally ill stated since the Pseudo-stoichiometric matrix K is generally not identifiable from a data set. We show in this paper how to identify the space generated by the columns of K and how to add constraints in order to determine a unique (or a set of) matrix K.

Through the studied example we have demonstrated that the proposed method can accurately estimate the values of the PS coefficients in spite of noises due to measurements and low sampling frequency.

It is worth noting that this approach does not necessarily require the availability of all the state variables ξ_i measurements. Of course, if the measurement of the ith biochemical component ξ_i is not available the ith line of matrix K cannot be determined by the method.

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