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Philippe de Larminat

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**IRIA**

CENTRE DE RENNES

**IRISA**

Institut National  
de Recherche  
en Informatique  
et en Automatique

Domaine de Voluceau  
Rocquencourt

BP 105

78153 Le Chesnay Cedex

France

Tél. (1) 39 63 55 11

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**ROBUST STABILITY  
OF EXPLICIT  
ADAPTIVE CONTROL  
WITHOUT  
PERSISTENT EXCITATION**

Philippe DE LARMINAT

Novembre 1986

**ROBUST STABILITY OF EXPLICIT ADAPTIVE CONTROL  
WITHOUT PERSISTENT EXCITATION**

Philippe DE LARMINAT

Professeur INSA  
IRISA - Campus de Beaulieu - 35042 Rennes Cédex  
et GRECO-CNRS "Systèmes Adaptatifs"

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**Abstract.-** This paper deals with adaptive control, based on explicit identification. The problem of the identified model stabilizability is solved in the passive approach, i.e. without requiring persistently exciting inputs. This solution is robust, covering time varying processes, unstructured model errors and underestimated model order.

**Key words.-** Adaptive control, Robustness, Indirect, Passive

**STABILITE ROBUSTE DE LA COMMANDE ADAPTATIVE EXPLICITE  
SANS EXCITATION PERSISTANTE**

**Résumé.-** Ce papier concerne la commande adaptative basée sur une identification explicite. Le problème de la stabilisabilité du modèle identifié est résolu dans l'approche passive, c'est à dire sans nécessiter des entrées continuellement excitantes. La solution est robuste, dans le contexte de processus variable dans le temps, avec erreurs de modèle non structurées et ordre sous estimé.

**Mots clés :** Commande adaptative, Robustesse, Indirecte, Passive

## INTRODUCTION

According to the certainly equivalence principle [1], the most natural approach for adaptive control associates some real time identification method, and continuous updating the control law from the identified model.

Before 1980, almost everybody thought that this approach could not lead to any complete theoretical analysis, in a somewhat general framework.

That is the reason why, between 1970 and 1980 most of the theoretical works concerned the "direct approach", i.e. direct adjustment without explicit identification (see e.g. [2] to [6]), in spite of major limitations, such as minimum phase hypothesis.

In the early eighties it was recognized that the stability conditions in indirect approach could be formulated in a very general and fruitful form [7,8]. Typically, these conditions are the following :

*i) the identified model must satisfy some smallness conditions concerning :*

- *the equation error  $v(t)$ , which appears in the process equations, when written with the identified  $\hat{\theta}(t)$ , and the observed input output signals,*
- *the evolution rate of  $\hat{\theta}(t)$ .*

*ii) the identified model must be stabilizable, for the adjustment algorithm may lead to a control parameter vector  $k(\hat{\theta})$ , such that the closed loop characteristic polynomial involved by  $\hat{\theta}(t)$  and  $k(\hat{\theta})$  be strictly Hurwitz.*

These conditions do not restrict the choice of control algorithm. Then the adaptive control problem begins to be widely recognized as a pure identification problem.

In fact, most of the classical identification methods, based on the Prediction Error Method [9], directly satisfy the first above condition (i).

Unfortunately these methods do not present any special properties concerning the above stabilizability condition (ii). In order to solve this key problem, the so called active approach states that the process must be persistently excited, either by means of the reference input, either by additive extra signals. Then, the convergence of  $\hat{\theta}(t)$  towards a vicinity of the exact (and stabilizable) parameters  $\theta^*(t)$  solves the problem [10].

However, artificial exciting inputs are generally nocuous for the control purpose itself, especially in the regulation mode.

An other solution lies in some projection techniques of  $\hat{\theta}(t)$  in an a priori given stabilizable (or admissible) domain  $D_A$ . This approach holds only if  $D_A$  is simply connected and convex, which is a very restrictive assumption.

A first general solution to the stabilizability problem was proposed by de Larminat [11]. It is based on the use of two models :

- a model  $\hat{\theta}(t)$ , delivered by an ordinary least square algorithm,
- a model  $\bar{\theta}(t)$ , constrained to be stabilizable, and then usable for control.

When  $\hat{\theta}(t)$  escapes from the admissible domain  $D_A$ , it is reinitialized into the intersection of  $D_A$  with an ellipsoid centered on  $\hat{\theta}(t)$ , defined by  $\|\bar{\theta} - \hat{\theta}\|_P^{-1} < 1$ , where  $P(t)$  is the classical L.S. matrix.

Althouth this algorithm was designed having in mind the noisy case, the complete proof of satisfying (i) and (ii) was performed in [11] only in the noise-free case, and one could fear it did not present any robustness property with respect to noise. The same criticism could be objected to a similar work of Lozano and Goodwin [12].

In [13], de Larminat presented a solution based on the same principles, including a robustness analysis, with regard not only to noise, but also to unstructured model errors (non linearities, underestimated model order), and even to time varying processes.

The present work consists in a reviewed and completed version of [13], then, it offers a very complete solution to the indirect passive approach in adaptive control. This solution takes form as a typical example of an identification algorithm, satisfying the above conditions (i) and (ii). In addition, a theorem of robust stability for time varying systems plays the role of a technical lemma, for the stability analysis of adaptive control systems. This theorem is widely derived from a previous work of Praly [14].

For simplicity, only one identification algorithm is presented. Though a general class is not explicitly given, its basic features are the following :

- the algorithm belongs to the Least-Square type, involving a significant matrix  $P$ , which is necessary for the stabilizability correction below. It means that scalar gains must be discarded,
- the classical forgetting is introduced, for time varying process identification,
- the prediction error is normalized by the norm of the observation vector,
- an attraction towards zero permits to keep  $\hat{\theta}$  and  $P$  bounded,
- all the previous characteristics are organized so that the pair  $(\hat{\theta}, P)$  define a certainty area around  $\hat{\theta}$ ,
- from this first algorithm, a stabilizable model  $\tilde{\theta}(t)$  is deduced : the pair  $(\hat{\theta}, P)$  is used as a permanent memory of the past input output data, in order to define a possible reinitialization for  $\hat{\theta}(t)$ , when it escapes the admissible domain  $D_A$ .

The general principles above are quite reasonable and their application is relatively simple. However, it was not straightforward that they could lead to a proof of overall stability for adaptive control systems. For simplicity, this paper deals with the continuous time case, for which complete proofs are provided.

In section 2, the hypotheses and notations are introduced, for the control of monovariate, continuous time, n-order processes. The concept of admissible domain  $D_A$  is also defined. Section 3 is devoted to a theorem of robust stability, particularly suitable for adaptive control analysis. This theorem formalizes that a process  $\{\dot{x} = F(t)x(t)+w(t)\}$  is stable if there exist convenient upper bounds for  $\|w(t)\|$  and  $\|\dot{F}(t)\|$ . In section 4, the primary identification algorithm is described and it is shown (section 5) that the robustness theorem applies, assuming that  $\hat{\theta}(t)$  remains uniformly stabilizable.

The heart of the paper relies in section 6, where the admissible model  $\bar{\theta}(t)$  is introduced : It is shown that  $\bar{\theta}(t)$  simultaneously satisfies the required conditions (i) and (ii). The key problem was to exhibit a convenient upperbound for the number of possible reinitialisation of  $\bar{\theta}(t)$ , in a given interval of time. The main conclusions are provided in section 7. The appendix describes the proof of the robust stability theorem.

## 2. PROCESS AND CONTROL LAW : NOTATIONS, EQUATIONS AND HYPOTHESES

First consider a deterministic, time invariant process, input  $u(t)$ , output  $y(t)$ , which is equivalently described by the following equations (2-1) to (2.3) :

$$\frac{d^n u}{dt^n} + a_1 \frac{d^{n-1} y}{dt^{n-1}} + \dots + a_{n-1} \frac{dy}{dt} + a_n y = b_1 \frac{d^{n-1} u}{dt^{n-1}} + \dots + b_{n-1} \frac{du}{dt} + b_n u \quad (2.1)$$

$$A(s)y = B(s)u \quad (2.2)$$

$$z(t) = \phi(t)^T \theta \quad (2.3)$$

where :

s is the differentiation operator

$$A(s) \triangleq s^n + a_1 s^{n-1} + \dots + a_n \quad (2.4)$$

$$B(s) \triangleq b_1 s^{n-1} + \dots + b_n \quad (2.5)$$

$$z(t) \triangleq \frac{d^n y}{dt^n} \quad (2.6)$$

$$\phi^T(t) \triangleq \left[ \begin{array}{c|ccc} \frac{d^{n-1} y}{dt^{n-1}} & \dots & \frac{dy}{dt} & y \\ \hline \frac{d^{n-1} u}{dt^{n-1}} & \dots & \frac{du}{dt} & u \end{array} \right] \quad (2.7)$$

$$\theta^T \triangleq \left[ \begin{array}{c|ccc} -a_1 & \dots & -a_{n-1} & -a_n \\ \hline b_1 & b_{n-1} & b_n & \end{array} \right] \quad (2.8)$$

A time-invariant control law is defined :

$$\frac{d^n u}{dt^n} = k^T \phi(t) + k_r y_r(t) \quad (2.9)$$

where :  $y_r$  is the reference signal,

$k_r$  a scalar gain,

$$k^T \triangleq - \left[ \begin{array}{c|ccc} q_1 & \dots & q_n & \\ \hline p_1 & \dots & p_n & \end{array} \right] \quad (2.10)$$

Then, the control law can be written as

$$P(s) u = - Q(s)y + k_r y_r \quad (2.11)$$

Nota : The feedback transfer  $Q(s)/P(s)$  is strictly proper (i.e.  $q_0 = 0$  in  $Q(s)$ ), which yields more simplicity without appreciable loss of generality. Similarly, one can introduce a polynomial  $K_r(s)$  instead of  $k_r(s)$ . Moreover, the orders of A, B, C, D could be lower than n.



The closed loop equations are written :

\*either into the polynomial form :

$$(AP + BQ) y = B k_r y_r \quad (2.12)$$

$$(AP + BQ) u = A k_r y_r \quad (2.13)$$

\*either into the state form :

$$\dot{\phi} = F\phi + w \quad (2.14)$$

where :

$$F \triangleq \begin{bmatrix} & & & \theta^T & & \\ & 1 & & & & \\ & & \ddots & & & \\ & & & 1 & & \\ & & & & 0 & \\ & & & & & 0 \\ & & & & & & k^T \\ & & & & & & & 1 \\ & & & & & & & & \ddots \\ & & & & & & & & & 1 \\ & & & & & & & & & & 0 \end{bmatrix}, \quad w \triangleq \begin{bmatrix} \vdots \\ 0 \\ \vdots \\ k_r \\ y_r \\ \vdots \\ 0 \\ \vdots \end{bmatrix} \quad (2.15)$$

In order to satisfy the required performances,  $k$  and  $k_r$  are adjusted to  $\theta$ , according to an application  $\mathcal{H}$  :

$$\begin{array}{ccc} \mathbb{R}^{2n} & \xrightarrow{\mathcal{H}} & \mathbb{R}^{2n+1} \\ \theta & \longmapsto & \begin{bmatrix} k \\ k_r \end{bmatrix} \end{array}$$

This adjustment law  $\mathcal{A}$  must at least satisfy :

•  $[A(s)P(s) + B(s)Q(s)]$  be an Hurwitz polynomial (2.16)  
(for stability)

•  $a_n p_n + b_n q_n = b_n k_r$  (2.17)  
(for zero static error)

All the classical control methods for linear systems lead to adjustment laws which satisfy at least (2.16).

However, according to the control method, then it exists some constraints on  $\theta$ , for example :

- $A(s)$  and  $B(s)$  must be coprime, when using all-pole placement,
- In addition,  $B(s)$  must be Hurwitz (minimum phase condition) for pole and zero placement, or perfect model following, or minimum output variance,
- For any method : if  $A(s)$  and  $B(s)$  are not coprime, their common factor must be Hurwitz. This necessary stabilizability condition is also sufficient for various methods, such as Linear Quadratic optimization,
- In order to satisfy (2.17),  $b_n$  must be non zero.

It follows that, for a given control method,  $\theta$  must belong to a specified subset of the parametric space, i.e. an Admissible Domain :  $D_A \subset \mathbb{R}^{2n}$ . For many adjustment laws  $\mathcal{A}$ ,  $D_A$  do not reduce to the stabilizable domain, but is strictly included in it.

In order to deal with concrete adaptive control problems, introduce a set of properties, defining the admissible domains.

Let  $\mathcal{K}$  an adjustment law, which yields  $k = k(\theta)$ , and thus  $F = F(\theta)$  (from 2.15). A subspace  $D_A$  is said to be admissible with respect to  $\mathcal{K}$  if there exists some positive constants  $\Omega_F$ ,  $\omega_F$ ,  $M_R$  and  $M_D$  such that, for any  $\theta \in D_A$ , the following  $P_F$ ,  $P_R$  and  $P_D$  properties hold :

$$P_F : \begin{cases} \|F(\theta)\| \leq \Omega_F & (2.18) \\ \operatorname{Re}(\lambda_i(\theta)) \leq -\omega_F < 0 & (2.19) \end{cases}$$

( $\lambda_1 \lambda_2 \dots \lambda_{2n}$  : Eigenvalues of  $F(\theta)$ )

$$P_R : |k_r| \leq M_R \quad (2.20)$$

$$P_D : \forall \theta_1, \theta_2 \in D_A : \frac{\|F(\theta_1) - F(\theta_2)\|}{\|\theta_1 - \theta_2\|} \leq M_D \quad (2.21)$$

Comments :

- \* (2.18) is a simple boundedness condition
- \* (2.19) involves the asymptotic stability of  $F$ .

It could be added more restrictive conditions (pole damping or others) but (2.19) is the strict minimum to be required.

- \* (2.20) will be associated with a boundedness hypothesis on  $y_r$ .
- \* Finally, the continuity condition  $P_D$  will be necessary when analysing adaptive control systems, where  $\theta$  (or  $\hat{\theta}$ ) becomes time-varying.



Now, it is proposed to define  $D_A$  as follows

$$\theta \in D_A \iff \begin{cases} \|\theta\| \leq R_\theta & (2.26) \\ \|k(\theta)\| \leq R_k & (2.27) \\ \|k_r(\theta)\| \leq M_r & (2.28) \end{cases}$$

where  $R_\theta, R_k, M_r$  are a priori given constants.

It is clear that  $D_A$  is an admissible domain. In effect, for any  $\theta \in D_A$  :

- \* (2.26) and (2.27) imply the existence of a bound  $\Omega_F$  in (2.18)
- \* (2.22) implies (2.19)
- \* from (2.24) and (2.25), it follows that  $k(\theta)$  components are some rational fractions of  $\theta$ , which denominators are not zero for any  $\theta$  satisfying (2.26) and (2.27). Thus their derivatives are bounded for any  $\theta \in D_A$ .  $M_D$  exists in (2.21).

N.B.: In (2.18) to (2.21), only the existence of the bounds  $\Omega_F, \omega_F, M_r, M_D$  is required. In the example above,

- \*  $M_r$  is directly given
- \*  $\Omega_F$  can be deduced from the given  $R_\theta$  and  $R_k$
- \*  $M_D$  will be more difficult to deduce from  $D(s), R_\theta$  and  $R_k$
- \* moreover, the exact shape of  $D_A$  is practically impossible to deduce. It is not convex, neither simply connected since the constraint (from 2.25, 2.28)

$$|b_n| \geq \frac{d_{2n}}{M_r} \quad (2.29)$$

at least divides it into two disconnected subspaces.

However the knowledge of the shape of  $D_A$  will not be necessary in the sequel. Similarly, the knowledge of the bounds  $\Omega_F$ ,  $\omega_F$ ,  $M_r$ ,  $M_D$  could be useful in order to quantify the robustness of the given control law  $\mathcal{A}$ , but is not necessary for proving the existence of this robustness.

Finally, it will be necessary to introduce a strongly admissible domain  $D_{SA}$ , based on the following assumptions :

- \*  $D_{SA}$  is strictly included into  $D_A$
- \* the distance  $\delta$  between  $\overline{D_A}$  and  $D_{SA}$  is non zero :

$$\delta \triangleq \text{Min} \quad \|\theta_1 - \theta_2\| > 0 \quad (2.30)$$

$$\theta_1 \in D_A$$

$$\theta_2 \in \overline{D_A}$$

In the case of pole placement,  $D_{SA}$  will be similarly defined, from some  $R'_\theta$ ,  $R'_k$ ,  $M'_r$  :

$$R'_\theta < R_\theta, R'_k < R_k, M'_r < M_r$$

The existence (not the knowledge) of  $\delta$  is straightforward, knowing that  $k(\theta)$  is bounded and differentiable when  $\theta \in D_A$ .

From the above example, it is clear that most of the reasonable control methods could exhibit similar properties : the admissible domain will be preferably defined from some thresholds occurring in the implementation of the method. It is obviously easier to determine the admissibility of  $\theta$  from the norm of  $k(\theta)$ , than from a direct measure (if exists !) of the coprimeness of  $A(s)$  and  $B(s)$ .

In addition,  $D_A$  will depend also from the a priori knowledge of the considered class of process.

In some very specific problems,  $D_A$  could be defined as a local vicinity of an a priori given model. Then, the convexity hypothesis could hold, but that will not be assumed in the sequel.

### 3. A THEOREM OF ROBUST STABILITY FOR SLOWLY TIME VARYING SYSTEMS

Reconsider now the state equation

$$\dot{x} = F(x) + w$$

in which  $F$  and  $w$  do not necessarily exhibit the structure defined in eq. (2.15).

Now,  $F(t)$  will be a function of time, and  $w(t)$  will include possible model errors.

More precisely, it means that,  $x(t)$  being some function of time,  $F(t)$  being some given model, either a priori given, either an identified one, then  $w$  is now defined as the difference :  $w \triangleq \dot{x} - Fx$ .

It is clear now that even if  $\{R_e(\lambda_i(t)) \leq -\omega_F\}$  for every  $t$ , the stability is no longer assumed, unless  $\|F\|$  and  $\|w\|$  be "relatively small". Various upperbounds could be proposed for  $\|F\|$  and  $\|w\|$ . In this section, such upperbounds will be selected, for their further interest when dealing with robust stability in adaptive control.

**Theorem 1**

Let  $x(t)$ ,  $w(t)$ ,  $F(t)$  be some functions of time ( $\dim. (n_F \times 1)$ ,  $(n_F \times 1)$ , and  $(n_F \times n_F)$ ). Assume that the following properties hold for every  $t$ ,  $\tau$  and  $T > 0$  :

$$\frac{dx}{dt} = F(t) x(t) + w(t) \quad (3.1)$$

$$\|x(0)\| \text{ is finite.} \quad (3.2)$$

There exist  $\omega_F$  and  $\Omega_F$ , positive constants, such that :

$$R_e \{ \lambda_i(t) \} \leq -\omega_F < 0 \quad (i = 1, 2, \dots, n_F) \quad (3.3)$$

$$\|F(t)\| \leq \Omega_F < \infty \quad (3.4)$$

Assume also that :

$$\int_t^{t+T} \frac{\|\dot{F}(\tau)\|}{k_D} d\tau \leq T + T_1 \quad (3.5)$$

$$\int_t^{t+T} \frac{\|w(\tau)\|^2}{M_w + k_x \|x(\tau)\| + k_\xi \xi(\tau)^2} d\tau \leq T + T_2 \quad (3.6)$$

where  $\xi(t)$  satisfies

$$0 \leq \xi(0) < \infty \quad (3.7)$$

$$T_\xi \dot{\xi}(t) = -\xi(t) + \|x(t)\| \quad (3.8)$$

and where

-  $T_1, T_2, M_w$  are some positive constants (possibly large)

-  $T_\xi, k_D, k_x, k_\xi$  are positive constants, which depend on  $\omega_F$  and  $\Omega_F$ .

Then :  $x(t)$  is uniformly bounded.



For  $T_\xi$ ,  $k_d$ ,  $k_x$ ,  $k_\xi$ , the following expressions are proposed :

$$T_\xi \leq T_F \quad (3.9)$$

$$k_d \leq \frac{\tau_F}{2T_F^3} \quad (3.10)$$

$$k_x \leq \frac{1}{16T_F} \sqrt{\frac{\tau_F}{T_F}}^3 \quad (3.11)$$

$$k_\xi \leq \frac{1}{16T_F} \sqrt{\frac{T_\xi}{T_F}}^3 \quad (3.12)$$

where

$$T_F \triangleq \frac{n_F^2}{2\omega_F} \left(\frac{2\Omega_F}{\omega_F}\right)^{2n_F} \quad (3.13)$$

$$\tau_F \triangleq \frac{1}{\Omega_F} \quad (3.14)$$

### Comments

The above expressions are not unique, and more efficient ones could be possibly found. Obviously, they depend on certain arbitrary choice occurring in the derivation of the proofs (see appendix). In concrete application (3.10) to (3.14) show that  $k_d$ ,  $k_x$ ,  $k_\xi$  could often be very small. That is the price to be paid for the generality of the hypotheses (3.1) to (3.8).

Under some additional constraints (damping coefficients of the complex conjugate  $\lambda_1$ , for example)  $k_d$ ,  $k_x$ ,  $k_\xi$  could be larger. However, our present interest does not lie in the robustness problem by itself, but in its application to adaptive control.

From this point of view, we prefer to base our work upon a minimal set of properties, like (3.3) and (3.4), for which :

- \* the above non zero constants  $k_d, k_x, k_\xi$  exist
- \* the robustness involved by (3.5) - (3.6) can be quantified (at least theoretically)
- \* the quantification depends only on some characteristics of  $F(t)$
- \* the general form of (3.9) to (3.13) permits to enlight some general connections between the characteristics  $(\omega_F, \Omega_F)$  and the robustness.

For example, if  $F(t)$  is the closed loop matrix (2.15), and if  $k(\theta)$  is a control based on some "large gain principle", then  $\Omega_F$  is large. The robustness dependence can be analyzed via (3.9) to (3.14).

Consider now the feature of the upperbounds (3.5) and (3.6).

Taking  $T$  large,  $k_d$  bounds the mean speed rate of  $F(t)$ . Taking  $T \rightarrow 0$ ,  $T_1$  bounds the magnitude of jumps  $F(t)$ . Then (3.5) permits continuous, but slow change in  $F(t)$ , and also large, but rare jumps.

Now, analyze how the bound (3.6) may cover unstructured model errors : Assume an exact,  $n_F$ -order, non linear model  $f^*(\cdot)$ .

$$\dot{x} = f^*(x) + w_e \tag{3.15}$$

where  $w_e$  is an exogeneous bounded input :

$$\|w_e\| \leq M_w \tag{3.16}$$

Now,  $F$  is a given model matrix. From (3.1),  $w(t)$  is defined as

$$w \triangleq w_e + f^*(x) - F x \tag{3.17}$$

If  $f^*(x)$  is weakly non linear, so that, for any  $x$  the following (3.18) inequality hold

$$\|f^*(x) - Fx\| \leq k_x \quad (3.18)$$

then (3.6) will be satisfied.

Consider now an exact model of order greater than  $n_F$ . For simplicity we reduce to the linear, deterministic case, where  $x(t)$  is assumed to be the solution of an extended state, exact model :

$$\frac{d}{dt} \begin{bmatrix} x \\ \xi \end{bmatrix} = \begin{bmatrix} F & F_{12} \\ F_{21} & F_{22} \end{bmatrix} \begin{bmatrix} x \\ \xi \end{bmatrix} \quad (3.19)$$

$$\dot{x} = Fx + w \quad (3.20)$$

where  $F$  is assumed to be the given model and  $w$  is the output of :

$$\begin{cases} \dot{\xi} = F_{22} \xi + F_{22} x \\ w = F_{12} x \end{cases} \quad (3.21a)$$

$$w = F_{12} x \quad (3.21b)$$

An other form of (3.21) is given by the convolution :

$$w(t) = H(t) * x(t) \quad (3.22)$$

where  $H(t)$  is the impulse response of the triplet  $\{F_{22}, F_{21}, F_{12}\}$

If  $F_{22}$  is exponentially stable,  $F_{12}$  or  $F_{21}$  sufficiently small, there exist  $T_\xi$  and  $k_\xi$ , such that :

$$\|H(t)\| \leq k_\xi e^{-t/T_\xi} \quad (3.23)$$

$$\text{and then} \quad \|x(t)\| \leq k_\xi \xi(t) \quad (3.24)$$

which satisfies (3.6) to (3.8)

More generally (3.6) to (3.8) permit to handle unstructured model errors, of the general form

$$w(t) = w(t, x(\tau) \mid \tau \leq t) \quad (3.25)$$

It could be thought that the simple inequality

$$\frac{\|w\|}{M_w + k_x \|x\| + k_\xi \xi} \leq 1 \quad (3.26)$$

could be sufficient for most of the robustness analysis, and (3.6) be an academic refinement.

In fact, (3.6) will be really necessary for adaptive control analysis, where  $F(t)$  results from an identified model. Then,  $w(t)$  depends on the equation error, and will satisfy an integral inequality like (3.6). Similarly, the identified  $\hat{\theta}(t)$  will satisfy an inequality like (3.5).

Finally, the above theorem will reveal itself as a basic "Technical Lemma", when analysing robust stability of indirect adaptive control systems.

#### Proof of the theorem

The proof is detailed in appendix A. It is based on a Lyapunov type approach, using the function :

$$W(t) = x^T(t) \Sigma(t) x(t) + \Gamma_\xi \xi^2(t) \quad (3.27)$$

where  $\Sigma(t)$  is the solution of the Lyapunov equation :

$$F^T(t) \Sigma(t) + \Sigma(t) F(t) + 2I = 0 \quad (3.28)$$

According to the stability theory, (3.3) and (3.5) imply the existence of upper and lower bounds :

$$\tau_F I \leq \dot{\Sigma}(t) \leq T_F I \quad (3.29)$$

The first part of the Appendix is devoted to deriving the explicit forms (3.12) and (3.13) for  $T_F$  and  $\tau_F$ .

The second part concerns the relationship between  $\dot{\Sigma}$  and  $\dot{F}$  : it is shown that

$$\|\dot{\Sigma}\| \leq T_F^2 \|\dot{F}\| \quad (3.30)$$

Then, from (3.27) to (3.30), it is proved in a third part that  $W(t)$  is bounded.

#### 4. AN IDENTIFICATION ALGORITHM ORIENTED TOWARD ADAPTIVE CONTROL

In the passive approach, the inputs are not necessarily persistently exciting. Thus, it is unrealistic to aim at tracking some "exact" model  $\theta^*(t)$ .

The only reasonable goal is to reduce the magnitude of the equation error :

$$v(t) \triangleq z(t) - \phi^T(t) \hat{\theta}(t)$$

and the speed :

$$\dot{\hat{\theta}}(t) \triangleq \frac{d\hat{\theta}(t)}{dt}$$

Both must be "relatively" small for the model to be usable.

Clearly, it will be interesting to bound  $v(t)$  and  $\dot{\hat{\theta}}(t)$  by some expressions in connection with inequalities (3.5) and (3.6), arising in the robustness theorem.

Fortunately, classical algorithms, such as continuous-time Least-Squares algorithm, directly satisfy such inequalities.

However, L.S. must be slightly modified in order to satisfy some additional requirements :

- $\hat{\theta}(t)$  must be kept bounded
- the real process may be noisy, slowly time varying, weakly non linear, and underestimated order
- the algorithm must be Least-Squares type, not only gradient type. In other words, a significant "variance covariance" matrix  $P$  must exist
- upper bound and lower bound over  $P$  must exist
- the identified model must be admissible, i.e. at least stabilizable
- in order to solve the stabilizability problem (see §5), the pair  $(\hat{\theta}(t), P(t))$  is required to define a certain domain around  $\hat{\theta}(t)$
- all that must be obtained without prejudice to inequalities over  $v(t)$  and  $\dot{\hat{\theta}}(t)$ .

In this paper, we present only, as a characteristic example, an algorithm which satisfies all the required conditions. One can imagine possible variations, although the above conditions are not straight-forward to meet together.

Define first the process to be identified, control input  $u(t)$ , output  $y(t)$ .

Assume that there exists some vector  $\theta^*(t)$ , so called "nominal" or "best model", and denote  $v(t)$  the equation error :

$$v(t) \triangleq z(t) - \phi^T(t) \theta^*(t) \quad (4.1)$$

where  $z(t)$  and  $\phi(t)$  are defined above (2.6), (2.7).

Some constants  $\sigma$ ,  $\rho$ ,  $e$ ,  $\beta$  are given, such that :

$$\frac{v(t)}{s(t)} \leq 2 \quad (4.2)$$

$$\text{where } s(t) \triangleq \sigma + r \|\phi(t)\| + \rho \psi(t) \quad (4.3)$$

$\psi(t)$  being solution of

$$\dot{\psi} = -\beta(\psi(t) - \|\phi(t)\|) \quad (0 \leq \psi(0) < \infty) \quad (4.4)$$

$\|\hat{\theta}(t)\|$  is bounded by a given  $R$  :

$$\|\theta^*\|^2 \leq R^2 \quad (4.5)$$

For further simplification the bound for  $\|\dot{\theta}^*\|$  is defined as follows : a positive  $\alpha$  is given, such that :

$$\|\dot{\theta}^*\| \leq \alpha^2 \frac{R^2 r^2}{R^2 + r^2} \quad (4.6)$$

#### Remarks

\* From (4.2), (4.3), (4.4), the process can be non linear, and underestimated order.

\* (4.5) defines an a priori, spheric domain. One can consider an ellipsoidal domain centered around any given  $\theta_N$  :

$$(\theta^* - \theta_N)^T Q (\theta^* - \theta_N) \leq R^2 \quad (4.7)$$

Where Q is non singular, factorizable into :

$$Q = S^T S \quad (4.8)$$

(4.1) can be rewritten as :

$$v(t) = |z(t) - \phi^T \theta_N| - |\phi^T S^{-1}| |S(\theta^* - \theta_N)| \quad (4.9)$$

Then replace  $z$  by  $(z - \phi^T \theta_N)$

$\phi^T$  by  $\phi^T S^{-1}$

$\theta^*$  by  $S(\theta^* - \theta_N)$

The new  $\theta^*$  satisfies now (4.5)

\* Note that the given constant  $r$  plays a role in the inequalities on  $v(t)$  and on  $\hat{\theta}^*(t)$  (cf. (4.5) and (4.6)). Thus for a linear, but time varying system,  $r$  could be zero from (4.5) but not from (4.6).

Then, from the given  $\sigma$ ,  $r$ ,  $\epsilon$ ,  $\beta$ ,  $r$ ,  $\alpha$ , the following identification algorithm is proposed :

$$\dot{\hat{\theta}}(t) = \alpha (P(t) \phi(t) \frac{v(t)}{s^2(t)} - \frac{P(t) \hat{\theta}(t) \lambda}{R^2}) \quad (4.10)$$

$$\dot{P}(t) = \alpha \left( \frac{-P(t) \phi(t) \phi(t)^T P(t)}{s^2(t)} + P(t) - \frac{P(t)^2}{R^2} \right) \quad (4.11)$$

with  $\|\hat{\theta}(0)\| \leq R \quad (4.12)$

$$P(0) = R^2 I \quad (4.13)$$

where  $v(t) \triangleq z(t) - \phi^T(t) \hat{\theta}(t) \quad (4.14)$

$s(t)$  is defined above (4.3), (4.4) ,

and where  $\lambda = 0$  if  $\|\hat{\theta}\| < R \quad (4.15)$

$$\lambda = 1 \text{ if } \|\hat{\theta}\| \leq R \quad (4.16)$$



Comments

The above algorithm could be compared with the exponentialled wheighted L.S., which are given by

$$\dot{\hat{\theta}} = P \phi v \tag{4.17}$$

$$\dot{P} = P\phi \phi^T P + \alpha P \tag{4.18}$$

The differences first concern the factor  $\alpha/s^2$  on  $P\phi v$  and  $p\phi\phi^T P$ . In connection with the hypotheses (4.2) to (4.6), this factor will permit to derive a certainty domain from the pair  $(\hat{\theta}, P)$ , and also the desired inequalities bounding  $v$  and  $\hat{\theta}$ .

Remarks that  $\alpha$  can be zero in 4.18 (no forgetting) but not in (4.10), (4.11). That will be the price of the certainty domain (4.25). On the other hand, the additional terms  $P\hat{\theta}\lambda/R^2$  and  $P^2/R^2$  work in association in order to bound  $\hat{\theta}$  and  $P$ .

The algorithm (4.10) to (4.16), under the hypotheses (4.1) to (4.6) exhibits the following properties.

Property 1 :  $P$  is bounded

$P(t) \geq \frac{R^2 r^2}{R^2 + R^2} I$	(4.19)
$P(t) \leq R^2 I$	(4.20)

Proof

Denote  $M(t) \triangleq P^{-1}(t)$  (4.21)

wich yield from (4.11) :

$$\dot{M} = \alpha \frac{\phi\phi^T}{s^2} + M - \frac{I}{R^2} \tag{4.22}$$

Let  $a$  be any constant vector, and  $U(t) \triangleq a^T M a$

$$\text{From (4.22) : } \dot{U} = \alpha \left( \frac{a^T \dot{\phi}}{s} \right)^2 - U + \|a\|^2/R$$

$$\text{From (4.3) : } \left( \frac{a^T \dot{\phi}}{s} \right)^2 \leq \frac{\|a\|^2 \|\dot{\phi}\|^2}{(\sigma + r \|\dot{\phi}\| + \rho\psi)^2} \leq \frac{\|a\|^2}{r^2}$$

$$\text{Thus : } -U + \frac{\|a\|^2}{R^2} \leq \frac{\dot{U}}{\alpha} \leq U + \frac{\|a\|^2}{R^2} + \frac{\|a\|^2}{r^2}$$

$$\text{Now : } U(0) = \frac{\|a\|^2}{R^2} \in \left[ \frac{\|a\|^2}{R^2}, \left( \frac{\|a\|^2}{R^2} + \frac{\|a\|^2}{r^2} \right) \right]$$

When  $U(t)$  rise the upper bound of the above interval,  $\dot{U}(t)$  becomes non positive. Thus  $U(t)$  cannot cross over the bound. Idem for the lower bound.

Thus, (4.19) and (4.20) are proved, via :

$$M \succcurlyeq I/R^2 \tag{4.23}$$

$$M \preccurlyeq I \left( \frac{1}{R^2} + \frac{1}{r^2} \right) \tag{4.24}$$

### Comments

Clearly, the term  $R^2/I$ , in (4.11), prevents the possible divergence of  $P$ , when using exponential forgetting.

On the other hand, if  $\phi(t)$  is not bounded,  $P$  could be infinitely small in the ordinary L.S. (4.17, 4.18). A first advantage of the normalization involved by  $r^2 \|\dot{\phi}\|^2$  in  $s^2$  (cf. 4.3) is to yield the lower bound (4.19).

Property 2 : Existence of a non trivial certainty ellipsoid :

$$\boxed{(\hat{\theta} - \theta^*)^T P^{-1} (\hat{\theta} - \theta^*) \leq 16} \quad (4.25)$$

Proof

define  $\tilde{\theta} \triangleq \hat{\theta} - \theta^*$  (4.26a)

$$V \triangleq \tilde{\theta}^T P^{-1} \tilde{\theta} \quad (4.26b)$$

by differentiation, using (4.18)

$$\dot{V} = \tilde{\theta}^T \dot{M} \tilde{\theta} + 2\tilde{\theta}^T P^{-1} (\dot{\hat{\theta}} - \dot{\theta}^*)$$

Then, from (4.22) and (4.10)

$$\begin{aligned} \frac{\dot{V}}{\alpha} &= \frac{(\tilde{\theta}^T \phi)^2}{s^2} - \tilde{\theta}^T M \tilde{\theta} + \frac{\tilde{\theta}^T \tilde{\theta}}{R^2} \\ &+ 2\tilde{\theta}^T \phi \frac{v}{s^2} - 2\lambda \tilde{\theta}^T \hat{\theta} - \frac{2\tilde{\theta}^T P^{-1} \dot{\theta}^*}{\alpha} + \left( \frac{v^2 - v^{*2}}{s^2} \right) \end{aligned}$$

Thus

$$\begin{aligned} \frac{\dot{V}}{\alpha} + \frac{v^2}{s^2} &= -V + \left( \frac{\tilde{\theta}^T \tilde{\theta}}{R^2} - 2\lambda \tilde{\theta}^T \hat{\theta} \right) + \frac{(\tilde{\theta}^T \phi)^2 + 2\tilde{\theta}^T \phi v + v^2}{s^2} \\ &- \frac{2\tilde{\theta}^T P^{-1} \dot{\theta}^*}{\alpha} \end{aligned} \quad (4.27)$$

consider that  $(\tilde{\theta}^T \phi + v) = (\hat{\theta} - \theta^*)^T \phi + (z - \phi^T \hat{\theta}) = z - \phi^T \theta^* = v$

thus

$$\frac{\dot{V}}{\alpha} + \frac{v^2}{s^2} = -V + \left( \frac{\tilde{\theta}^T \tilde{\theta}}{R^2} - 2\lambda \tilde{\theta}^T \hat{\theta} \right) + \frac{v^2}{s^2} - \frac{2\tilde{\theta}^T P^{-1} \dot{\theta}^*}{\alpha} \quad (4.28)$$

Now, consider the following terms of the second member of 4.28 :

$$\boxed{\frac{\tilde{\theta}^T \tilde{\theta}}{R^2} - 2 \lambda \tilde{\theta}^T \hat{\theta} \leq 4} \quad (4.29)$$

In effect

- if  $\|\hat{\theta}\| < R$ , then  $\lambda = 0$

Then  $\|\hat{\theta}\| \leq \|\hat{\theta}\| + \|\theta^*\| \leq 2R$ , which yields (4.29)

- If  $\|\theta\| \geq R$ , then  $\lambda = 1$  and..

$$\begin{aligned} \frac{\tilde{\theta}^T \tilde{\theta}}{R^2} - 2 \lambda \tilde{\theta}^T \hat{\theta} &= \frac{1}{R^2} [\tilde{\theta}^T \tilde{\theta} - 2\tilde{\theta}^T \hat{\theta} + \hat{\theta}^T \hat{\theta} - \hat{\theta}^T \hat{\theta}] \\ &= \frac{1}{R^2} \theta^{*T} \theta^* - \frac{1}{R^2} \hat{\theta}^T \hat{\theta} \\ &\leq \frac{1}{R^2} \theta^{*T} \theta^* \\ &\leq 1, \text{ which yields again (4.29)} \quad \square \end{aligned}$$

(ii) from hypothesis (4.2)  $\boxed{\frac{V^2}{S} \leq 4}$  (4.30) □

(iii)  $\boxed{2 \frac{|\tilde{\theta}^T P^{-1} \dot{\theta}^*|}{\alpha} \leq 2 \sqrt{V}}$  (4.31)

In effect, from the Schwartz inequality :

$$|\tilde{\theta}^T P^{-1} \dot{\theta}^*| \leq \sqrt{\tilde{\theta}^T P^{-1} \tilde{\theta}} \sqrt{\dot{\theta}^{*T} P^{-1} \dot{\theta}^*}$$

Then, using (4.26b), (4.24), and (4.6) :

$$|\hat{\theta}^T P^{-1} \dot{\theta}^*| \leq \sqrt{V} \sqrt{\|\dot{\theta}^*\|^2 \frac{R^2 + r^2}{R^2 r^2}} \leq \alpha \sqrt{V} \quad \square$$

By substitution of (4.29), (4.20) and (4.31) into (4.28)

$$\frac{\dot{V}}{\alpha} + \frac{V^2}{s^2} \leq -V + 4 + 4 + 2\sqrt{V} \quad (4.32)$$

which yield

$$\frac{\dot{V}}{\alpha} \leq -(V - 2\sqrt{V} - 8) = -(\sqrt{V} - 4)(\sqrt{V} + 2) \quad (4.33)$$

Thus  $\dot{V}$  becomes negative for  $\sqrt{V} > 4$ . Knowing that  $0 < V(0) < 16$ , it follows that  $V$  is always lower than 16.

#### Comments

(4.25) defines a continuity domain arround  $\hat{\theta}$ , which is not trivial, In other related works, similar equality arises, such as

$$\hat{\theta}^T P^{-1} \tilde{\theta} \leq V_M$$

Where  $V_M$  is deduced from the upper bounds of  $\|\theta^*\|$ ,  $\|\hat{\theta}\|$ , and  $P^{-1}$ , so that the above certainty domain be trivial, including the given a priori domain  $\|\theta^*\| < R^2$  !

In our case,  $V_M$  is independant of all the other parameters ( $V_M = 16$ ), and the lower bound of  $P$  may be very small, if  $r^2 \ll R^2$ . Thus if  $P$  becomes small, the certainty domain may be reduced to a very little subspace of a priori domain.

Property 3 :  $\hat{\theta}$  is bounded by

$$\boxed{\|\hat{\theta}\| \leq 5R} \quad (4.34)$$

In effect, from (4.25), where  $P \leq R^2 I$ , it follows  $\|\hat{\theta} - \theta^*\| \leq 4R$  and from  $\|\theta^*\| \leq R$ , it yields (4.34)

Property 4 : an inequality for  $v$ .

For any positive  $t$  and  $T$

$$\boxed{\int_t^{t+T} \frac{v^2}{s^2} d\tau \leq 16 \left( T + \frac{1}{\alpha} \right)} \quad (4.35)$$

**Proof**

Recall (4.32), in which  $\sqrt{V} \leq 4$ , it yields

$$\frac{\dot{V}}{\alpha} + \frac{v^2}{s^2} \leq 16$$

Then, by integration :

$$\frac{V(t+T) - V(t)}{\alpha} + \int_t^{t+T} \frac{v^2}{s^2} d\tau \leq 16T$$

which yields (4.35), using  $0 \leq V(t)$  and  $V(t+T) \leq 16$

Property 5 : an inequality for  $\dot{\hat{\theta}}(t)$

For any positive  $t$  and  $T$

$$\boxed{\int_t^{t+T} \|\dot{\hat{\theta}}\| d\tau \leq 16 \sqrt{n} R \alpha \left( T + 1/\alpha \right)} \quad (4.36)$$

Proof

$$\text{From (4.10) } \|\dot{\hat{\theta}}\| \leq \left\| \frac{\alpha P \phi v}{s^2} \right\| + \left\| \frac{\alpha P \dot{\hat{\theta}}}{R^2} \right\| \quad (4.37)$$

where  $\|P\| \leq R^2$ ,  $\|\hat{\theta}\| \leq 5R$

Thus

$$\int_t^{t+T} \|\dot{\hat{\theta}}\| d\tau \leq \int_t^{t+T} \left\| \frac{\alpha P \phi v}{s^2} \right\| d\tau + \int_t^{t+T} 5R\alpha d\tau \quad (4.38)$$

Consider the term  $\left\| \frac{\alpha P \phi v}{s^2} \right\| = \left\| \frac{\alpha P \phi}{s} \right\| \left| \frac{v}{s} \right|$

Applying the Schwartz inequality

$$\left\{ \int_t^{t+T} \left\| \frac{\alpha P \phi}{s} \right\| \left| \frac{v}{s} \right| d\tau \right\}^2 \leq \int_t^{t+T} \left\| \frac{\alpha P \phi}{s} \right\|^2 d\tau \int_t^{t+T} \left| \frac{v}{s} \right|^2 d\tau \quad (4.39)$$

On the other hand

$$\begin{aligned} \left\| \frac{P \phi}{s} \right\|^2 &= \text{Tr} \left( \frac{P \phi \phi^T P}{s^2} \right) = \text{Tr} \left( P - \frac{P^2}{R^2} - \frac{\dot{P}}{\alpha} \right) \quad (\text{from 4.11}) \\ &\leq \text{Tr} \left( R^2 I - \frac{\dot{P}}{\alpha} \right) \end{aligned}$$

Thus

$$\int_t^{t+T} \left\| \frac{P \phi}{s} \right\|^2 d\tau \leq \text{Tr} (R^2 I) T + \frac{\text{Tr}[P(t)] - \text{Tr}[P(t+T)]}{\alpha}$$

$$\leq \text{Tr} (R^2 I) T + \frac{\text{Tr}(R^2 I)}{\alpha} = \text{Tr} (I) R^2 \left( T + \frac{1}{\alpha} \right)$$

I being the 2n-unit matrix :  $\text{Tr}(I) = 2n$

Thus

$$\int_t^{t+T} \left\| \frac{P \phi}{s} \right\|^2 d\tau \leq 2n R^2 \left( T + \frac{1}{\alpha} \right) \quad (4.40)$$

Then substitute (4.35) and (4.40) into (4.39)

$$\int_t^{t+T} \left\| \frac{\alpha P \psi v}{s^2} \right\|^2 d\tau \leq 32n \alpha^2 R^2 \left( T + \frac{1}{\alpha} \right)^2 \quad (4.41)$$

Using (4.38) :

$$\int_t^{t+T} \left\| \dot{\hat{\theta}} \right\|^2 d\tau \leq \sqrt{32n} \alpha R \left( T + \frac{1}{\alpha} \right) + 5 \alpha R T$$

$$\leq (\sqrt{32n} + 5) \alpha R T + \sqrt{32n} R \quad (4.42)$$

$$\leq (\sqrt{32n} + 5) \alpha R \left( T + \frac{1}{\alpha} \right)$$

knowing that

$$\sqrt{32n} + 5 \leq (\sqrt{32} + 5) \sqrt{n} < 16 \sqrt{n}, \quad (\text{because } n \geq 1)$$

thus (4.36) is proved.



**5. ROBUST STABILITY OF AN ADAPTIVE CONTROL, ASSUMING THE STABILIZABILITY OF THE IDENTIFIED MODEL**

The robust stability results from the following theorem.

**THEOREME 2**

Let  $\mathcal{P}$  a process, parameters  $\theta^*(t)$  satisfying (4.1) to (4.6).

Let  $\hat{\theta}(t)$  the identified parameters, identified by (4.10) to (4.15).

Assume (asa temporary extra-hypothesis), that  $\hat{\theta}(t)$  is admissible, for every  $t$ , with respect to the given adjustment law  $\mathcal{A}$ , the admissible domain beeing defined by (2.18) to (2.21).

Then the closed loop system is uniformly stable if :

$$\alpha > 0 \tag{5.1}$$

$$16 \sqrt{n} R \alpha \leq k_d / M_d \tag{5.2}$$

$$4 \sqrt{2} r \leq k_x \tag{5.3}$$

$$4 \sqrt{2} \rho \leq k_\xi \tag{5.4}$$

$$1/B \leq T_F \tag{5.5}$$

where  $T_F, k_x, k_\xi, k_d$  are defined in (3.9) to (3.13).

**Proof**

Let :

$$x \stackrel{\Delta}{=} \phi, \quad F \stackrel{\Delta}{=} \begin{bmatrix} \hat{\theta}^T(t) \\ \vdots \\ k^T(\theta) \\ \vdots \\ 0 \end{bmatrix}, \quad w \stackrel{\Delta}{=} \begin{bmatrix} v \\ \vdots \\ k_r(\theta) y_r \\ \vdots \\ 0 \end{bmatrix}$$

Then :

- $x, F$  and  $w$  satisfy (3.1)
- assuming  $\|\phi(0)\|$  finite yields (3.2)
- $\hat{\theta}(t)$  being admissible, (2.18) and (2.19) yields (3.3) and (3.4)
- note  $\xi \stackrel{\Delta}{=} \psi$ , define  $T_\xi = 1/\beta$ , then (3.7) and (3.8) are satisfied

From (2.21),  $\hat{\theta}$  being admissible :

$$\|\dot{F}\| \leq M_D \|\dot{\hat{\theta}}\| \quad (5.7)$$

Then, (3.35) becomes

$$\int_t^{t+T} \frac{\|\dot{F}\|}{k_d} d\tau \leq \frac{M_D}{k_D} \int_t^{t+T} \|\dot{\hat{\theta}}\| d\tau$$

From (3.36)

$$\int_t^{t+T} \frac{\|\dot{F}\|}{k_d} d\tau \leq \frac{M_D}{k_D} 16 \sqrt{n} \alpha R \left(T + \frac{1}{\alpha}\right)$$

From (5.2), it yields now (3.5) with  $T_1 = 1/\alpha$ , which is finite from (5.1).

From definitions (5.6), it follows

$$\frac{\|w\|^2}{(M_w + k_x \|x\| + k_\xi \xi)^2} = \frac{v^2 + k_r^2 y_r^2}{(M_w + k_x \|\phi\| + k_\xi \psi)^2}$$

using (5.3) and (5.4)

$$\frac{\|w\|^2}{(M_w + k_x \|x\| + k_\xi \xi)^2} \leq \frac{v^2 + k_r^2 y_r^2}{(M_w + 4\sqrt{2} r \|\psi\| + 4\sqrt{2} r \psi)^2}$$

$\hat{\theta}$  being admissible

$$k_r^2 \leq M_r^2 < \infty$$

Define  $Y_r$  as the maximum value of  $y_r(t)$

$$y_r^2(t) < Y_r^2 < \infty$$

Then define

$$M_w \triangleq \sqrt{2}(4\sigma + M_r Y_r) < \infty$$

It follows

$$\begin{aligned} \frac{\|w\|^2}{(M_w + k_x \|x\| + k_\xi \xi)^2} &\leq \frac{M_r^2 Y_r^2 + v^2}{(\sqrt{2} M_r Y_r + 4\sqrt{2}(\sigma + r \|\phi\| + \rho \psi))^2} \\ &\leq \frac{M_r^2 Y_r^2 + v^2}{2M_r^2 Y_r^2 + 32s^2} \\ &\leq \frac{1}{2} + \frac{v^2}{32s^2} \end{aligned}$$

Now, by integration, using (4.34) :

$$\int_t^{t+T} \frac{\|w\|^2 d\tau}{(M_w + k_x \|x\| + k_\xi \xi)^2} < \frac{T}{2} + \frac{1}{2} \left(T + \frac{1}{\alpha}\right) = T + \frac{1}{2\alpha}$$

Defining  $T_2 = 1/2\alpha < \infty$ , inequality (3.6) is satisfied.

Now, all the necessary conditions of the robustness theorem are satisfied, thus the stability is proved.

### Comments

In (5.2) to (5.5) the first members of the inequalities concern the model of the process (noise, model errors, rate of variation), which are related with the design parameters of the identification algorithm. The second members concern the closed loop system characteristics ( $\omega_F$ ,  $\Omega_F$ ), which are related with the chosen adjustment law  $\mathcal{A}$ .

To some extent,  $k_d$ ,  $k_x$ ,  $k_\xi$  are the measure of the intrinsic robustness of  $\mathcal{A}$ . It follows also that  $\mathcal{A}$  must be as continuous as possible, in order to yield  $1/M_d$  large.

$k_d$ ,  $k_x$ ,  $k_\xi$ ,  $M_d$  being now assumed given, (5.2) to (5.4) impose  $\alpha$ ,  $r$ ,  $\rho$  to be small. Then (4.2) to (4.6) bound the non linearities, the unmodelled dynamics components in  $v$ , and the magnitude of  $\theta^*$ .

Note that  $\alpha$ ,  $r$ ,  $\rho$  will be generally very small, but  $T_F$  being large, slow unmodelled dynamics are permitted by (5.5).

Moreover,  $\sigma$  is not constrained : it must be only finite. It means that large bounded disturbances do not entail the stability.

Moreover, if the process is strictly linear, time invariant, exactly known model order, the adaptive control will be stable, even for  $r$  and  $\rho = 0$ .

It yields that the normalization (by  $s = \sigma + r\|\phi\| + \rho\|\psi\|$ ) and the lower bound ( $P \gg I \frac{r^2 R^2}{r^2 + R^2}$ ) vanish.

Thus, normalization and lower bound of  $\rho$  are **not** necessary features in the strictly linear, time-invariant case.

## 6. SOLVING THE STABILIZABILITY PROBLEM

The above theorem (§5) locally solves the stabilizability problem. In effect, if the a priori domain (4.7) is sufficiently small, and is included in the admissible domain, then  $\hat{\theta}(t)$  will remain continuously admissible.

However, in most cases, the a priori domain is large, and includes non admissible areas.

Then, if  $\hat{\theta}(t)$  reach a nonadmissible area, it is necessary to do something, e.g.:

i) to constrain  $\hat{\theta}(t)$  into the admissible domain, by means of some amendement of the above identification algorithm. Notice that it could be very difficult if  $D_A$  has a complex shape, and if it is not simply connected. Then jumps are to be emphasized, because  $\theta^*(0)$  and  $\hat{\theta}(0)$  are not necessarily in a same connected area.

ii) an other solution consists in waiting for the emergence of  $\hat{\theta}(t)$  from the non admissible domain ( $\bar{D}_A$ ). However if there is no persistingly exciting inputs,  $\hat{\theta}(t)$  can stay indefinitely in  $\bar{D}_A$ .

iii) even if  $\hat{\theta}(t)$  is transiently allowed to enter in  $\bar{D}_A$ , it is at least necessary to freeze  $k(\hat{\theta})$ , in order to avoid unreasonable values of  $k(\hat{\theta})$  and/or  $u(t)$ . Then, it can be said that the model from which  $k$  is adjusted can be different of the identified model. This principle was already used in the past (e.g. in "cautious control").

The same principle is applied here, under the following form :  
the equations of  $\hat{\theta}$  being unmodified, then a distinct model  $\bar{\theta}(t)$  is defined, from  $\hat{\theta}(t)$ , such that  $\bar{\theta}(t)$  be always admissible, and satisfy the desired inequities.

Define  $\bar{\theta}(t)$  as the solution of

$$\dot{\bar{\theta}} = \alpha P \phi \frac{\bar{v}}{s^2} + \sum_{i=0}^{\infty} \delta(t-t_i) \Delta_i \quad (6.1)$$

where :

- $\bar{\theta}(0) = \hat{\theta}(0) \in D_A$
- $\bar{v} \triangleq z - \phi^T \bar{\theta}$
- The instant times  $t_i$  in (6.1) are those where  $\bar{\theta}(t)$  reaches the frontiers of  $D_A$
- $\delta(t-t_i)$  is the Dirac pulse, at time  $t_i$
- $\Delta_i \triangleq \bar{\theta}(t_i^+) - \bar{\theta}(t_i^-)$  is an arbitrary jump, such that  $\bar{\theta}(t_i^+)$  belongs to the intersection of the strongly admissible domain  $D_{SA}$  (see end of §2), with an ellipsoid  $E(t_i)$  centered over  $\hat{\theta}(t_i)$ , and defined as :

$$\{\bar{\theta} \in E(t_i)\} \iff \{\|\bar{\theta} - \hat{\theta}(t_i)\|_{P^{-1}(t_i)}^2 \leq 16\} \quad (6.2)$$

where  $\hat{\theta}(t)$  and  $P(t)$  result from the above identification algorithm (4.10) to (4.15).

The hypotheses on the process  $\mathcal{P}$  are the following

- the assumptions of §4 (eq. (4.1) to (4.6))
- moreover, assume that  $\theta^*(t)$  is strictly included in  $D_{SA}$  for every  $t$  (Fig.6.1)

$$\min_{t \geq 0, \theta \in D_{FA}} \|\theta^*(t) - \theta\| \triangleq \Delta > 0 \quad (6.3)$$

- assume that  $\delta$  (see 2.30) satisfies

$$\delta < R \quad (6.4)$$

- and that

$$\theta \in D_A \Rightarrow \|\theta\| \leq R \quad (6.5)$$

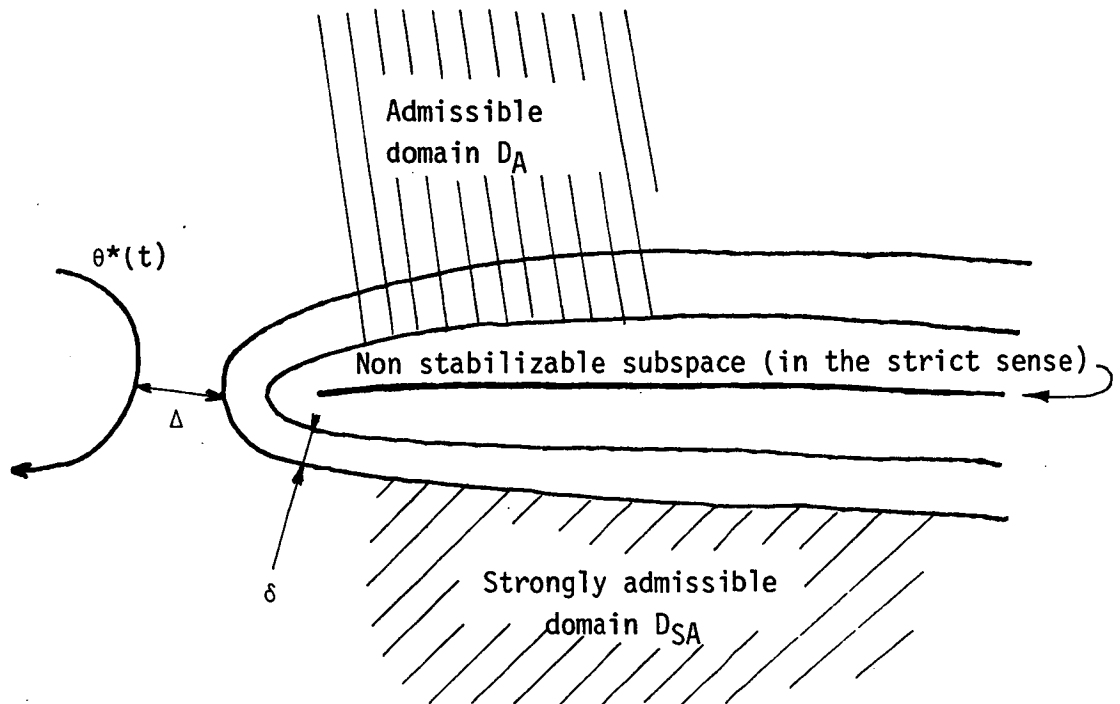


Fig.6.1: The admissible and strongly admissible domains

First, notice that the intersection  $D_{FA} \cap E(t_1)$  exists, since it includes at least  $\theta^*(t_1)$  (from (6.5), and (4.22) to (4.24)).

Then, a typical trajectory looks like  $\bar{\theta}(t)$  on figure 6.2

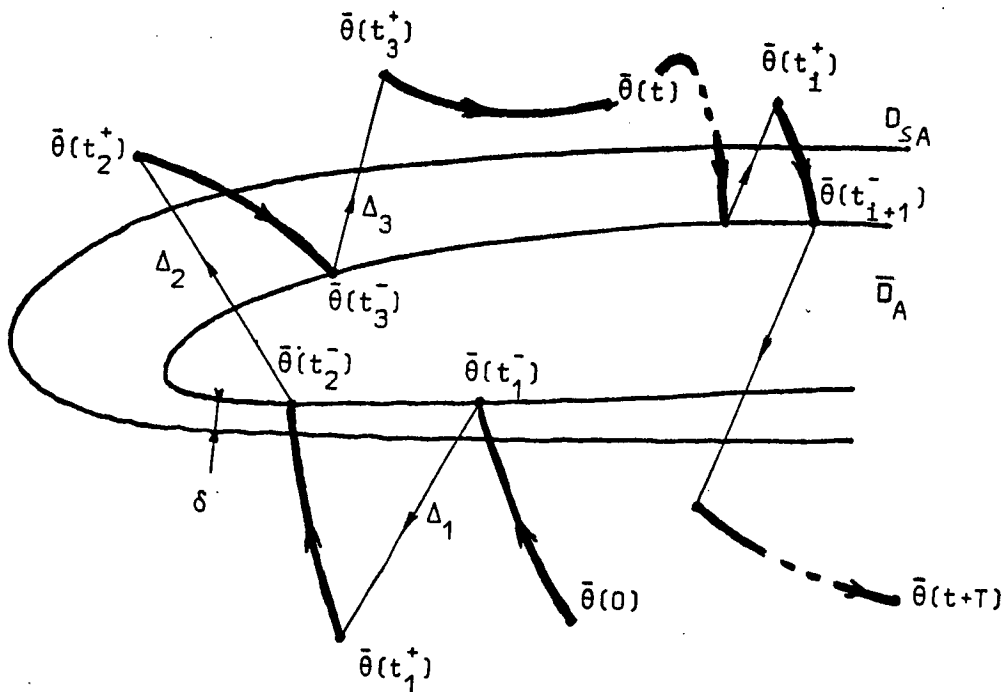


Figure 6.2 : A typical trajectory  $\bar{\theta}(t)$



Consider now the search problem for a reinitialization  $\bar{\theta}(t_1^+)$ .

If it occurs that  $\hat{\theta}(t_1) \in D_{FA}$ , simply take  $\bar{\theta}(t_1^+) = \hat{\theta}(t_1)$ .

If  $\hat{\theta}(t_1) \notin D_{FA}$ , recall that :

- $P(t_1)$  is bounded (4.20)
- $\hat{\theta}(t_1)$  is bounded (4.34)
- $\theta^*(t_1)$  is strictly included in  $E(t_1)$  - (6.2)
- $D_{FA} \subset D_A$  (bounded, from (6.5))

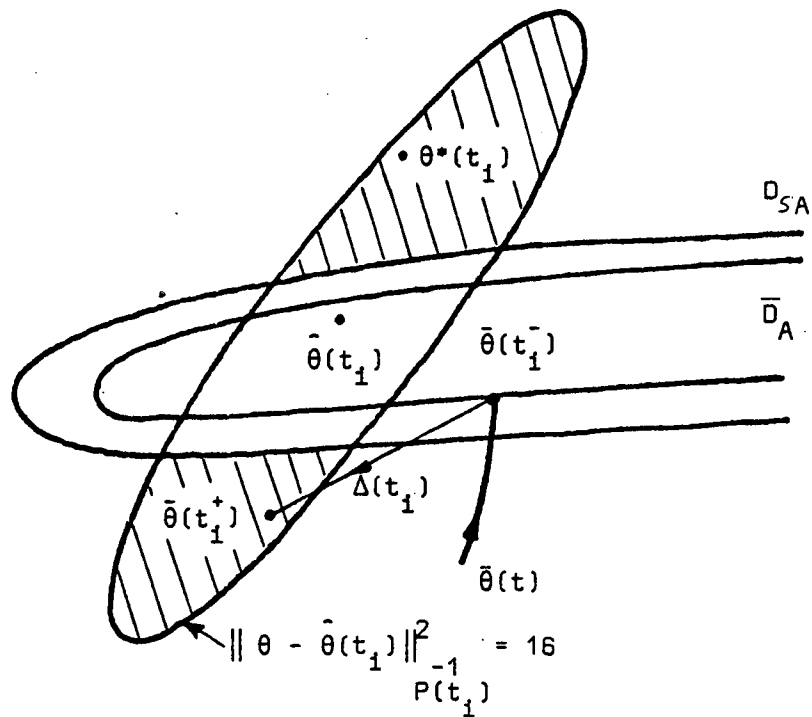


Figure 63 :  $\hat{\theta}(t_1) \in D_{SA}$

From examination of the worst case in a figure like (Fig.6.3), it follows that there exists a non zero lower bound for the following ratio :

$$\text{Ratio} = \frac{\text{Volume of } E(t_1) \cap D_{FA} \text{ (dashed)}}{\text{total volume of } E(t_1)} \gg R_m > 0$$

In the limit,  $R_m$  approaches unity if  $\bar{D}_A$  and  $\bar{D}_{FA}$  approach the strictly non stabilizable domain, whose measure is zero (Fig.6.1).

Then, one can design some search algorithm for  $\bar{\theta}(t_i^+)$ .

In the general case where the shape of  $D_{FA}$  is complex and unknown, a simple way lies in implementing a random search, defining

$$\bar{\theta}(t_i^+) = \hat{\theta}(t_i) + P^{1/2}(t_i) \gamma \quad (6.6)$$

where  $P^{1/2}$  is a factorization of  $P$ , and  $\gamma$  a random vector, uniformly distributed into the radius-4-sphere.

From the existence of  $R_m$ , it follows that the expected number of trials will be finite (mean of a Bernoulli variable), and if  $R_m$  approaches unity, this number will also approach unity.

Of course, anyone can imagine more sophisticated procedures. However, such procedures must succeed **without any exception** (even if jumps across  $D_{FA}$  reveals necessary). In fact, **systematic procedures may sometimes deceive** due to some unexpected case, so that a random choice can be the most cautious way.

### Main properties of the algorithm

a) Consider again the figure (6.2) and define  $N(t, t+T)$  as the number of jumps between  $t$  and  $t+T$ . Define also  $D(t, t+T)$  as the length of the trajectory of  $\bar{\theta}(t)$ , excluding jumps (heavy line on figure 6.2).

From the definition of the distance  $\delta$ , and the localization of  $\bar{\theta}(t_i^-)$  and  $\bar{\theta}(t_i^+)$  (respectively on the frontier of  $D_R$ , and into  $D_{SA}$ ), it is clear that :

$$D(t, t+T) \geq [N(t, t+T) - 1] \delta \quad (6.7)$$

b) define now

$$\bar{V}(t) \triangleq \| \bar{\theta} - \theta \|_P^2 \quad (6.8)$$

At an instant time  $t_1^+$ ,  $\bar{\theta}(t_1^+)$  satisfies

$$\| \bar{\theta}(t_1^+) - \hat{\theta}(t_1) \|_{P^{-1}(t_1)}^2 \leq 16$$

and from (4.25)

$$\| \hat{\theta}(t_1) - \theta^*(t_1) \|_{P^{-1}(t_1)}^2 \leq 16 \text{ (éq. (4.25))}$$

thus

$$\bar{V}(t_1^+) \leq 4 \times 16 = 64 \quad (6.9)$$

Similarly to the proof of (4.24), from  $t_1^+$  as initial time, it follows :

$\bar{V}(t) \leq 64 \quad \text{for every } t$

(6.10)

c) Using (6.10), and similarly with (4.35)

$$\int_{t_1^+}^{t_{1+1}^-} \left( \frac{\bar{V}}{s} \right)^2 d\tau \leq 64 \left[ t_{1+1} - t_1 + \frac{1}{\alpha} \right] \quad (6.11)$$

Then, if N reinitializations occur between t and t+T

$\int_t^{t+T} \left( \frac{\bar{V}}{s} \right)^2 d\tau \leq 64 \left[ T + \frac{N+1}{\alpha} \right]$

(6.12)

d) From (6.1), D(t, t+T) is given by

$$D(t, t+T) = \int_t^{t+T} \left\| \alpha P \phi \frac{v}{s^2} \right\| d\tau$$

Then, from (4.40), (6.12) and the Schwartz inequality

$$D^2(t, t + T) \leq \alpha^2 \cdot 2n R^2 \left(T + \frac{1}{\alpha}\right) \cdot 64 \left[T + \frac{N + 1}{\alpha}\right] \quad (6.13)$$

Using (6.7) :

$$(N - 1)^2 \delta^2 \leq 128n R^2 (\alpha T + 1) (\alpha T + N + 1)$$

Now, define

$$N_0 \triangleq \frac{128n R^2}{\delta^2} \quad (6.14)$$

It follows

$$(N - 1)^2 \leq N_0 (\alpha T + 1) (N - 1 + \alpha T + 2)$$

Thus

$$(N - 1)^2 \leq N_0 (\alpha T + 1) (N - 1) + N_0 (\alpha T + 1) (\alpha T + 2) \quad (6.15)$$

For simplicity, the last term is bounded using  $N_0 > 1$  (from 6.4) and  $\alpha T < 2 \alpha T$

$$N_0 (\alpha T + 1) (\alpha T + 2) \leq N_0 [N_0 (\alpha T + 1) (2\alpha T + 2)] = 2 N_0^2 (\alpha T + 1)^2$$

(6.15) becomes

$$(N - 1)^2 - N_0 (\alpha T + 1) (N - 1) - 2N_0^2 (\alpha T + 1) \leq 0$$

By factorization

$$[(N - 1) + N_0 (\alpha T + 1)] [(N - 1) - 2N_0 (\alpha T + 1)] \leq 0$$

Thus

$$- N_0 (\alpha T + 1) \leq \underline{(N - 1)} \leq 2N_0 (\alpha T + 1)$$

and thus

$$\boxed{N(t, t + T) \leq 1 + 2N_0(\alpha T + 1)} \quad (6.16)$$

This key result provides a bound of the possible number of reinitialization between times  $t$  and  $t+T$ .

Now, it will be easy to bound  $\bar{v}^2$  and  $\bar{\theta}(t)$ .

e) Substituting (6.16) into (6.12)

$$\begin{aligned} \int_t^{t+T} \frac{\bar{v}^2}{s^2} d\tau &\leq 64 \left[ T + \frac{1 + 2N_0(\alpha T + 1) + 1}{\alpha} \right] \\ &= 64 \left[ T + \frac{2}{\alpha} + 2N_0 \left( T + \frac{1}{\alpha} \right) \right] \\ &\leq 64 \left[ 2T + \frac{2}{\alpha} + 2N_0 \left( T + \frac{1}{\alpha} \right) \right] \end{aligned}$$

Define

$$\boxed{N_1 = N_0 + 1} \quad (6.17)$$

It follows

$$\boxed{\int_t^{t+T} \frac{\bar{v}^2}{s^2} d\tau \leq 128 N_1 \left( T + \frac{1}{\alpha} \right)} \quad (6.18)$$

to be compared with (4.35) : ...  $\leq 16 \left( T + \frac{1}{\alpha} \right)$

f) Similarly, from (6.16) and (6.13)

$$D^2(t, t + T) \leq \alpha^2 2n R^2 \left( T + \frac{1}{\alpha} \right) \cdot 128 N_1 \left( T + \frac{1}{\alpha} \right)$$

From (6.15)

$$128n R^2 = N_0 \delta^2 \leq N_1 \delta^2$$

Thus

$$\boxed{D(t, t + T) \leq 2 \alpha \delta N_1 \left( T + \frac{1}{\alpha} \right)} \quad (6.19)$$

On the other hand, the jumps satisfy  $\|\Delta_1\| \leq 2R$  (from 6.5). It follows the bound for the whole length (now including jumps).

$$\int_t^{t+T} \|\dot{\bar{\theta}}\| \, d\tau \leq D(t, t+T) + 2R N(t, t+T) \quad (6.20)$$

Transform using (6.16) and (6.19)

$$\int_t^{t+T} \|\dot{\bar{\theta}}\| \, d\tau \leq 2\alpha N_1 \delta \left(T + \frac{1}{\alpha}\right) + 2R(1+2N_0(\alpha T+1))$$

For simplicity, introduce  $\delta < R$ , and  $(1 + N_0(1+\alpha T)) < 2N_1(1+\alpha T)$  (from 6.17). It follows

$$\boxed{\int_t^{t+T} \|\dot{\bar{\theta}}\| \, d\tau \leq 6N_1 \alpha R \left(T + \frac{1}{\alpha}\right)} \quad (6.21)$$

to be compared with (4.37).

Now, from the new inequalities (6.18) and (6.2), the robustness theorem applies again, and leads easily to the following theorem :

### Theorem 3

Let  $\mathcal{P}$  the process. The parameters  $\theta^*(t)$  satisfy (4.1) to (4.6) and (6.3) to (6.5), where the domains  $D_A$  and  $D_{SA}$  are related to some given adjustment law satisfying (3.3), (3.4).

The identified model is given by (6.1).

Then, the closed loop system is globally uniformly stable if :

$$\alpha > 0 \quad (6.22)$$

$$4N_1 \alpha R \leq k_d/M_d \quad (6.23)$$

$$16\sqrt{N_1} r \leq k_x \quad (6.24)$$

$$16\sqrt{N_1} \rho \leq k_\xi \quad (6.25)$$

$$1/\beta \leq T_F \quad (6.26)$$

where

$$N_1 \triangleq \frac{128n R^2}{\delta^2} + 1 \quad (6.27)$$

and where  $T_F, k_x, k_\xi, k_d$  are defined by (3.9) to (3.19)

### Comments

From inequalities (6.23) to (6.25), robustness is clearly reduced, due to the number  $N_1$  (eq. 6.27), in which  $R/\delta$  is necessarily large.

More precisely, for a given process,  $\sigma, \alpha, r, \rho, R$ , are to be defined from the level of noise, non-linearities, under-modellization, and the rate of time variations, but not from (6.23) to (6.25).

The reason is that the existence of  $\bar{\theta}$  depends on the existence of the non empty subspace  $D_{SA} \cap E(t_i)$ .

Thus, the above data ( $\sigma, \alpha, r, \rho, R$ ) must be defined from the best available prior knowledges.

Now, consider that  $\delta$  is introduced in order to ensure the existence of the upper-bound (6.16) for  $N(t, t+T)$ , even in the worst imaginable case. It follows that transgressing (6.23) to (6.25) fortunately does not imply instability.

An other interpretation of the conditions (6.22) to (6.25) is that for a given indirect adaptive control, defined from non zero coefficients  $\alpha$ ,  $r$ ,  $\rho$ . There exist a non empty class of weakly undermodelized and time varying processes, for which stability is ensured.

## 7. CONCLUSIONS

The main contributions of the paper are the following :

First, a theorem of robust stability is provided, dealing with weakly undermodelized systems (dynamics and non-linearities). This theorem belongs to the so called "small gain" family. As an original feature, it may deal also with slowly time varying systems.

Moreover, the given upper bounds are possibly satisfied not only by the "exact" models of the processes, but by the classically identified models (typically R.L.S. algorithms).

It follows that the above theorem plays the role of a basic technical Lemma, when analyzing indirect adaptive control systems.

If assuming the identified model be stabilizable for every time, the application of the theorem is rather easy and our results are not really stronger than those of PRALY [14], from which ours are derived.

The main resemblance lies in signals normalization by  $1/\|\phi\|$ , but there are some differences in the way for bounding  $\hat{\theta}$  and  $P$ . Moreover, we are dealing with adaptive control of slowly time varying systems.



Then, we proposed, just as a prototype, an identification algorithm satisfying the conditions which are required for applying the robustness theorem. Among other properties, the pair  $\hat{\theta}$ ,  $P$  defines a certainty ellipsoid around  $\hat{\theta}$ . This domain is non-trivial, in the following sense : if  $P$  becomes small, the domain really reduce to a small domain (better than the given a priori knowledges).

The existence of this certainty domain already is, by itself, an usefull property. Moreover, it is the basis for producing a new model  $\bar{\theta}(t)$ , distinct from  $\hat{\theta}(t)$ , which is not only stabilizable for every  $t$ , but also satisfies the required conditions when applying the robustness theorem.

Up to now, the proof concerns only one "prototypical" identification algorithm. However, the main feature of this algorithm are rather common, and generalizations will be provided in the next future.

The only goal of this paper was to prove the **existence** of some fair solution to globally stable adaptive control in the purely passive approach.

Obviously, it remains thru that exciting inputs are a propitious factor for identification, and then for adaptive control. However it is very important to claim that exciting inputs are **not** a necessary condition for robust overall stability of adaptive control.

REFERENCES

- [1] **Y. BAR-SHALOM and E. TSE.**  
"Dual effect, certainty equivalence, and separation in stochastic control",  
**IEEE Trans. Automat. Contr.**, vol. AC-19, n°5, Oct. 1984, pp.494-500.
- [2] **K.-J. ASTROM and B. WITTENMARK.**  
"On self tuning regulators", **Automatica**, vol.9, 1973, pp.185-199.
- [3] **I.-D. LANDAU.**  
"A survey of Model Reference Adaptive TEchniques - Theory and applications",  
**Automatica**, vol.10, 1974, pp.353-379
- [4] **R.-V. MONOPOLY.**  
"Model reference adaptive control with an augmented error signal", **IEEE  
Trans. Automat. Contr.**, vol. AC-19, Oct. 1974, pp. 474-484.
- [5] **K.-S. NARENDRA and L.-S. VALAVANI.**  
"Stable adaptive controller design - Direct control", **IEEE Trans. Automat.  
Contr.**, vol. AC-23, aug. 1978, pp. 570-583.
- [6] **Ph. de LARMINAT.**  
"On overall stability of certain adaptive control systems", **5th IFAC Symposium  
on Identification**, Darmstadt, F.R.G., 1979.
- [7] **Ph. de LARMINAT.**  
"Unconditional stabilization of linear discrete systems via adaptive control",  
**Systems and Control Letters**, vol.1, 1981, pp.7-11.
- [8] **G.-C. GOODWIN and K.-S. SIN.**  
"Adaptive control of non minimum phase systems", **IEEE Trans. Automat. Contr.**,  
vol. AC-26, n°2, April 1981, pp.478-484.
- [9] **L. LJUNG and T. SODERSTROM.**  
"Theory and practice of recursive identification", **MIT Press**, Cambridge,  
Mass., 1983.

- [10] **G.-C. GOODWIN and E.-K. TEOH.**  
"Persistency of excitation in the presence of possible unbounded signals",  
**IEEE Trans. Automat. Contr.**, vol. AC, 1983.
- [11] **Ph. de LARMINAT.**  
"On the stabilizability condition in indirect adaptive control", **Automatica**,  
vol. 20, n°6, 1984, pp. 793-795.
- [12] **R. LOZANO-LEAL and G.-C. GOODWIN.**  
"A globally convergent adaptive pole placement algorithm without a  
persistency of excitation requirement", **IEEE Trans. Automat. Contr.**,  
vol. AC-30, n°8, aug. 1985, pp. 795-708.
- [13] **Ph. de LARMINAT.**  
"Une solution robuste au problème de la stabilisabilité dans la commande  
indirecte passive", **Colloque CNRS, Commande adaptative**, Grenoble (FR),  
Nov. 1984.
- [14] **L. PRALY.**  
"Robustness of indirect adaptive control based on pole placement design",  
**Proceedings of the IFAC workshop on application of adaptive control theory**,  
San Francisco, 1983.

APPENDIX

PROOF OF THE ROBUSTNESS THEOREM

First part

Lemma 1

Let  $\Sigma$  be the symmetric solution of

$$F^T \Sigma + \Sigma F + 2I = 0 \quad \text{A.1}$$

where  $F$  satisfies the properties  $P_F$  :

$$\left[ \begin{array}{l} \|F\| \leq \Omega < \infty \\ R_E(\lambda_1) \leq -\omega_F < 0 \end{array} \right. \quad \begin{array}{l} \text{A.2} \\ \text{A.3} \end{array}$$

Then :

$$\Sigma \leq T_F I \quad \text{A.4}$$

$$\Sigma \geq \tau_F I \quad \text{A.5}$$

Where :

$$T_F \triangleq \frac{n_F^2}{2\omega_F} \left[ \frac{2\Omega_F}{\omega_F} \right]^{2n_F} \quad \text{A.6}$$

$$\tau_F = \frac{1}{\Omega_F} \quad \text{A.7}$$

**Proof**

i) For any eigenvector  $p_i$  of  $F$  :

$$|\lambda_i| = \frac{\|\lambda_i p_i\|}{\|p_i\|} = \frac{\|F p_i\|}{\|p_i\|} \leq \max_{q \neq 0} \frac{\|Fq\|}{\|q\|} \triangleq \|F\|$$

Thus, from (A.2)

$$|\lambda_i| \leq \Omega_F$$

A.8

ii) Let  $a(s)$  be the characteristic polynomial of  $F$  :

$$a(s) \triangleq s^{n_F} + a_1 s^{n_F-1} + \dots + a_{n_F} = (s - \lambda_1)(s - \lambda_2) \dots (s - \lambda_{n_F})$$

Then :

$$\left. \begin{aligned} |a_1| &= \left| \sum_{i=1}^{n_F} \lambda_i \right| \leq n_F \Omega_F = C_{n_F}^1 \Omega_F \\ |a_2| &= \left| \sum_{i=1}^{n_F} \sum_{\substack{j=1 \\ i \neq j}}^{n_F} \lambda_i \lambda_j \right| \leq C_{n_F}^2 \Omega_F^2 \\ &\vdots \\ |a_{n_F-1}| &\leq C_n^{n-1} \Omega_F^{n-1} \\ |a_{n_F}| &\leq \Omega_F^n \end{aligned} \right\}$$

A.10

iii) lets consider a factor  $\frac{1}{s-\lambda_i}$  of  $\frac{1}{a(s)}$

where  $\lambda_i = \alpha_i + j\beta_i$ ,  $\alpha_i^2 + \beta_i^2 = |\lambda_i|^2 \leq \Omega_F^2$ ,  $\alpha^2 \geq \omega_F^2$

$$\text{then } \frac{1}{|j\omega - \lambda_i|^2} = \frac{1}{(\omega - \beta)^2 + \alpha^2}$$

and obviously :

$$\left| \frac{1}{j\omega - \lambda_i} \right|^2 \leq \frac{1}{\alpha^2} \leq \frac{1}{\omega_F^2}$$

A.11

there exists also  $\gamma$  satisfying

$$\frac{1}{(\omega - \beta)^2 + \alpha^2} \leq \frac{\gamma}{|\lambda_i|^2 + \omega^2}$$

$\gamma$  must satisfy :

$$\gamma[(\omega - \beta_i)^2 + \alpha_i^2] - |\lambda_i|^2 - \omega^2 \geq 0$$

which yields

$$\gamma(\omega^2 - 2\beta_i\omega + \beta_i^2 + \alpha_i^2) - |\lambda_i|^2 - \omega^2 \geq 0$$

$$(\gamma - 1)\omega - 2\beta_i\gamma + (\gamma - 1)|\lambda_i|^2 \geq 0$$

which is always satisfied for

$$\beta_i\gamma = (\gamma - 1)|\lambda_i|$$

Thus :

$$\gamma = \frac{|\lambda_i|}{|\lambda_i| - |\beta_i|}$$

Other form : 
$$\gamma = \frac{|\lambda_i| (|\lambda_i| + |\beta_i|)}{(|\lambda_i| - |\beta_i|) (|\lambda_i| + |\beta_i|)} = \frac{|\lambda_i|^2 + |\lambda_i| |\beta_i|}{|\lambda_i|^2 - \beta_i^2}$$

$$= \frac{|\lambda_i|^2 + |\lambda_i| |\beta_i|}{\alpha^2} \leq \frac{2|\lambda_i|^2}{\alpha_i^2} \leq \frac{2\Omega_F^2}{\omega_F^2}$$

Finally :

$$\left| \frac{1}{j\omega - \lambda_i} \right|^2 \leq \frac{2\Omega_F^2}{\alpha^2 (|\lambda_i|^2 + \omega^2)} \leq \frac{2\Omega_F^2}{\omega_F^2 (\omega_F^2 + \omega^2)}$$

A.12

An upper bound of  $\left| \frac{\omega}{j\omega - \lambda_i} \right|$  can also be easily verified :

$$\left| \frac{\omega}{j\omega - \lambda_i} \right|^2 \leq \frac{|\lambda_i|^2}{\alpha^2} \leq \frac{\Omega_F^2}{\omega_F^2}$$

A.13

iv) Prove that

$$\| (j\omega I - F)^{-1} \| \leq \frac{n_F^2}{2} \left( \frac{2\Omega_F}{\omega_F} \right)^{2n_F} \frac{1}{\omega_F^2 + \omega^2}$$

A.14

**Proof**

First, verify that

$$\begin{aligned}
 (sI - F)^{-1} = \frac{1}{a(s)} \{ & s^{n_F-1} + a_1 s^{n_F-2} + \dots + a_{n_F-2} s + a_{n_F-1} \} I \\
 & + (s^{n_F-2} + a_1 s^{n_F-3} + \dots + a_{n_F-2}) F \\
 & \vdots \\
 & + (s + a_1) F^{n_F-2} \\
 & + F^{n_F-1} \}
 \end{aligned} \tag{A.15}$$

(by multiplication of (A.15) by (sI-F) and using the Caley-Hamilton theorem :  
 $F^{n_F} + a_1 F^{n_F-1} + \dots + a_{n_F} I = 0$ )

Then, using (A.2), (A.10), (A.15), it follows

$$\begin{aligned}
 \|(j\omega I - F)^{-1}\| \leq & \left| \frac{1}{a(j\omega)} \right| \times \{ |\omega|^{n_F-1} + C_{n_F}^1 \Omega_F |\omega|^{n_F-2} + \dots + C_{n_F}^{n_F-1} \Omega_F^{n_F-1} \\
 & + \Omega_F |\omega|^{n_F-2} + C_{n_F}^1 \Omega_F^2 |\omega|^{n_F-3} + \dots + C_{n_F}^{n_F-2} \Omega_F^{n_F-1} \\
 & \vdots \\
 & + \Omega_F^{n_F-2} |\omega| + C_{n_F}^1 \Omega_F^{n_F-1} \\
 & + \Omega_F^{n_F-1} \}
 \end{aligned} \tag{A.16}$$

consider any term of (A.16) defined as :

$$a_i \triangleq \left| \frac{1}{a(j\omega)} \right| \cdot \times \Omega_F^i |\omega|^{n_F-1-i}$$

$a_i$  can be rewritten into

$$a_i = \left[ \frac{\Omega_F}{|j\omega - \lambda_1|} \times \dots \times \frac{\Omega_F}{|j\omega - \lambda_1|} \right] \times \left[ \frac{|\omega|}{|j\omega - \lambda_{i+1}|} \times \dots \times \frac{|\omega|}{|j\omega - \lambda_{n_F-1}|} \right] \times \left[ \frac{1}{|j\omega - \lambda_{n_F}|} \right]$$

Then, from (A.11), (A.12) and (A.13) :

$$a_i \leq \left( \frac{\Omega_F}{\omega_F} \right)^i \left( \frac{\Omega_F}{\omega_F} \right)^{n_F-1-i} \left( \frac{\Omega_F}{\omega_F} \sqrt{\frac{2}{\omega_F^2 + \omega^2}} \right)$$

From which :

$$a_1 \leq \left( \frac{\Omega_F}{\omega_F} \right)^{n_F} \sqrt{\frac{2}{\omega_F^2 + \omega^2}}$$

Thus, (A.16) becomes

$$\| (j\omega I - F)^{-1} \|^2 \leq \left( \frac{\Omega_F}{\omega_F} \right)^{2n_F} \frac{2}{\omega_F^2 + \omega^2} \left[ \begin{array}{c} 1 + C_{n_F}^1 + \dots + C_{n_F}^{n_F-1} \\ + 1 + C_{n_F}^1 + \dots + C_{n_F}^{n_F-2} \\ \vdots \\ + 1 + C_{n_F}^1 \\ + 1 \end{array} \right]^2 \quad \text{A.17}$$

The last factor is given by

$$\left\{ \frac{n_F}{2} (1 + C_{n_F}^1 + C_{n_F}^2 + \dots + C_{n_F}^{n_F-1} + 1) \right\}^2 = \left\{ \frac{n_F}{2} 2^{n_F} \right\}^2$$

Thus (A.17) becomes (A.14) :

$$\| (j\omega I - F)^{-1} \|^2 \leq \frac{n_F^2}{4} \left( \frac{2\Omega_F}{\omega_F} \right)^{2n_F} \frac{2}{\omega_F^2 + \omega^2}$$

(v) End of proving (A.4) and (A.6)

Recall that if

$$PF + F^T P + Q = 0 \quad \text{A.18}$$

where  $F$  is asymptotically stable and  $Q$  is a symmetric matrix (positive definite or not), then :

$$P = \int_0^{\infty} e^{F^T \tau} Q e^{F \tau} d\tau \quad \text{A.19}$$

Here,  $Q = 2I$ ,  $P = \Sigma$ .



On the other hand, the Fourier transform of  $e^{Ft}$  is  $(j\omega I - F)^{-1}$ , then, applying the Parseval inequality :

$$\Sigma = 2 \int_0^{\infty} e^{F^T \tau} e^{F\tau} d\tau = 2 \int_0^{\infty} (j\omega I - F)^{-T} (j\omega I - F)^{-1} \frac{d\omega}{2\pi}$$

Then

$$\|\Sigma\| \leq 2 \int_{-\infty}^{+\infty} \|(j\omega I - F)^{-1}\|^2 \frac{d\omega}{2\pi}$$

Recall that

$$2 \int_{-\infty}^{+\infty} \frac{1}{\omega_F^2 + \omega^2} \frac{d\omega}{2\pi} = \frac{1}{\omega_F}$$

Thus, using (A.14)

$$\|\Sigma\| \leq \frac{n_F^2}{2\omega_F} \left( \frac{2\Omega_F}{\omega_F} \right)^{2n_F}$$

which proves (A.4) and (A.6)

(vi) Proof of (A.5) and (A.7)

Let  $\xi(t)$  be a solution of  $\dot{\xi} = F\xi$ , and define  $E \triangleq \xi^T \xi$

Then  $\dot{E} = 2\xi^T F\xi$

and  $|\dot{E}| \leq 2\|\xi\|^2 \|F\| \leq 2E\Omega_F$

Thus  $\underline{-2E\Omega_F} \leq \dot{E} \leq 2E\Omega_F$ .

By integration of the above inequality

$$E(t) \geq E(0) e^{-2\Omega_F t} = \|\zeta(0)\|^2 e^{-2\Omega_F t}$$

A last integration gives

$$\int_0^{\infty} E(t) dt \geq \frac{\|\zeta(0)\|^2}{2\Omega_F}$$

On the other hand

$$E(t) = \zeta(0)^T \begin{bmatrix} e^{F^T t} & \\ & e^{Ft} \end{bmatrix} \zeta(0)$$

From (A.18) and (A.19) :

$$\int_0^{\infty} E(t) dt = \zeta(0)^T \frac{\Sigma}{2} \zeta(0)$$

Thus, for any  $\zeta(0)$  :

$$\zeta^T(0) \Sigma \zeta(0) \leq \frac{\|\zeta(0)\|^2}{\Omega_F}$$

which proves (A.5), (A.7)

## Second Part

### Lemma 2

Now,  $F$  is assumed to be time varying, then, the solution of (A.1) becomes  $\Sigma(t)$  :

$$F^T(t)\Sigma(t) + \Sigma(t)F(t) + 2I = 0 \tag{A.20}$$

Assume that  $\Omega_F$  and  $\omega_F$  are constants in (A.2), (A.3).

Then (A.4), (A.5) are true for all  $t$ , and :

$$\boxed{\|\dot{\Sigma}(t)\| \leq 2T_F^2 \|\dot{F}\|} \tag{A.21}$$

Proof

By differentiation of (A.20) :

$$F^T \dot{\Sigma} + \dot{\Sigma} F + (\dot{F}^T \Sigma + \Sigma \dot{F}) = 0$$

Apply (A.18), (A.19) with  $P = \dot{\Sigma}$  and  $Q = (\dot{F}^T \Sigma + \Sigma \dot{F})$

$$\dot{\Sigma} = \int_0^{\infty} e^{F^T(t)\tau} \left[ \dot{F}(t) \Sigma(t) + \Sigma(t) \dot{F}(t) \right] e^{F(t)\tau} d\tau$$

Then

$$\begin{aligned} \|\dot{\Sigma}\| &\leq 2\|\dot{F}\| \cdot \|\Sigma\| \left\| \int_0^{\infty} e^{F^T\tau} e^{F\tau} d\tau \right\| \\ &\leq 2\|\dot{F}\| \cdot \|\Sigma\| \left\| \frac{\Sigma}{2} \right\| \leq \|\dot{F}\| T_F^2 \quad (\text{from (A.4)}) \end{aligned}$$

**Third part**

Introduce the following positive function :

$$W(t) \triangleq x^T(t) \Sigma(t) x(t) + T_{\xi} \xi^2(t) \tag{A.22}$$

By differentiation, using (3.1) and (3.8)

$$\dot{W} = x^T \dot{\Sigma} x + 2x^T \Sigma (Fx + w) - 2(\xi - \|x\|) \xi$$

Using (A.1) :

$$\begin{aligned} \dot{W} &= x^T \dot{\Sigma} x + 2x^T \Sigma w - 2x^T x - 2\xi^2 + 2\|x\| \xi \\ &= x^T \dot{\Sigma} x + 2x^T \Sigma w - x^T x - \xi^2 - \left[ \|x\|^2 + \xi^2 - 2\|x\| \xi \right] \end{aligned}$$

$$\text{where } -x^T x - \xi^2 \leq -\frac{x^T \Sigma x}{T_F} - \frac{T_{\xi} \xi^2}{T_F} \quad (\text{From (A.4) and (3.9)})$$

use again (A.22) :

$$\dot{W} \leq x^T \dot{\Sigma} x + |2x^T \Sigma w| - \frac{W}{T_F}$$

A.23

• consider now the first term  $x^T \dot{\Sigma} x$  of (A.23) :

From (A.21), (A.5), (A.22), it follows :

$$x^T \dot{\Sigma} x \leq \|x\|^2 T_F^2 \| \dot{F} \| \leq \frac{x^T \Sigma x}{T_F} T_F^2 \| \dot{F} \| \leq \frac{T_F^2}{T_F} W \| \dot{F} \|$$

and, from (3.10)

$$\boxed{x^T \dot{\Sigma} x \leq \frac{1}{2T_F} \frac{\| \dot{F} \|}{k_d} W}$$

A.24

• Then consider  $x^T \Sigma w$ . From the Schwartz inequality :

$$|x^T \Sigma w| \leq \sqrt{x^T \Sigma x} \sqrt{w^T \Sigma w}$$

From (A.22) and (A.4) :

$$|x^T \Sigma w| \leq \sqrt{W} \sqrt{T_F \|w\|^2} \leq \sqrt{T_F} \sqrt{W M} \frac{w}{M}$$

A.25

where

$$M(t) \triangleq M_w + k_x \|x(t)\| + k_\xi \xi(t)$$

A.26

From (A.5) :

$$M \leq M_w + k_x \sqrt{\frac{x^T \Sigma x}{T_F}} + k_\xi \sqrt{\frac{T_\xi \xi^2}{T_\xi}}$$

From (A.22) :

$$M \leq M_w + \left( \frac{k_x}{\sqrt{T_F}} + \frac{k_\xi}{\sqrt{T_\xi}} \right) \sqrt{W}$$

Then, (A.25) becomes :

$$|x^T \Sigma w| \leq \left[ \sqrt{T_F} M_w \sqrt{W} + \left( \sqrt{\frac{T_F}{T_F}} k_x + \sqrt{\frac{T_F}{T_\xi}} k_\xi \right) W \right] \left\| \frac{w}{M} \right\|$$

and from (3.11) and (3.12) :

$$\boxed{2|x^T \Sigma w| \leq \left[ 2\sqrt{T_F} M_w \sqrt{W} + \frac{1}{4T_F} W \right] \left\| \frac{w}{M} \right\|}$$

A.27

Now, from (A.23), (A.24) and (A.27) :

$$\frac{\dot{W}}{W} \leq -\frac{1}{T_F} + \frac{1}{2T_F} \frac{\| \dot{F} \|}{k_d} + \left( \frac{2\sqrt{T_F} M_W}{\sqrt{W}} + \frac{1}{4T_F} \right) \left\| \frac{W}{M} \right\| \quad \text{A.28}$$

Define  $W_0$  as :

$$W_0 \triangleq \text{Max} \{ W(0), (8T_F \sqrt{T_F} M_W)^2 \}$$

and  $t_0$  a time  $t$  (if it exists) such that  $W(t_0) = W_0$ .

Then, as long as  $W(t) \geq W_0$ , it yields

$$\frac{2\sqrt{T_F} M_W}{\sqrt{W}} \leq \frac{1}{4T_F},$$

and A.28 becomes

$$\frac{\dot{W}}{W} \leq -\frac{1}{T_F} + \frac{1}{2T_F} \frac{\| \dot{F} \|}{k_d} + \frac{1}{2T_F} \left\| \frac{W}{M} \right\| \quad \text{A.29}$$

Apply the Schwartz inequality :

$$\left( \int_t^{t+T} \left\| \frac{W}{M} \right\| \cdot 1 \, d\tau \right)^2 \leq \int_t^{t+T} \left\| \frac{W}{M} \right\|^2 \, d\tau \int_t^{t+T} 1 \, d\tau$$

From (3.6) :

$$\left( \int_t^{t+T} \left\| \frac{W}{M} \right\| \, d\tau \right)^2 \leq (T + T_2) T \quad (\leq (T + T_2)^2)$$

Thus

$$\int_t^{t+T} \left\| \frac{W}{M} \right\| \, d\tau \leq T + T_2 \quad \text{A.30}$$

By integration of (A.29), using (3.5) and (A.30) :

$$\int_{t_0}^{t_0+T} \frac{\dot{W}}{W} \, d\tau \leq -\frac{1}{2T_F} + T_1 + \frac{1}{2T_F} + T_2 = \frac{T_1 + T_2}{2T_F}$$

Thus

$$\text{Log} \left( \frac{W(t_0 + t)}{W(t_0)} \right) \leq W_0 \frac{T_1 + T_2}{2T_F}$$

and

$$W(t_0 + t) \leq W_0 e^{\frac{T_1 + T_2}{2T_F}}$$

Thus  $W(t)$  is uniformly bounded, and from (A.22), (A.5) :

$$\|x\|^2 \leq \frac{x^T \Sigma x}{\tau_F} \leq \frac{W}{\tau_F} \leq \frac{W_0}{\tau_F} e^{\frac{T_1 + T_2}{2T_F}} < \infty$$

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