Rib Waveguide Plasmonic Sensor for Lab-on-Chip Technology

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Abstract. A prompt medical diagnosis is of major importance, starting the appropriate treatment earlier results in better outcomes and faster recovery times. Plasmonic biosensors based on photonic integrated circuits (PIC) are potential candidates in the development of lab-on-chip (LOC) technology, allowing digitalization of results and virtualization of laboratorial procedures in the detection of important biomarkers. These sensors have the advantages of high sensitivity and faster analysis when compared with traditional laboratorial methodologies. We study the possibility of exciting a surface plasmon, using low-cost fabrication methods and techniques based on amorphous silicon compounds, rib waveguide geometry and dimensions compatible with plasma-enhanced chemical vapor deposition (PECVD) and ultraviolet (UV) lithography. Results of Finite-Difference Time-Domain (FDTD) simulation of the plasmon excitation and sensor response are presented and discussed.

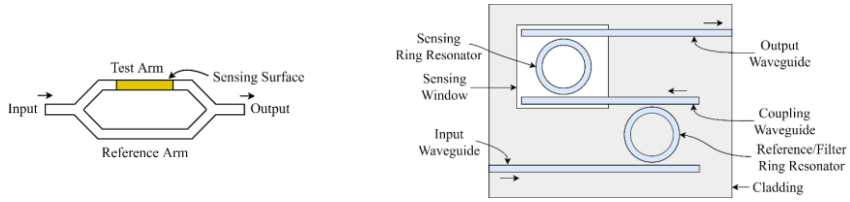
Keywords: Plasmonics, Lab-on-chip, Amorphous silicon, Photonic integrated circuit.

1 Introduction

Clinical assays are fundamental diagnostic tools employed to detect disease markers on samples of human tissue and fluids. Conventional techniques require expensive laboratory equipment and trained personnel, making the process complex, expensive and time-consuming. Lab-on-chip (LOC) technology, based on compact optical devices, such as photonic integrated circuit (PIC) biosensors, can be designed to detect several biomarkers (e.g. proteins, nucleic acids, drugs, pathogens and human cells) [1], paving the way to the development of Point-of-Care (PoC) diagnostic platforms. Studies demonstrate that these highly integrated sensors can be employed in the diagnosis of several diseases and health conditions, such as viruses [2], cancers [3] and acute kidney injury [4]. Early biomarker detection contributes to improving patient prognosis. State-of-the-Art photonic biosensors are able to detect analytes in a few

minutes [5] and can achieve very high sensitivities [1], with detection limits between 10^{-4} and 10^{-6} RIU (refractive index units) or even less [1, 6–8].

The success of PoC testing platforms is dependent on the development of technologies which are easily adapted to the detection of various analytes with high sensitivity and suitable for low-cost large scale deployment. Surface Plasmon Resonance sensors based on the Kretschmann configuration [9] are an example of a technology which excels on sensitivity and adaptability to different analytes. On the negative side, the equipment is too expensive and bulky for mass deployment in PoC applications. There is much interest in solutions that avoid large or expensive components, such as motor rotation stages and prisms, and which are based on low-cost materials and fabrication processes. In recent studies a large diversity of photonic sensor architectures comprising waveguides have been reported, the vast majority of sensors lay inside one of the following categories: 1) Plasmonic sensors based solely on waveguides [10–12]; 2) Interferometric sensors, Fig. 1, exploring surface plasmon resonance [13–15], the evanescent wave effect [16] or the interference between two modes (bimodal waveguides) [17]; 3) Sensors employing one or more ring resonators [18, 19], Fig. 1; 4) Sensors featuring cavities [20, 21].



(a) (b)

Fig. 1. Top view of two photonic sensor configurations (simplified). (a) Mach-Zehnder Interferometer (MZI) implementation based on waveguides, comprising Y-junction splitter and combiner. (b) An example of ring resonator topology, the Vernier-cascade sensor [22], this configuration comprises three waveguides and two ring resonators, the filter ring resonator and input waveguide are totally covered by the cladding.

The trend has been to reduce the form factor of the photonic circuits, to achieve higher integration, leveraged by sub-micrometer lithographic processes [19, 21, 23–25], however, there is a major drawback in size reduction, which are the increased manufacturing costs. A possible alternative are larger photonic devices, which can be produced at lower costs [26]. Despite current trends, multi-micron sensor devices have been proposed in the last decade [16, 17], these designs are based on rib waveguides. Considering the State-of-the-Art in biosensing, the following research question is proposed:

- What could be a suitable method to develop a low-cost, highly sensitive, compact and efficient sensor system that can be suitable to the detection of various biomarkers in point-of-care medical applications?

Sub-micron waveguides have the advantage of higher integration, however, when compared with multi-micron waveguides, the former have the disadvantages of higher losses and higher sensitivity to fabrication imperfections [26]. Multi-micron waveguides can be fabricated using low-cost processes with lower spatial resolutions,

such as Plasma-Enhanced Chemical Vapor Deposition (PECVD) combined with ultraviolet (UV) lithography. Multi-micron rib waveguides have some advantages when compared with other waveguide types (e.g. strip waveguides), in terms of light coupling efficiency, losses and production costs, making them suitable for biosensing applications [16]. Large cross-section rib waveguides can be designed to support single-mode (SM) operation [27–29], resulting in reduced light coupling loss when interfaced with optical fibers [30] and lower losses due to side-wall roughness [31].

Hydrogenated amorphous silicon (a-Si:H) and its compounds, hydrogenated amorphous silicon carbide (a-SiC:H) and hydrogenated amorphous silicon nitride (a-SiN:H), can be deposited by PECVD at lower temperatures (typically, between 200 °C - 400 °C) [32], reducing fabrication costs. By controlling the compound percentages, it is possible to fine tune the material structure and optical properties, like for example the refractive index [33], allowing the integration of several components, such as power splitters, interferometers, waveguides and photodetectors.

In this research, finite-difference time-domain (FDTD) and Finite Element Method (FEM) simulations are performed to study a SM rib waveguide surface plasmon resonance sensor. The photonic circuit is of low complexity and can be fabricated with inexpensive materials, such as silicon dioxide (SiO_2) and nitrogen-rich a-SiN:H, the sensitive layer is made of a thin silver layer (Ag), with 40 nm thickness. The device can be fabricated using low-cost methods such as PECVD and UV lithography, also benefiting from better light coupling efficiency, due to its larger cross-section. The operating wavelength is 405 nm, the same used in high-definition optical discs, in the limit of the visible spectrum.

2 Contribution to Technological Innovation for Digitalization and Virtualization

Industry 4.0 is a concept devised to the industrial domain, comprising individualization and virtualization [34], implemented by new technologies for automation and data exchange. This concept applied to the health domain is called Health 4.0 [35]. The six principles of Industry 4.0 [34] are: 1) Interoperability; 2) Virtualization; 3) Decentralization; 4) Real-Time Capability; 5) Service Orientation; 6) Modularity. Biosensors and LOC technology contribute to all seven principles of Health 4.0:

Interoperability can be achieved by aggregation and integration of the different devices and services, being a major step towards the generation of meaningful information [35]. Data fusion combines information collected from different sensors to more accurately assess the patient's health conditions [36], helping medical staff in the establishment of a personalized treatment.

With point-of-care analytical platforms, the clinical assay procedure can be partially virtualized, because the laboratory is "contained within a single device" and result interpretation can be made by computational algorithms, contributing to a significant reduction of the workload and the physical size of the lab.

Decentralization is accomplished due to the portability of the LOC platform, enabling clinical assays to be conducted *in-loco*, by a single doctor, nurse or analyst,

the service is personalized, meaning healthcare can shift from centralized to a customized patient-oriented service.

Biosensors are extremely fast and typically can provide results within minutes [5], significantly contributing for real-time diagnosis. Due to the increased access to clinical assays, appropriate disease follow-up and prevention measures can be taken, so the probability of serious episodes and hospital admission lowers significantly.

The sensors' output is converted into the digital domain, allowing interfacing with latest generation networks (i.e. 5G) and cloud technologies, which are enablers for service orientation in the health domain [35]. The concept of modularity is also applicable to PoC equipment for medical assays, considering that the equipment features one or more receptacles were biosensor "cartridges" can be inserted or removed. Following this approach, LOCs can adapt to detect different analytes, the sensor "cartridges" can also be periodically upgraded or replaced if malfunctioning.

Another principle was added later: Safety, security and resilience [35]. In order to minimize the risks for the patients, it is important to assure the reliability and resilience of the system, by improving the biosensor's sensitivity and selectivity.

Conventional medical diagnostics rely primarily on the symptomatology, being prone to fail due to inadequate reporting or lack of symptoms on initial stages of disease [36]. Machine learning (ML), artificial intelligence (AI) and the internet of things (IoT) have the potential to be applied with biosensors, allowing real-time monitoring [37].

3 Theoretical Background and Sensor Configuration

The sensor developed in this study is based on a SM silicon-on-insulator (SOI) rib waveguide, having an a-SiN:H core deposited over a SiO_2 substrate, Fig. 2. The plasmonic section is covered by a thin silver (Ag) layer. It differs from the work of Fantoni *et al.* [12], because it is focused on a multi-micron design, made possible by a rib geometry, different waveguide materials and operating wavelength.

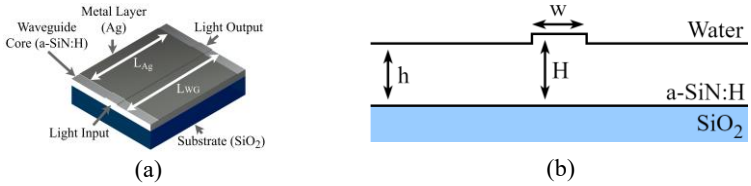


Fig. 2. Sensor design based on the rib waveguide. (a) Tridimensional model, L_{WG} and L_{Ag} represent waveguide and silver layer lengths, respectively. (b) Transversal section, w represents rib width, H rib height and h slab height.

3.1 Single-Mode Rib Waveguide Dimensioning

It is desirable to design waveguides for SM propagation in order to maximize power efficiency. Rib waveguide SM operation was the focus of several studies [27–29]. Rib waveguide geometry is characterized by three main parameters, rib width (w), rib

height (H) and slab height (h), Fig. 2. To guarantee the design is compatible with low-cost lithographic and deposition processes (UV and PECVD), the width of the rib (w) should be equal to or greater than 1 μm, so it was set at 1.5 μm, to allow a small margin. Etch depth (D) was defined as 0.1 μm, the maximum r value was set at 0.9. Expression (1) establishes the relationship between rib waveguide design parameters and SM operation [28, 29], the expression is valid for $0.5 \leq r < 1$. By replacing h in $r = h/H$ by $H - D$, the rib height (H) can be obtained from (1):

$$w/H \leq \alpha + r \cdot (1 - r^2)^{-1/2} . \tag{1}$$

Parameter α is 0 when considering the Effective Index Method (EIM), Pogossian *et al.* [28] or 0.3 according to Soref *et al.* [27]. Following the more conservative approach of null α, the resulting rib height value is 0.82 μm, implying a slab height value of 0.72 μm, which were the dimensions used in this study.

3.2 Surface Plasmon Polariton (SPP) Excitation

Surface Plasmon Polaritons can only be excited by TM guided modes. In order to excite the SPP the effective refractive index difference between the plasmonic mode and the waveguide fundamental TM mode must be small. SPP complex refractive index as a function of angular frequency is given by (2):

$$n_{eff_{SPP}}(\omega) = \sqrt{\frac{\varepsilon_d(\omega)\,\varepsilon_m(\omega)}{\varepsilon_d(\omega) + \varepsilon_m(\omega)}}, \tag{2}$$

where ω is the angular frequency in rad/s, $\varepsilon_d(\omega)$, $\varepsilon_m(\omega)$ correspond to the complex permittivity function of the sample medium and metal, respectively.

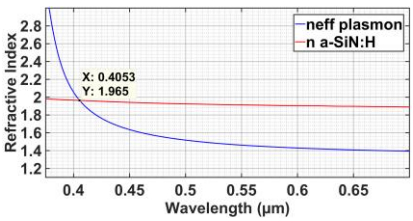


Fig. 3. Effective refractive index of the SPP (real component), represented in blue, refractive index of a-SiN:H with Si/N < 1 (real component), represented in red. The intersection point shows an ideal SPP excitation wavelength of 405 nm and a refractive index of 1.965.

From (2) and considering that the effective refractive index of the waveguide's fundamental mode is similar to the index of the core material, the intersection point is found in Fig. 3. The resulting wavelength of 405.3 nm is ideal to excite the SPP from the fundamental TM mode of the waveguide. Results assume the sample medium is water, the metal layer is silver (refractive index from Jiang *et al.* [38]) and the waveguide material is a-SiN:H with Si/N ratio under 1 (refractive index from Charifi *et al.* [39]). The intersection point occurs for a refractive index of 1.965.

4 Results

4.1 Modal Analysis

In Fig. 4, the major electric and magnetic XY field distributions are depicted, on the top of the rib a small field intensity is present, this effect makes plasmon excitation possible. The mode's effective refractive index is 1.949, the extinction coefficient is 2.8×10^{-12}, because the material is considered non-dispersive.

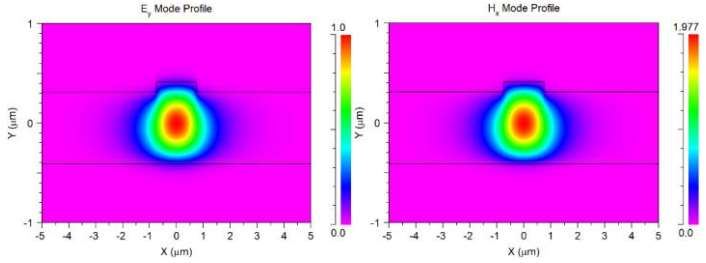


Fig. 4. Fundamental TM mode of the rib waveguide obtained in FEM simulation. (a) E_y and (b) H_x fields. Layers are delimited by black lines (from top to bottom, water, a-SiN:H and SiO_2).

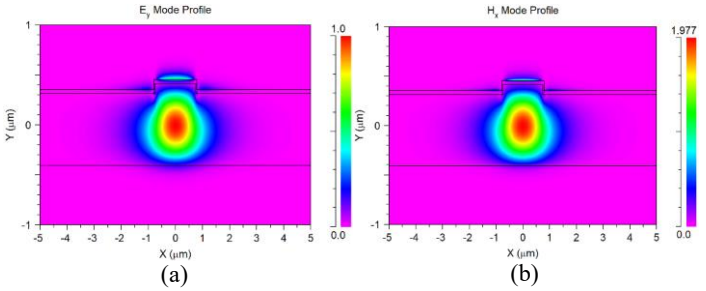


Fig. 5. FEM simulation results of the coupling between the fundamental TM mode and the SPP. (a) E_y and (b) H_x fields. Layers are delimited by black lines (from top to bottom, water, silver, a-SiN:H and SiO_2).

In Fig. 5, it is possible to notice the coupling between the fundamental TM mode of the rib waveguide and the surface plasmon mode, in this region of the sensor a thin silver layer with 40 nm thickness is deposited over the waveguide's core. The plasmonic field is visible over the center of the silver layer placed on top of the waveguide's rib. The effective refractive index of the mode is approximately 1.948. The deviation from the predicted refractive index of 1.965 (Fig. 3) is under 0.9 %.

In Fig. 6, the vertical cuts of the major electric and magnetic fields are represented, the higher peaks represent the waveguide fundamental TM mode, which is confined within the waveguide's core. Minor peaks are also visible, which correspond to the SPP propagating over the silver layer.

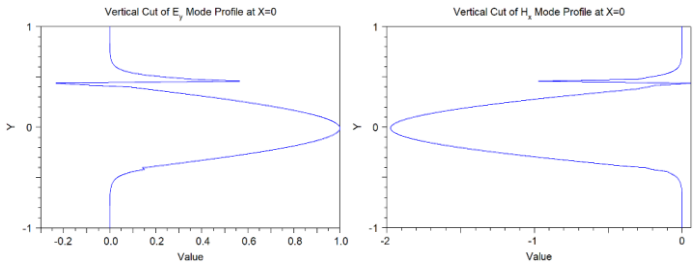


Fig. 6. Vertical cut of: (a) E_y and (b) H_x fields, the characteristic plasmon field profile is present on the top, showing coupling between the waveguide TM mode and SPP mode.

4.2 Sensor's Response

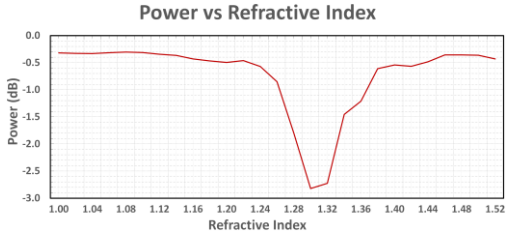


Fig. 7. Transmitted power as a function of the sample medium refractive index.

The sensor's response was simulated for a waveguide length (L_{WG}) of 12 µm and a silver layer length (L_{Ag}) of 10 µm, Fig. 2. FDTD simulations were performed for sample medium refractive index values between 1 and 1.52. The fundamental TM mode is coupled to the input of the waveguide and power is measured at the output.

In Fig. 7, for refractive index values between 1.29 and 1.31, a large dip is observable in the sensor's response, output power is under -2.7 dB, confirming the sensing behavior. The attenuation from the baseline is 2.2 dB.

5 Conclusions and Future Work

A plasmonic sensor based on a rib waveguide was designed and simulated. The waveguide geometry and multi-micron size allows light coupling from optical fibers, requiring only a plane-convex lens termination to converge the light beam. Due to the large size of the sensor, simple design and constituting materials (a-SiN:H), low-cost fabrication techniques can be employed, such as PECVD and UV lithography.

The sensitivity window covers the refractive index of human body fluids making it interesting to biosensing platforms. The dip in the power of the transfer function is still

modest leaving room for improvement. Since the sensor operates with visible light (405nm), testing is facilitated. This wavelength is also used in high-definition optical disks. Further studies are necessary to establish the optimal metal and waveguide lengths. Equally important is the impact of the silicon-to-nitrogen ratio of a-SiN:H. Discovering the ideal proportion is fundamental to achieve the best plasmon excitation scenario. It is also necessary to improve the a-SiN:H model with k values based on experiments conducted at visible light wavelengths (400 nm to 700 nm).

Acknowledgments. Research supported by FCT - Fundação para a Ciência e Tecnologia, through grant SFRH/BD/07792/2021 and projects PTDC/NAN-OPT/31311/2017, FCT/MCTES: UIDB/00066/2020, and by Instituto Politécnico de Lisboa, through project IPL/2021/wavesensor_ISEL.

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