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Pauline Morin, Antoine Muller, Georges Dumont, Charles Pontonnier. Comparison of two contact detection methods for ground reaction forces and moment estimation during sidestep cuts, runs and walks. *Journal of Biomechanical Engineering*, 2024, 146 (1), pp.1-9. 10.1115/1.4064034. hal-04256186

HAL Id: hal-04256186

<https://inria.hal.science/hal-04256186v1>

Submitted on 24 Oct 2023

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Comparison of two contact detection methods for ground reaction forces and moment estimation during sidestep cuts, runs and walks

Force platforms often limit the analysis of human movement to the laboratory. Promising methods for estimating ground reaction forces and moments can overcome this limitation. The most effective family of methods consists of minimizing a cost, constrained by the subject's dynamic equilibrium, for distributing the force over the contact surface on the ground. The detection of contact surfaces over time is dependent on numerous parameters. This study proposes to evaluate two contact detection methods: the first based on foot kinematics and the second on pressure sole data. Optimal parameters for these two methods were identified for walking, running and sidestep cuts tasks. The results show that a single threshold in position or velocity is sufficient to guarantee a good estimate. Using pressure sole data to detect contact improves the estimation of the position of the centre of pressure. Both methods demonstrated a similar level of accuracy in estimating ground reaction forces.

Keywords: Biomechanics, Motion analysis, Ground reaction forces, Outside laboratory experiments

1 Introduction

Methods for analysing human movement based on inverse dynamics make it possible to calculate biomechanical quantities such as intersegmental moments during movement. They require ground reaction forces and moments (GRF&M), traditionally measured by force platforms. The analysis of human movement without the need for force platforms represents a major application opportunity outside the laboratory, with applications in many fields, such as sport, ergonomics and physical activity monitoring, requiring to estimate the GRF&M instead of measuring them.

Several approaches can be used to estimate GRF&M from motion capture data [1–3] or pressure insoles data [4, 5]. The estimation of GRF&M from motion capture data based on the equations of dynamics is indeterminate in the case of multiple contacts. Solving this indeterminacy using an optimization approach has already yielded good results on several movements and subjects [1, 6, 7]. A cost function is minimized, constrained by the subject's dynamic equilibrium to distribute the overall force over the contact surfaces.

In [1, 8, 9], contact surfaces are discretized into a set of points located under the feet (from 12 to 40 points under each foot). A point is considered to be in contact with the ground if its vertical position is lower than a position threshold z_0 (from 0.02 m to 0.04 m) and if its velocity norm is lower than a velocity threshold v_0 (from 0.8 m.s⁻¹ to 1.3 m.s⁻¹). The position and velocity thresholds will hereafter be grouped together under the term kinematic thresholds. In [1], the kinematic thresholds ($z_0 = 0.03$ m and $v_0 = 0.8$ m.s⁻¹) were chosen using a preliminary sensitivity study on walking trials. In [8, 9], the values of the kinematic thresholds were defined empirically. The use of these kinematic thresholds is only possible for movement on a ground of known level. The adjustment of kinematic threshold values can be time-consuming and requires knowledge of motion analysis (order of magnitude

of motion-specific velocities, errors in estimating positions from motion data), which is why the values presented are widely used without individualisation or adaptation to the task studied. In addition, the methods used in these studies consider a single-solid foot model. A two-solids foot model would a priori allow more accurate kinematic tracking and therefore better detection of contact via the use of kinematic thresholds.

Pressure insoles provide quantities (position of the centre of pressure, quantity of pressure on several zones under the feet) to describe foot-ground contact at the cost of a limited impact on the subject's movement [4, 5]. To our knowledge, no method based on an optimization approach for estimating the GRF&M uses the pressure sole data for contact detection. This type of pressure insole approach would be compatible with experiments outside the laboratory, allowing a wide range of application studies.

In the present study, two methods of estimating GRF&M differing in their method of contact detection were compared: one method of contact detection based on motion data and another based on pressure insole data. The performance of the methods was evaluated in terms of the accuracy of the GRF&M estimate relative to the force-platform data. This study assumes that by improving the contact detection method, the GRF&M estimation method will be improved. The first contact detection method was similar to that presented in the [1, 6, 9, 10] studies and used kinematic thresholds (position and velocity). The second was based on the use of pressure insoles using a pressure threshold. A parametric study was carried out to determine the thresholds for each of the two contact detection methods.

2 Material and methods

2.1 Experimental procedure. The cohort consisted of 4 women and 10 men (age: 29 ± 2 yo, height: 1.8 ± 0.1 m, weight: 70 ± 10 kg). The inclusion criterion was to wear size 38, 39, 42 or 43 shoes since two sizes of insoles were available (38-39

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Version 1.18, October 24, 2023

and 42-43 EU). Each subject signed an informed consent form and a pseudonimisation protocol was followed for data storage. The experimental protocol was approved by INRIA's National Ethics Committee (Comité Opérationnel d'Evaluation des Risques Légaux et Ethiques, 2021-06, 22/02/2021).

Whole-body motion capture was performed by placing 46 reflective markers on standardised anatomical landmarks in accordance with the recommendations of the International Society of Biomechanics [11, 12]. Motion capture data were recorded using a Qualisys optoelectronic motion capture system (200 Hz, 22 12 Mpixels OQUS 7+ cameras). GRF&M were recorded with two AMTI force platforms (2000 Hz). The pressure under the foot, the position of the centre of pressure (CoP), the vertical force and the acceleration of the foot were recorded by Moticon[®] insoles (OpenGo, 100 Hz, 16 pressure cells covering 65% of the surface of the insole, with a resolution of $0.25\text{N}/\text{cm}^2$ and a hysteresis of $< 1\%$ [13], an inertial measurement unit (IMU) at the centre of each insole). The insole data was linearly interpolated from 100 Hz to 200 Hz to match the frequency of the Qualisys system and synchronized with the optoelectronic data in accordance with [14]. The wireless insoles were inserted into the subjects' personal sports shoes.

Prior to data collection, the pressure insoles were reset and calibrated according to the manufacturer's recommendations. During the experiment, each subject performed 15 sidestep cuts, 15 runs and 15 walks at comfort speed, i.e. 15 trials per subject per condition to obtain an acceptable statistical comparison [15]. Sidestep cuts were always performed using the right foot as the support foot. Subjects had to modulate their stride so as not to touch the two platforms during a given step. Of the 630 trials collected, 521 trials were studied: the 45 trials relating to one participant that required additional pre-processing due to insole malfunction were discarded, as were 64 other trials for multiple causes (markers obscured, one-off pressure sole malfunction, platform data not usable due to failure to follow experimental instructions).

2.2 Contact detection. The area under each foot was divided into a set of 16 points. The points were defined on the foot model according to the coordinates of the centre of each pressure cell of the Moticon[®] insole: according to the manufacturer's documentation, the position of the centre of each pressure cell was defined in the reference frame of the sole and the position of the centre of each cell was expressed in the reference frame of the foot model. For this purpose, a transformation matrix between the sole frame and the foot frame, determined as in [14], was used. For all participants, the matrix used was that determined during a randomly selected running trial for the participant with the highest height, in order to obtain the most accurate placement of the contact points in relation to the foot. The points were located under the foot and the participants wore sports shoes (with sole thicknesses ranging from 0.01 m to 0.03 m). As a result, the vertical position of the points never reached zero.

Two contact detection methods were used to determine at each moment and for each contact point whether it was active, i.e. in contact with the ground.

The first method of contact detection was a kinematic threshold detection based on the method presented in [1, 6, 7, 9, 10]. Contact induced zero relative velocity between the foot and the ground (it was assumed that there was no sliding between the foot and the ground defined as a plane), which implied a constant distance that can be determined (minimum distance between the contact point and the ground). A point was considered active if its distance from the ground (corresponding to its vertical position if the ground was horizontal and to its normal given by the direction of gravity) was less than a threshold value z_0 and if the norm of its velocity was less than a threshold value v_0 . A parametric study was carried out by comparing the results obtained with different threshold values:

- position threshold z_0 (in m) : 0.01 (minimum thickness of the shoe soles), 0.02, 0.05 [1], 0.1, 0.2 and 1;
- velocity threshold v_0 (in $\text{m}\cdot\text{s}^{-1}$) : 0.5, 0.8 [1], 3, 5 and 10.

The positions and velocities of the contact points were calculated from the trajectories of the markers and an osteo-articular model, in an inverse kinematics step. The human body was modelled by a geometric model composed of 19 rigid bodies linked by 17 joints corresponding to 43 degrees of freedom. A two-part foot model was chosen in order to better track the kinematics of the foot. The geometric model was calibrated using the method presented in [16]. The inverse kinematics step was performed using a multibody kinematics optimization performed with a penalty-based Levenberg-Marquardt algorithm [17]. The position of the markers and the joint coordinates were filtered using a Butterworth low-pass filter with no phase shift and at cut-off frequencies of 10 Hz and 5 Hz respectively, as recommended in [9, 18]. From the joint coordinates obtained, the position of the potential contact points was calculated using a direct geometric model, and their velocity was obtained using second-order finite differentiation of position.

The second method of contact detection was a pressure threshold detection. A point was considered to be in contact if the pressure measured at this point by the Moticon[®] pressure insole was higher than a threshold value p_0 . A parametric study was carried out by comparing the results obtained with different pressure threshold values (in $\text{N}\cdot\text{cm}^{-2}$): 0 (pressure insoles contact detection criterion), 0.25 (insole measurement resolution), 1.5, 2, 3, 4, 5, 6, 7, 9, 11 and 13.

A permanent contact condition was also considered to challenge the usefulness of contact detection methods in the external force estimation method.

2.3 GRF&M estimation. To compare the contact detection methods, a method for estimating the GRF&M using an optimization approach was developed. This method was based on the method presented in [9] (Figure 1 shows the general methodology). The method used as input the motion data, the geometric model and the inertial model (established from anthropometric tables from [19]) specific to the participant.

The inverse kinematics step and the contact detection step were detailed in the previous paragraph.

In the dynamic equilibrium calculation step, global external forces and moments were computed using the Recursive Newton-Euler Algorithm (RNEA). The moments were expressed at the origin of the pelvis.

The distribution of the global effort estimated the force \mathbf{F}_i (vector 3×1) on each active contact point among the $N = 32$ potential contact points. The external force vector \mathbf{F} (vector $3N\times 1$) corresponded to the concatenation of the vectors \mathbf{F}_i . As soon as at least three contact points were considered active, there was an infinite number of solutions (6 equation, 9 unknown). At each instant, a sequential quadratic programming method determined $\mathbf{F}_i = (\text{Fi}^x \text{Fi}^y \text{Fi}^z)^T$ by solving the following minimization problem:

$$\min_{\mathbf{F}} \sum_{i=1}^N \|\mathbf{F}_i\|^2 \quad (1)$$

such as $\left\{ \begin{array}{l} \text{Dynamic equilibrium of the whole body,} \\ \forall i \in \llbracket 1, N \rrbracket, \text{Fi}^x < \text{Fi}^x_{\text{imax}}, \text{Fi}^y < \text{Fi}^y_{\text{imax}} \text{ et } \text{Fi}^z < \text{Fi}^z_{\text{imax}}. \end{array} \right.$

The problem was constrained by the dynamic equilibrium and by the maximal effort $\mathbf{F}_{\text{imax}} = (\text{Fi}^x_{\text{imax}} \text{Fi}^y_{\text{imax}} \text{Fi}^z_{\text{imax}})^T$ defined as admissible for each potential contact point i . \mathbf{F}_{imax} was proportional to the weight of the participant (BW). As in the study [10], a frictional cone was considered defined by Coulomb's law with a friction coefficient $\mu = 0.5$. This approximation was used to linearize the constraint. With \mathbf{z} as the normal to the contact surface, we had:

$$\mathbf{F}_{\text{imax}} = k_i \times \begin{pmatrix} \mu \\ \mu \\ 1 \end{pmatrix}. \quad (2)$$

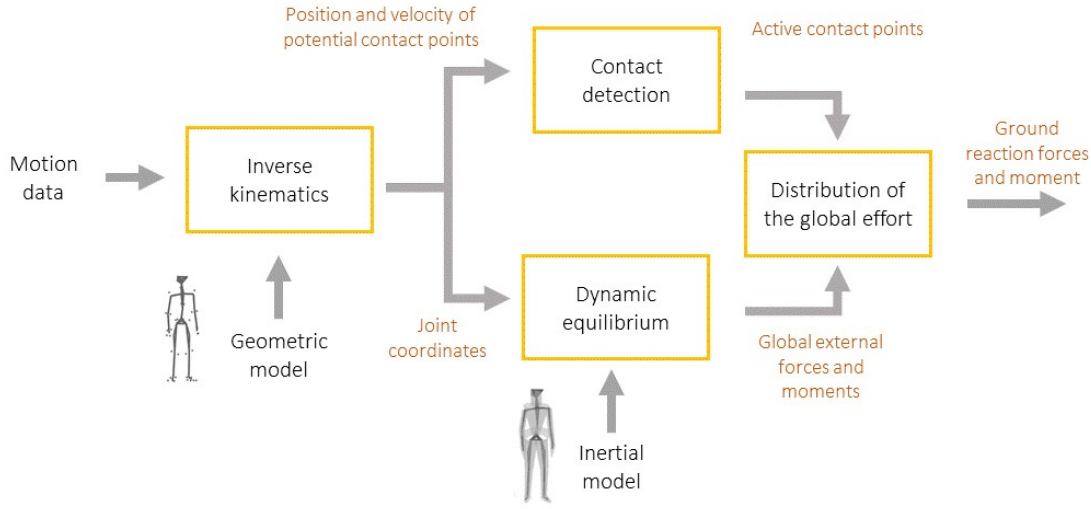


Fig. 1 General methodology for estimating GRF&M from motion data based on the optimization approach. The different stages of the method are boxed in yellow. The quantities estimated during the method are shown in yellow. The input quantities (models and experimental data) are shown in black.

193 The value of k_i depended on the number of active contact points:

$$194 \quad k_i = \begin{cases} 0.4 \times \frac{N}{N_{active}(t)} \times BW & \text{if the point is active,} \\ 0 & \text{else.} \end{cases} \quad (3)$$

195 The coefficient of 0.4 was determined empirically in [1, 9].
196 $N_{active}(t)$ is the number of active contact points at time t , guar-
197 anteeing a constant reserve force at each instant.

198 Each component of the estimated effort was filtered using the
199 same filter as that used to filter the joint coordinates in order to
200 avoid the appearance of filtering artifacts [20]. All the methods
201 were implemented in CusToM [21].

202 **2.4 Parametric study.** Both CoP position and resultant force
203 were compared between measured and estimated data to assess
204 the performance of a given set of contact detection parameters.
205 Such comparison could only be done when at most one foot was
206 in contact with a given force platform. Contact between the foot
207 and the force platform was considered active when both measured
208 and estimated forces were higher than 10 N [8, 22, 23] (the force
209 platform admitted an accuracy of 0.5% of the measured force).

210 At each instant and for each foot, the error on the resultant
211 force was defined as the norm of the difference between estimated
212 $\mathbf{F}_{estimated}$ and measured \mathbf{F}_{pf} resultant forces:

$$213 \quad \text{Error}_{resultant} = \|\mathbf{F}_{pf} - \mathbf{F}_{estimated}\|. \quad (4)$$

214 At each instant and for each foot, the CoP position error
215 (of zero altitude) was defined as the distance between estimated
216 $\mathbf{CoP}_{estimated}$ and measured \mathbf{CoP}_{pf} CoP positions:

$$217 \quad \text{Error}_{CoP} = \|\mathbf{CoP}_{estimated} - \mathbf{CoP}_{pf}\|. \quad (5)$$

218 The root mean square errors (RMSEs) of these errors were cal-
219 culated for each trial to quantify the difference between the esti-
220 mated and measured [24]. The average RMSEs on the resultant
221 force and on the position of the CoP were compared for each type of
222 movement studied according to the values of the contact detection
223 parameters used.

224 For both contact detection methods, the set of parameters giv-
225 ing the most accurate estimate of the external force for all types

of movement was identified. For each type of movement stud- 226
ied and for each type of error, the minimum mean value of the 227
RMSE ($RMSE_{min}$) was identified. This value was multiplied 228
by a coefficient $k_{threshold} > 1$ and the RMSE results below 229
 $k_{threshold} * RMSE_{min}$ were retained. The value of $k_{threshold}$ 230
was increased (with an increment of 0.01) until a set of detection 231
thresholds was common to each type of movement and each type 232
of error. 233

2.5 Comparison. The two contact detection methods were 234
compared in terms of the accuracy of the GRF&M estimate ob- 235
tained with the optimal parameters of each method. For each con- 236
tact detection method, the average duration of contact sequences 237
(the time during which at least one point belonging to the foot 238
was in contact with the ground) and the average number of active 239
contact points per contact phase were calculated. The average du- 240
ration of the sequences during which the force platforms measured 241
a force greater than 10 N was calculated. 242

The significance of differences in the accuracy of the GRF&M 243
estimate was statistically tested. The distribution of RMSEs ob- 244
tained with each detection method was compared using a Wilcoxon 245
test after rejecting the hypothesis of a normal distribution using a 246
Shapiro-Wilk test. 247

3 Results 248

The results of the parametric study on the choice of kinematic 249
thresholds are presented in Figure 2. The optimum value for the 250
position threshold was $z_0 = 0.05$ m and the optimum value for 251
the velocity threshold was $v_0 = 3$ m.s⁻¹ with $k_{threshold} = 1.17$. 252
The results of the parametric study on the choice of the pressure 253
threshold are presented in Figure 3. The optimum value for the 254
pressure threshold was $p_0 = 4$ N.cm⁻² with $k_{threshold} = 1.06$. 255

The error on the resultant force and on the CoP position obtained 256
for each movement is summarized in Table 1 using each contact 257
detection method and using a permanent contact. Both contact de- 258
tection methods ensured a similar accuracy in estimating resultant 259
force, whereas the pressure threshold allowed a better estimate of 260
the CoP position. 261

The accuracy of the external force estimation decreased when 262
the detection thresholds did not detect all the contact instants (Fig- 263
ure 2), e.g. for $z_0 = 0.01$ m and $v_0 = 0.5$ m.s⁻¹. The accuracy of 264
the external force estimation decreased when the detection thresh- 265
olds allowed permanent detection of contact (Figure 3). 266

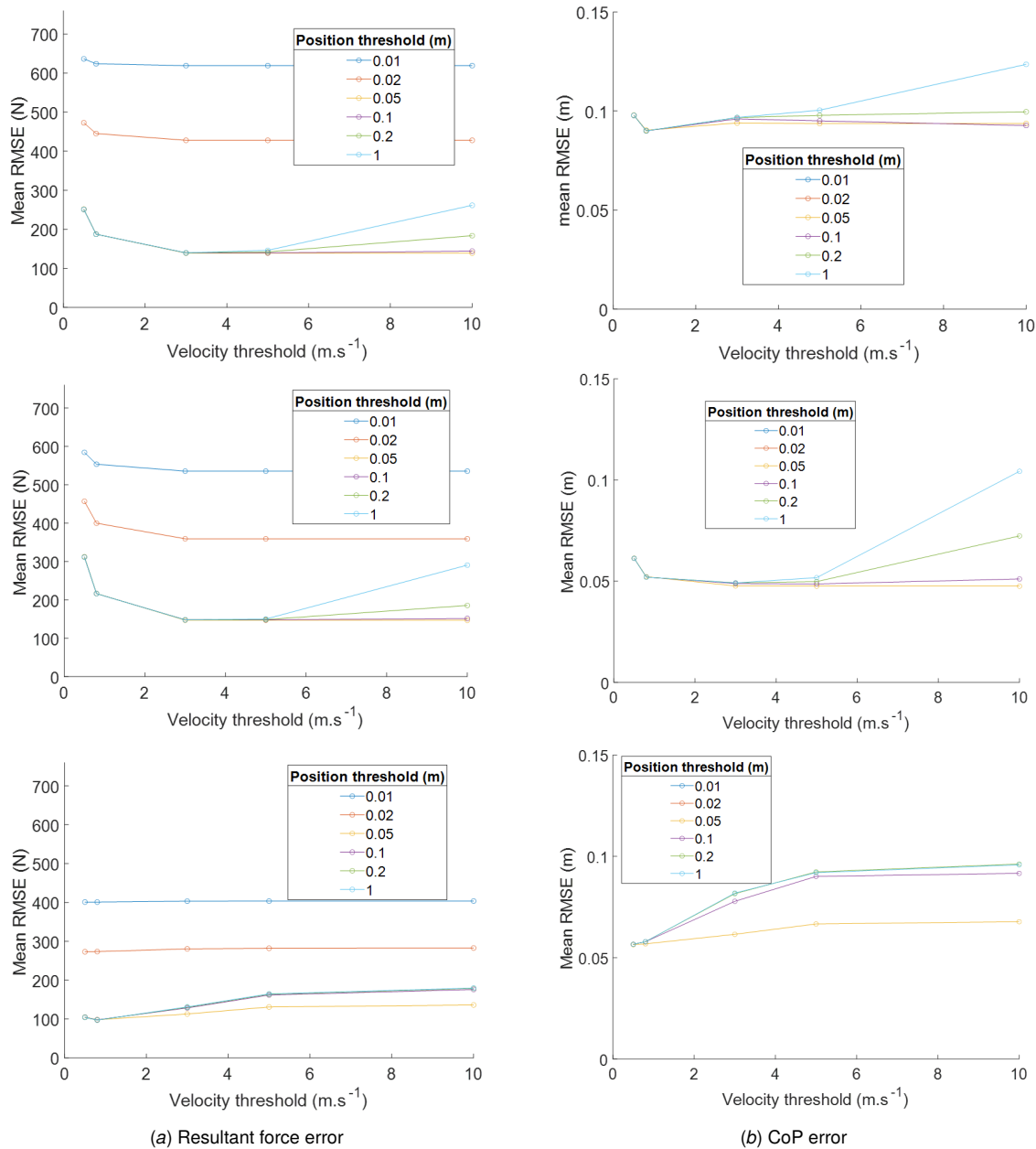


Fig. 2 Accuracy of the GRF&M estimate during sidestep cuts (top), runs (middle) and walks (bottom) according to the kinematic thresholds used: error on the resultant force and error on the CoP position.

267 The average contact times and the average number of active
 268 contact points during a contact are listed in Table 2 according to the
 269 type of motion. The absence of contact detection resulted in a null
 270 estimated external force and therefore a high error when the foot
 271 was actually in contact with the ground. The global equilibrium
 272 of the biomechanical model obtained from the RNEA algorithm
 273 generated dynamic residuals generated by kinematics and model
 274 inaccuracies [25], in addition to the external forces. If a contact
 275 was detected improperly, the method computed external forces to
 276 balance the residuals even if no actual force was measured.

277 The GRF&M were estimated for each trial using each contact de-
 278 tection method with the optimal parameter values. Component by
 279 component, the estimated GRF&M were compared to the GRF&M
 280 measured by the force platforms in Figure 4 (moments are ex-
 281 pressed at the origin of the platforms).

282 The RMSEs obtained were normalized according to the mass of
 283 the participants for comparison with the literature in Table 3.

4 Discussion

284 The current study aimed at comparing two contact detection
 285 methods for GRF&M estimation. A parametric study was per-
 286 formed to find the best set of parameters to be used for the type of
 287 trials studied (walks, runs, and sidestep cuts).
 288

289 **4.1 Parametric study.** The optimal values of the kinematic
 290 thresholds presented in [8] and [1] were $z_0 = 0.05$ m and
 291 $v_0 = 1$ m.s⁻¹ for the study of various sports-related movements,
 292 and corresponded to the optimal values of the thresholds for the
 293 walking trials in our study. Sidestep cuts and runs involved more
 294 acceleration quantities than walking: the norm of the ground reac-
 295 tion force was significantly greater than the norm of the resultant
 296 of the forces corresponding to the action of gravity. The optimal
 297 value of the velocity threshold for these movements was logically
 298 higher than the optimal value of the velocity threshold for walking
 299 in our study.

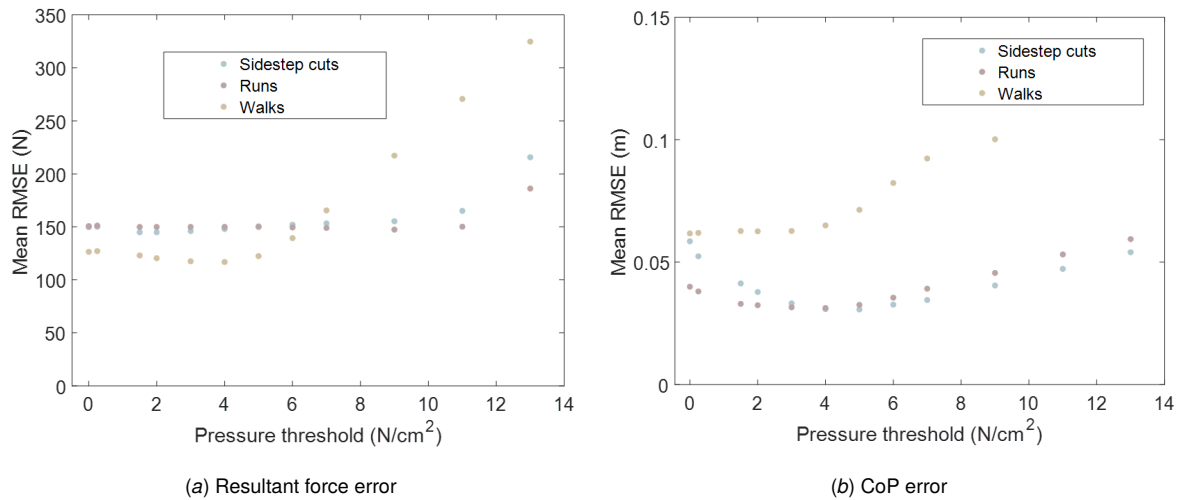


Fig. 3 Accuracy of the external force estimate according to the pressure threshold used.

TABLE 1 Resultant error and CoP position error for each movement and contact detection method.

Contact detection method	Sidestep cut		Run		Walk	
Kinematic threshold ($z_o=50\text{mm}$ et $v_0 = 3\text{m}\cdot\text{s}^{-1}$)	94 mm	147 N	48 mm	144 N	62 mm	113 N
Pressure threshold ($p_0 = 4\text{N}\cdot\text{cm}^{-2}$)	31 mm	148 N	31 mm	150 N	65 mm	117 N
Permanent contact	103 mm	264 N	95 mm	264 N	87 mm	177 N

300 **4.2 Contact detection.** In [22], the authors estimated the dura- 334
 301 tion of the contact phases between 0.69 s and 1.00 s. Our study 335
 302 estimated the duration of contact phases for walking at 0.5 s. The 336
 303 difference may be explained by the elimination of the double stance 337
 304 phase at the end and/or beginning of the gait cycle if, in our study, 338
 305 it was performed with both feet on the same platform. The duration 339
 306 of certain contact phases did not correspond to complete contact 340
 307 phases of the gait and cannot be interpreted as such. They can 341
 308 however be compared according to the contact detection method.
 309 Differences in contact time for walk trials may also be explained
 310 by the stride modification of the subjects to avoid double contact
 311 phases on a single platform.

312 Sidestep cuts and runs are more dynamic movements than walk- 342
 313 ing, with shorter contact times. The average contact duration for 343
 314 running (0.25 s with kinematic threshold detection and 0.24 s with 344
 315 pressure threshold detection) was comparable to the durations esti- 345
 316 mated in [26]: the authors estimated the average duration of contact 346
 317 phases during the runs at 0.25 s using a contact detection method 347
 318 based on thresholds on vertical force measured by a force platform. 348

319 In [23], contrary to our results, the authors described a signifi- 349
 320 cant difference between their results obtained from insole data and 350
 321 the use of kinematic thresholds for event detection during walks. 351
 322 This difference can be explained by the fact that the authors ex- 352
 323 ploited the number of active pressure cells in the pressure insole 353
 324 to detect the contact instants. 354

325 Both contact detection methods detected similar contact dura- 355
 326 tions (Table 2), but the kinematic threshold method detected con- 356
 327 tact over the entire foot, in a more global way than the pressure 357
 328 threshold method, which detected contact with more finesse lo- 358
 329 cally. This phenomenon can be seen in Figure 5 where there was 359
 330 two alternatives phases for the contact detection method with kine- 360
 331 matic thresholds : a phase with zero contact points detected as 361
 332 active, and a phase where all the points under the foot are detected 362
 333 as active. For the pressure threshold contact detection method, 363
 364
 365

334 there was a phase with zero contact points and a phase with a fluctu- 335
 336 ating number of active contact points. Walking is characterized 337
 338 by the foot rolling over the ground, which the kinematic threshold 339
 340 detection method did not detect compared to the pressure threshold 341
 342 method. Such observation may militate to develop a more detailed
 343 model of the foot to test its capability to discriminate the contact
 344 zones of the foot during the gait with regard to the current method,
 345 or to individualize the kinematic thresholds per contact point. 346

347 **4.3 Estimation accuracy.** Considering the CoP position esti- 348
 349 mation accuracy, [8] estimated the mean RMSE to be 25 mm along 349
 350 the anteroposterior axis and 9 mm along the mediolateral axis for 350
 351 running and 23 mm along the anteroposterior axis and 9 mm along 351
 352 the mediolateral axis for walking. The difference with our results 352
 353 may be explained by different experimental conditions: in [8], partic- 353
 354 ipants moved on a treadmill which should affect the length of 354
 355 CoP trajectories along each axis. 355

356 Considering the GRF&M estimation accuracy, the differences in 356
 357 RMSE between the results obtained in our study and in [9] may be 357
 358 related to the difference in the movements studied: the movements 358
 359 in our study are more dynamic than manual handling tasks. We 359
 360 compared our results obtained in running with those in [8] obtained 360
 361 for movements at a speed of $3\text{m}\cdot\text{s}^{-1}$; we compared our results in 361
 362 walks with those obtained for a movement at $1.4\text{m}\cdot\text{s}^{-1}$. Our study 362
 363 did not include tasks comparable to the squat and step-up tasks 363
 364 studied in [1]. AP and ML components may also be affected by 364
 365 the lack of minimization of the internal forces during the motion 365
 [27].

366 **4.4 Perspective of use.** The search for optimal values for the 366
 367 kinematic thresholds common to all the movements studied nec- 367
 368 essitated a deterioration in the accuracy of the external force es- 368
 369 timate compared with the minimum value obtained with another 369
 370 set of kinematic thresholds (for walk trials, the RMSE on the re- 370

Table 2 Average duration of contact phases and average number of active contact points during a contact phase according to the contact detection method and the movement studied.

	Contact duration (s)			Mean number of active contact points	
	Kinematic threshold	Pressure threshold	Plateforme	Kinematic threshold	Pressure threshold
Sidestep cut	0.28 ± 0.04	0.27 ± 0.04	0.28 ± 0.04	10.6 ± 1	8.1 ± 0.7
Run	0.25 ± 0.03	0.24 ± 0.03	0.24 ± 0.03	10.8 ± 1	8.5 ± 0.8
Walk	0.50 ± 0.06	0.48 ± 0.01	0.43 ± 0.03	11.4 ± 1	5.0 ± 0.7

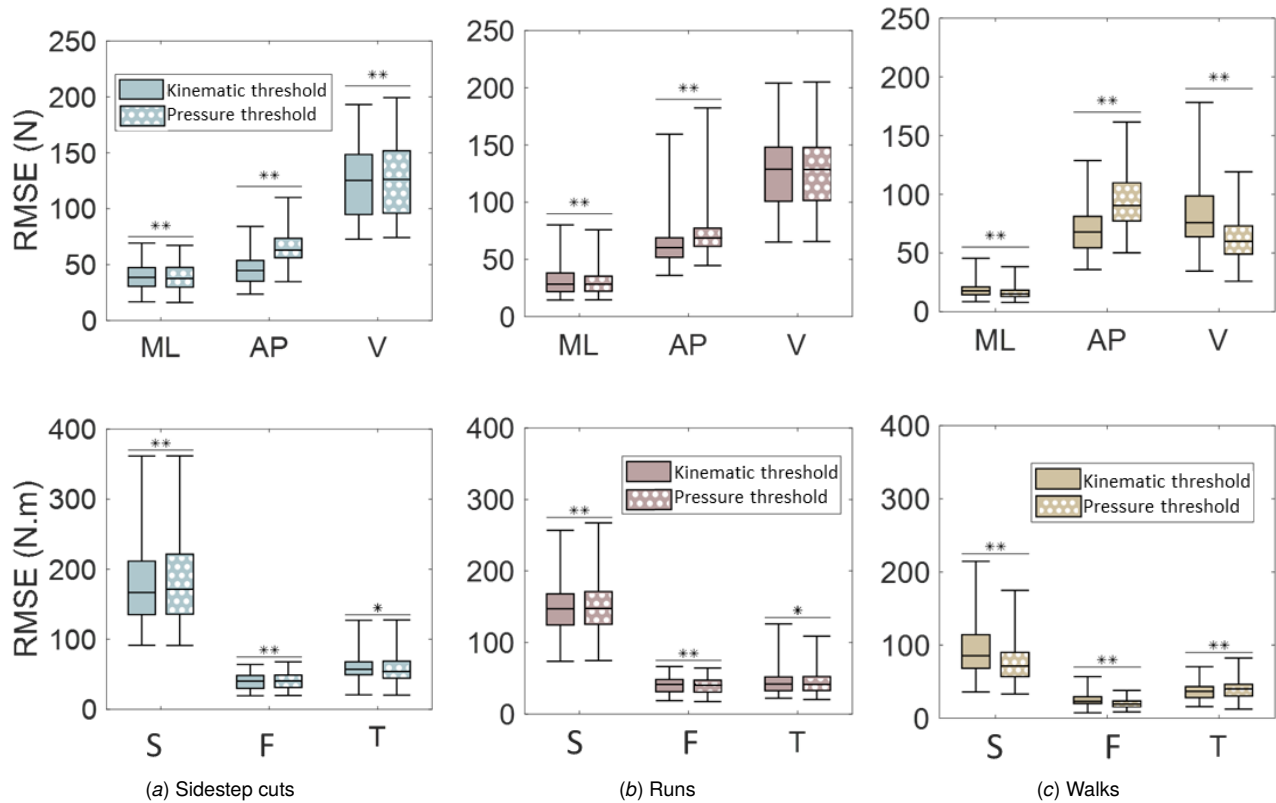


Fig. 4 RMSE between the estimated GRF&M and the GRF&M measured by the force platforms according to the contact detection method. The pattern in the boxes differentiates the contact detection method used. The RMSE for each component of the GRF&M is represented: the resultant along the medial-lateral axis (ML), along the anterior-posterior axis (AP), along the vertical axis (V) and the axis moment normal to the frontal plane (F), to the sagittal plane (S), to the transverse plane (T). Pairwise comparison (Wilcoxon) are indicated by “**” for $p < 0.001$ and “*” for $p < 0.01$.

366 sultant force was 13% higher than its minimum value). A position
 367 threshold of $z_0 = 0.05$ m and a velocity threshold greater
 368 than $v_0 = 3$ m.s⁻¹ as well as a position threshold greater than
 369 $z_0 = 0.05$ m and a velocity threshold of $v_0 = 3$ m.s⁻¹ make it
 370 possible to obtain an accuracy of estimation of the external error
 371 comparable to the accuracy obtained with the set of parameters
 372 $z_0 = 0.05$ m and $v_0 = 3$ m.s⁻¹. Contact detection can therefore be
 373 implemented using a single kinematic threshold, either in position
 374 or velocity. This result makes it possible to envisage other exper-
 375 imental conditions for contact detection, based on other technol-
 376 ogies: for example, an inertial measurement unit (IMU) measures
 377 the acceleration of the foot over time and, by integration, the speed
 378 of the foot, which is sufficient in some cases to detect contact. By
 379 using a single position threshold, contact can be detected using
 380 distance sensors between the foot and the ground.

381 For the contact method using pressure threshold, the low value
 382 of $k_{threshold}=1.06$ suggested using a common pressure threshold
 383 for all the studied movements. The use of a single threshold means
 384 that tests involving different types of movement can be studied.
 385 The estimation of the external forces with pressure insoles can be

386 implemented on mobile floors, of different heights to study the
 387 ascent of steps for example.

388 None of the contact detection methods consistently performed
 389 better on all GRF&M components. The pressure threshold contact
 390 detection method constrained the minimization problem more than
 391 the kinematic threshold method by systematically detecting fewer
 392 contact points during contact phases. This had no significant impact
 393 on the overall accuracy of the method. The use of sole data to
 394 detect contact allowed us to know more precisely which areas
 395 of the foot were in contact during movement. As a result, the error
 396 in estimating the position of the CoP was lower than with the
 397 kinematic threshold method. Nevertheless, the accuracy obtained
 398 in estimating the COP using a contact detection method based on
 399 a pressure threshold was inferior to estimating the position of the
 400 CoP based on its direct measurement by the insole [14].

401 **4.5 Limitations and perspectives.** The kinematic thresholds
 402 used were equal for all the contact points placed under the foot
 403 and therefore at different heights (effect linked to the shape of
 404 the shoes and soles). Each contact point had its own trajectory.

Table 3 Comparative table of RMSEs normalized by the weight of participants between external forces estimated and measured by force platforms according to different studies.

Reference	Motion	V (N/kg)	AP (N/kg)	ML (N/kg)
Kinematic thresholds	Sidestep cut	1.79	0.67	0.57
	Run	1.82	0.88	0.46
	Walk	1.15	0.98	0.26
Pressure threshold	Sidestep cut	1.80	0.94	0.55
	Run	1.81	1.02	0.44
	Walk	0.88	1.34	0.23
[1]	Walk	0.68	0.30	0.19
	Squat and step up	0.70	0.24	0.29
[8]	Walk	0.94	0.42	0.17
	Run	2.45	0.69	0.19
[9]	Handling task	0.51	0.22	0.19

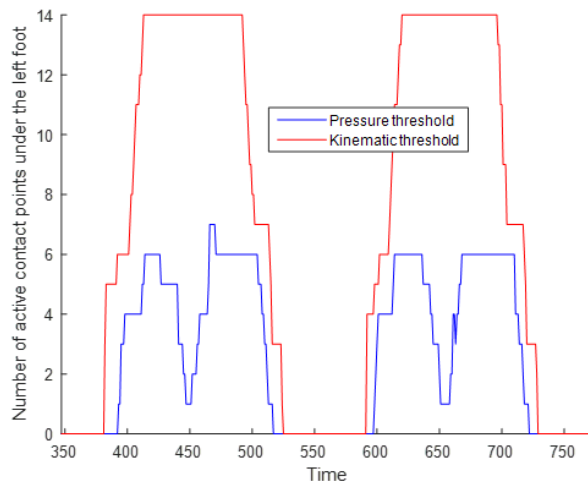


Fig. 5 Example of contact detection during a walking trial under the participant's left foot using the kinematic threshold (red) and pressure threshold (blue) contact detection method.

this study with regard to the kinematic results.

Each component of the external force on each solid (right foot, toes of the right foot, left foot and toes of the left foot) was filtered with a cut-off frequency of 5 Hz. According to [18], this cut-off frequency is suitable for studying human movement but degrades the information at the instants when contact begins and ends. The use of a filter with a higher cut-off frequency or an adaptive filter such as a Kalman filter could be considered. Other smoothing techniques can be used to improve the prediction results during these phases too [10].

5 Conclusion

Two contact detection methods were evaluated on different displacement movements. Contact detection can be based on the use of kinematic thresholds: contact is detected if the foot is close to the ground and not moving. This method can be used with just one of these two criteria, chosen according to the experimental constraints. Contact detection using pressure insoles data can be deployed outside the laboratory. The value of the threshold does not vary according to the movement studied: the study of sequences comprising different movements can be considered. Using insole data to detect contact provides a better estimate of the CoP compared to estimating the CoP with a contact detection method based on foot kinematics. The two contact detection methods demonstrated comparable accuracy in terms of estimating the magnitude of the external forces whereas exhibiting different accuracy component per component.

Acknowledgments

This study was partially supported by the ANR within the framework of the PIA EUR DIGISPORT project (ANR-18-EURE-0022). This work was partially supported by French government funding managed by the National Research Agency under the Investments for the Future program (PIA) with the grant ANR-21-ESRE-0030 (CONTINUUM project).

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