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# Elastic Rods for Fluid Dance Movements Modeling

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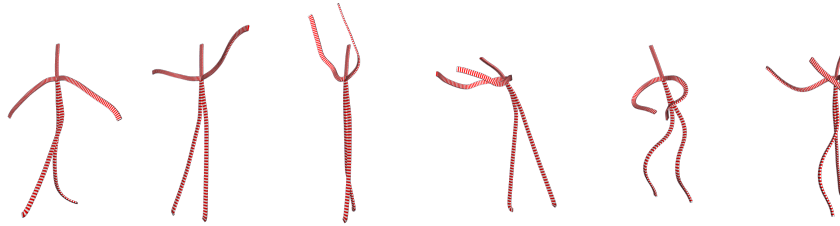


Figure 1: Our model in different poses of the dance

## Abstract

We present a new abstract representation of choreographic motion that conveys the typical fluidity of modern dances, such as those by Isadora Duncan, better than traditional human-like or skeleton-based representations. Our model is formed by five flexible ribbons joining at the solar plexus and is animated from motion capture data using an optimization-based algorithm.

## CCS Concepts

•Human-centered computing → Visualization; •Computing methodologies → Animation;

## 1. Introduction

Isadora Duncan's choreography is one of the foundation of modern dance. In her work, Duncan wanted to uncover what she described as "the natural movement". In her definition, natural movement is unrestricted, respecting both the structure of the body and the pull of gravity: "Such movements will always have to depend on and correspond to the form that is moving" [Dun28]. That is, each movement performed is seen through the lens of a dancer's body. In her "natural movement" philosophy, she also expressed that the center of movement and energy is the solar plexus.

Unfortunately, Isadora Duncan always refused to be filmed, because she thought that the frame rate of the camera at the time (about 24 frames per seconds) was not enough to represent the fluidity of her choreography. Therefore her choreographic knowledge was transmitted mostly orally from one generation of Duncanian dancers to another. Although part of her repertoire has been translated into dance notations (such as Laban and Sutton notations), those notations are hard to decipher and not well known amongst the dance community. One can also wonder if the fluidity of her natural movement can be expressed through such succinct notation.

In this paper we propose a graphical model that represents Duncan's danced choreography while staying as close as possible to her movement qualities and philosophy. To this end, we worked closely

with a professional Duncanian dancer from the third generation of Duncan's students. We recorded the expert as she danced several pieces using motion capture at a high frame rate. Through multiple discussions with our expert, we were able to design a model which stays faithful to Duncan's philosophy and style. Our result is a star-shaped representation made of 5 flexible rods that can bend, twist and stretch and smoothly deform to follow the pre-recorded motion capture markers positions.

## 2. Related Work

### 2.1. Physical models for dance

Previous work has traditionally addressed this issue by introducing physical models of the dancer. Mass-spring systems have been a main part of physical models used to represent motion, especially in dance, as these systems can easily represent the joints and bones of the human skeleton. In particular, Piana et al. [PAN\*16] use mass-spring figures to analyze movement fluidity. Hsieh [Hsi07] creates a new grammar using verbs and adjectives and associate a special mass-spring system to convey motion. Fdili Alaoui et al. [FABJB13] propose an interactive installation to capture the dancer's movements, and run physical simulations to analyze their motion qualities. Our model of elastic rod can be seen as a new contribution to this long line of research.

## 2.2. Dance visualization

Video is one of the first technology to be used by choreographers to represent dance motion, such as Wiliam Forsythe in [FS99, PSF\*09]. However in [Bro89], Brooks demonstrates how the traditional tools of cinematography affect and distort the perception of choreographic movement. Moreover, De Boer et al. [dB-JTAPN18] investigated which representations conveyed movement the best between textual description, 2d animations, 3d animations and auditory description and found that dancers preferred 3d animations. Motion capture has thus emerged as a promising tool for dance representation as it allows to have a precise 3D recording. While the preferred visualization style for motion capture in most previous work is stick figures or human-like avatars, some authors and artists have chosen to explore more abstract visualization styles. D. Poulin and M. Époque developed a concept of “dance without bodies” by using particle animation guided by motion capture data [Szp14]. Astier shows the motion capture markers without revealing the dancers bodies in his movie *Clinamen* [Arc20]. Our method is a new way of using motion capture data to represent dance in an abstract way.

## 3. Input Data

The input of our model is a prerecorded dance captured using a motion capture system. Our mocap set-up relies on 64 spherical trackers (markers) whose positions in the 3d space is recorded at 100 frames per second (see Figure 2 for an illustration of the marker locations).

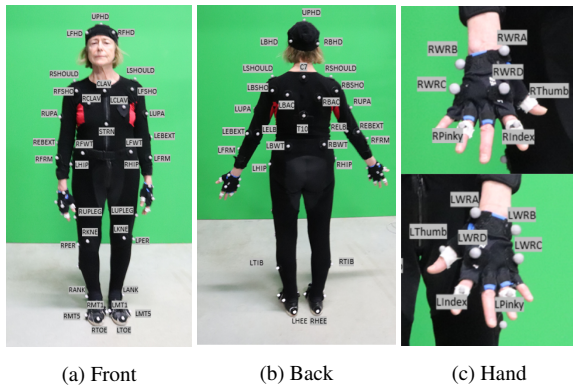


Figure 2: Positions of the markers on the dancer’s body.

## 4. Modeling the dancer

Our model of the dancer was co-designed with an expert Duncanian dancer of the third generation, following the general principles of natural movement, as expressed by Isadora Duncan in her autobiography [Dun27] and other writings [Dun28]. In her autobiography Duncan describes her attempts to find “the central spring of all movement” and her discovery that it should be located in the solar plexus : “I know only one dance and it is this movement: drawing back your hands to the solar plexus, whereupon an inner force opens up your arms and raises them” [Dun27].

## 4.1. Dancer Representation

Taking into account the above requirements expressed by our expert dancer, we propose to model the dancer’s body as an abstract figure in the shape of a starfish, with five ribbons attached together at the solar plexus. Using ribbons instead of a rigid skeleton would follow the fact that the dance of Isadora Duncan is unconstrained to one’s body. We also hope that it will convey the fluidity of the movement better, as rods are not restricted to bend and twist at a fixed set of locations only (the joints of a skeleton). In practice, our ribbons are modeled as isotropic rods, i.e. have a circular cross-section, which let them equally bend and twist in any direction. However, we *display* them as *flat* ribbons to better visualize their twist.

### 4.1.1. Natural shapes of rods’ centerlines

We assume that the natural shape (ie. shape at rest) of the rod is straight, so as not to favor any particular direction for bending and twisting. We define the natural shapes of the rods by using the mocap data when the dancer takes a T-pose. It is a pose most mocap systems ask the user to take to calibrate the system and is present at the beginning of all our recordings. Therefore, using this pose allows us to make sure that the natural shape of our rods is consistent across all animations, while exhibiting low bending of the limbs, which is coherent with our assumption for the rods to be straight at rest.

We process each limb (arms and legs) and the head separately and create a rod for each. To this end, we first manually group all the markers according to their body location. To make sure all rods join at the solar plexus we precompute the position of the later (defined, in our implementation, as the midpoint between the markers CLAV and C7, as labelled in Figure 2) and make the centerline of our rod - a straight segment in our case - start at this position. To define the direction of the segment, we perform principal component analysis on the positions of the markers of the group associated to the body part being processed and use the vector associated to the largest variance. Finally, we size the segment by projecting all the markers of the group onto the line defined by the solar plexus and the direction computed above and set as segment’s end point the projected point furthest away from the solar plexus.

### 4.1.2. Orientation of the ribbons in the natural pose

Since we process each group separately, there is no guarantee that the obtained centerlines pass through a common plane, and, in practice, the arms are indeed slightly tilted forward. As we still want our ribbons to be orientated consistently, we rotate them around their respective centerlines so that their normals are as close as possible to a common vector, chosen to be the normal to the solar plexus and defined as the normal to the plane passing through the markers RCLAV, LCLAV and CLAV.

## 4.2. The Discrete Elastic Rod model

In order to deform and animate our ribbons, we need to associate them to a numerical physical model for rods. We choose *Discrete Elastic Rods* [BWR\*08], a discrete geometric model for the simulation of elastic rods that can stretch, bend and twist. In this model,

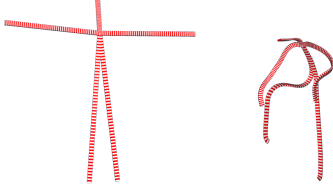


Figure 3: Left: natural pose, Right: deformed pose

134 a rod is defined by a centerline, and a set of material frames, track-  
 135 ing the rotations of the rods' cross-sections around the centerline  
 136 with respect to an untwisted rod configuration. The vertices of the  
 137 centerline  $\Gamma$  will be denoted by  $(x_i)_{i \in [0, n+1]}$  and its edges  $e^i =$   
 138  $x_{i+1} - x_i$ ,  $i \in [0, n]$ . The set of material frames  $M^i = \{t^i, m_1^i, m_2^i\}$  are  
 139 defined per edge, and are considered to be adapted to the centerline  
 140 curve, that is  $t^i = e^i / \|e^i\|$ . The rotation angle with respect to the  
 141 untwisted reference frame  $\{t^i, u^i, v^i\}$  at is denoted  $\theta^i$ . Throughout  
 142 this paper, we will use the following convention: lower (resp. upper)  
 143 indices refer to quantities associated to a vertex  $x_i$  (resp. edge  
 144  $e^i$ ). Three types of energies are associated to the rod :  $E_{bend}(\Gamma)$  and  
 145  $E_{stretch}(\Gamma)$  which depend on the  $x_i$  in the case of a straight isotropic  
 146 rod and  $E_{twist}(\Gamma)$  which depends on the  $\theta^i$  in the case of a straight  
 147 isotropic rod (see more details in [BWR\*08]).

## 148 5. From mocap to dancing rods

149 We want the rods to follow the dancer's movements. To achieve  
 150 this, we connect each ribbon to the different markers associated to  
 151 it using springs. We want to be able to determine the position of  
 152 the ribbon and its orientation at each time frame. To do so we will  
 153 minimize the total energy of the physical model which combines 2  
 154 types of energies: the energy associated to the ribbon's internal de-  
 155 formation (twist, bend and stretch) and the energy associated with  
 156 the springs that were attached to the ribbon.

### 157 5.1. Adding energies to follow the dance

158 In this section, we introduce energies which will enable the rod to  
 159 follow the data (i.e. the markers positions) and therefore to match  
 160 the dancer's movement closely. We use two kinds of energies: the  
 161 linear position energy and the angular position energy. For that pur-  
 162 pose we will introduce springs between each marker and its pro-  
 163 jection onto the ribbon. Therefore the total energy of our ribbon  
 164 becomes  $E(\Gamma) = E_{bend}(\Gamma) + E_{twist}(\Gamma) + E_{stretch}(\Gamma) + E_{linear}(\Gamma) +$   
 165  $E_{angular}(\Gamma)$ . In the following section, we denote  $s_k$  the position at  
 166 current time of marker number  $k$ .

#### 167 5.1.1. Linear spring associated with data

168 Each marker is associated to an edge. At time  $\tau = 0$  we project  
 169 the marker  $\bar{s}_k$  onto the centerline. This projection gives a point  $\bar{c}_k$   
 170 which belongs to the edge  $\bar{e}_{i_k}$  as displayed in Figure 4. We express  
 171  $c_k$  with respect to the two vertices of the edge  $x_{i_k+1}$  and  $x_{i_k}$  using  
 172 barycentric coordinates :  $c_k = y_k x_{i_k} + (1 - y_k) x_{i_k+1}$  with  $y_k \in [0, 1]$ .  
 173 We denote  $z^k = s_k - c_k$ . The energy associated to a marker  $s_k$  is  
 174 then :

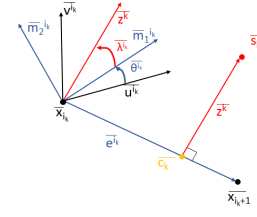


Figure 4: Angular spring connecting a marker to an edge

$$E_{linear}(\Gamma) = \sum_{k=0}^p E_{linear}(e^{i_k}) = \frac{1}{2} \sum_{k=0}^p a_k (\|\bar{z}^k\| - \|z^k\|)^2,$$

175 where  $a_k$  is the rigidity of the spring.

#### 176 5.1.2. Angular spring associated with data

We want the angular difference between the marker and its asso-  
 ciated edge to remain constant in order for a change of angle to  
 impact the position of the material frame. We therefore evaluate  
 the rotation around the tangent  $t^{i_k}$ . For that purpose, we first project  
 $z^k$  to the reference frame  $u^{i_k}$  and  $v^{i_k}$  :  $w^k = (z^k \cdot u^{i_k})u^{i_k} + (z^k \cdot v^{i_k})v^{i_k}$ .  
 Then we denote  $\lambda^{i_k}$  the minimum angle required to move  $m_1^{i_k}$  to  $w^k$   
 see Figure 4. The energy for this angular spring associated with the  
 edge  $e^{i_k}$  is  $E_{angular}(e^{i_k}) = \frac{1}{2} q_k (\widehat{\lambda}^{i_k} - \lambda^{i_k})^2$ , where  $q_k$  is the rigid-  
 ity of the spring. We want to express this angle with respect to  
 $\theta$ . We denote  $\widehat{u}^{i_k} z^k$  the angle between  $u^{i_k}$  and  $z^k$ . We then have  
 $\lambda = \widehat{u}^{i_k} z^k - \theta^{i_k}$ . The total energy can then be written as

$$E_{angular}(\Gamma) = \frac{1}{2} \sum_{k=0}^p q_k (\widehat{u}^{i_k} z^k - \theta^{i_k} - \widehat{u}^{i_k} z^k + \theta^{i_k})^2.$$

### 177 5.2. Enforcing an orientation

178 Throughout the simulation, we want the different rods to remain  
 179 joined at the plexus. This translates into the following constraints  
 180 :  $e^0 = p$ , where  $p$  is the current position of the plexus as defined  
 181 in Section 4.1. We also want to ensure that the orientation of the  
 182 material frame and the reference frame remain stable to avoid over-  
 183 twisting of the rods. To this end, we will ask the second vector  
 184 of the reference frame of each rod at the solar plexus,  $v_0$ , to align  
 185 as closely as possible to the normal  $n$  at the solar plexus, i.e. we  
 186 will ask  $v_0$  to match the normal  $n$  when projected onto the plane  
 187 of the rod's cross section, orthogonal to the tangent  $t_0$ . We then ask  
 188 the initial material frame to match the reference frame using the  
 189 constraints  $\theta^0 = 0$ .

### 190 5.3. Procedure to create motion

We consider that at each time frame the rod is at a state of equi-  
 librium, i.e. a state that minimizes its total energy, which enables  
 to perform optimization on the energy function. Therefore, at each  
 time step we want to find the optimal rod which minimizes its total  
 energy.

Since we decided to have a straight isotropic rod, each energy  
 term either depends on the position of the centerline ( $x_i$ ) or on the

angles of the material frames  $\theta_i$ . We recall that the total energy of the system is

$$E(\Gamma) = E_{bend}(\Gamma) + E_{twist}(\Gamma) + E_{stretch}(\Gamma) + E_{linear}(\Gamma) + E_{angular}(\Gamma).$$

We know that  $E_{bend}(\Gamma)$ ,  $E_{stretch}(\Gamma)$  and  $E_{linear}(\Gamma)$  depend only on the position of the centerline whereas  $E_{twist}(\Gamma)$  and  $E_{angular}(\Gamma)$  depends on the angles  $\theta^i$ .

This lets us treat the optimization of the two sets of variables independently. Since the reference frame is necessary to evaluate the angular spring energy and depends on the centerline position (because it is adapted), we first find the optimal centerline position and then we find the optimal position of the material frame as shown in Algorithm 1. The variables for the first optimization problem are the vertices  $x_i$  and the variables for the second problem are the  $\theta^i$ . In order to solve the optimization problem we used a Newton's method from the Ipopt library [WB06]. To speed optimization, we use the solution corresponding to the previous time frame as the starting state of Newton's method for the current time frame. Finally, each rod is treated as an independent problem.

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**Algorithm 1:** Simulation steps for one rod
 

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**input :** Set of markers

**output:** Animated rod

- 1 Create initial rod;
  - 2 **for** each time frame **do**
  - 3     Find optimal  $(x_i)_{i \in [0, N]}$  and set centerline;
  - 4     Compute and set reference frames;
  - 5     Find optimal  $(\theta^i)_{i \in [0, N-1]}$  and set material frames;
- 

## 5.4. Implementation

We implemented this method in C++ using Ipopt [WB06] library for the optimization, Eigen [GJ\*10] for linear algebra, Mapple software to compute the Hessian and gradient of the functions and libigl for visualization [JP\*18].

## 6. Experimental results

We evaluated our system on a set of 6 dances (*Prelude*, *Moment Musical*, *Folatrerie*, *Etude Revolutionnaire*, *Water Study* and *Mother*), recorded twice (except *Water Study*) all choreographed by Isadora Duncan and performed by our expert dancer, giving us a total of 11 recordings. We assess our model by looking at the data produced during the process described by Algorithm 1.

### 6.1. Number of segments

With this model, we have the choice of the number of segments used to discretize the rods. Figure 5 shows the resulting ribbons corresponding to different discretizations. We also have the freedom to create a skeleton like figure as shown in Figure 5 (a) by using ribbon edges of different sizes. A rod, in the continuous setting, is smooth and can bend at any location. Such a behavior can be approximated by using a high number of segments. We decided to go with 100-edge ribbons that offered a good trade-off between smoothness and tractability (see Figure 5 (d)).

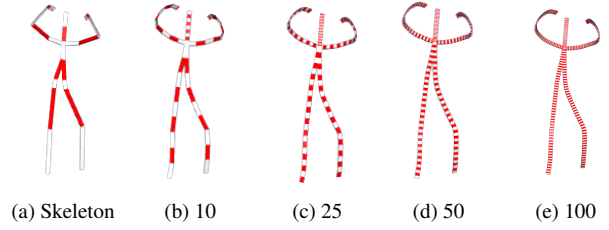


Figure 5: Output ribbons corresponding to the same input data but different number of segments

### 6.2. Weights of the energy terms

We also need to set the stiffnesses of the different energies that we use in our formulation ( $\eta$  for stretch,  $\beta$  for twist,  $\alpha$  for bend,  $a_k$  for linear data and  $q_k$  for angular data). The more weight we put on the data terms, the closer to the data the rods will be, and the highest the weights of the rods' energies the smoother the rods are going to be. We found that the best tradeoff for a smooth yet close to the data rod was choosing  $\eta = \alpha = \beta = 100$  and  $a_k = q_k = 0.1$ .

### 6.3. Energies Analysis

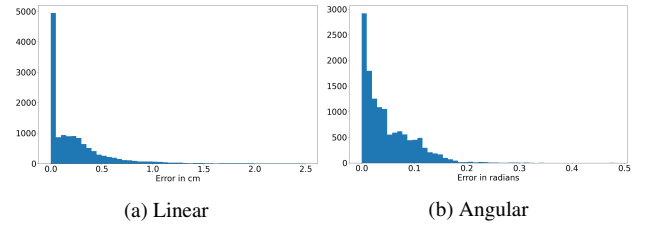


Figure 6: Histogram of total linear/angular energy for *Folatrerie*

We also looked at the error related to the input data to know how far our model is from our source data, measured via our linear and angular energies. In Figure 6a, we can see that most errors are between 0 and 0.05 cm and are majored by 2.5 cm. This means the total linear displacement in *Folatrerie* for any time frame for all ribbons is at most 2.5 cm. In Figure 6b we can see that the angular displacement is mainly between 0 and 0.05 radians. We conclude that our rods remain close to the input markers, ensuring that they follow the dance closely.

## 7. Conclusion

In this paper we presented a new visualization method for dance motion, with the special goal of transmitting important principles in Isadora Duncan's dance heritage. Our method was co-designed with Duncan experts. As a result, we are now planning to create and distribute a novel corpus of Duncan dances, acquired with modern motion capture techniques and displayed as dancing elastic rods, for use by Duncan scholars and students. The new visualization appears to be much more readable than the traditional dance notations (Sutton, Laban) used to transcribe the choreographic style of Isadora Duncan in the past.

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