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On Strict Homogeneous Lyapunov Function for Generalized Homogeneous PI Controller

Yu Zhou, Andrey Polyakov, Gang Zheng

Abstract—This paper investigates a generalized homogeneous PI (Proportional-Integral) control for a linear plant. A Lyapunov function for analysis of the closed-loop system is designed. For negative homogeneity degree, the obtained Lyapunov function becomes a strict Lyapunov function allowing an advanced analysis to be provided. In particular, a class of the disturbances to be rejected by the control law is characterized, a maximum control magnitude and the settling-time of the closed-loop system are estimated.

I. INTRODUCTION

The integral term in a linear controller is introduced to reject non-vanishing perturbations. PI controllers have been applied in various fields due to the relative simplicity and robustness, in addition to satisfactory performance. The PI controller design in frequency domain is well-developed for SISO (single input single output) linear system. For the MIMO (multiple-input and multiple-output) linear system, the PI parameters can be tuned using LMIs. The integral term also works for nonlinear control design [24], [19], [7], [11], [12]. As known, a memoryless discontinuous controller (e.g. sliding mode algorithm) can also stabilize a system with non-vanishing perturbations. Theoretically compared to continuous integral control, sliding mode control [25] can reject a larger class of bounded perturbations with better robustness properties. But the main problem of a discontinuous controller in practice is “chattering”, introducing the integral term may potentially reduce the “chattering” caused by the discontinuity. A classical example of PI integral sliding mode controller is the super-twisting algorithm [14].

Homogeneity is a dilation symmetry. All linear and a lot of essentially nonlinear models of mathematical physics are homogeneous (symmetric) in a generalized sense [21]. Homogeneity is widely used in control theory for system analysis, regulation and observer design ([9], [1], [15], [18], [3], [2], [21]). Homogeneity has some useful features such as: local stability means global one; the rate of convergence of homogeneous system is defined by its homogeneity degree; homogeneous systems are robust with respect to external perturbations and time delays.

Implicit Lyapunov function (ILF) combines two important notions from mathematical and stability analysis: Implicit

function and Lyapunov function. In [28], the design of a homogeneous controller using ILF shows that the ILF makes the gain tune can be reduced to an LMI problem and systematized the control design and analysis.

A weighted homogeneous PI algorithm is designed in [16]. The linear geometric homogeneous PI controller was considered in [21] and utilized for an upgrade of existing linear control law to a generalized homogeneous one. In [27] on real experiments it was shown that such an upgrade may essentially improve the control performance. However, the theoretical analysis of this very efficient control law is not complete. Inspired by [17] we introduce a strict Lyapunov function for the closed-loop system with such a generalized homogeneous PI algorithm. This function allows us to present the missed analysis for the case of negative homogeneity degree.

- We provide an estimate of the magnitude of the homogeneous PI controller under consideration.
- We derive an estimate the settling time of the closed-loop system controlled by the homogeneous PI algorithm with negative degree.
- We characterize a class of perturbations to be rejected by means of the homogeneous PI algorithm.

The main problem of integral control is the saturation since the control signal in integral control is obtained through time integration. Estimating the magnitude and settling time helps solve the wind-up problem and actuator constrained situation. A class of perturbations, that the homogeneous PI controller can reject, shows that the homogeneous PI controller has better robustness properties than the proportional algorithm.

The paper is organized as follows. Section II presents the basic knowledge of the homogeneous systems and the canonical homogeneous norm. Section III recalls the form of homogeneous proportional control. Section IV introduces the homogeneous proportional-integral control and analyzes it via a strictly Lyapunov function. In section V, a simulation of linear MIMO system is used to validate the theorem.

Notation. \mathbb{R} is the set of real numbers, $\mathbb{R}_+ = \{x \in \mathbb{R} : x \geq 0\}$; $\|\cdot\|$ is a norm in \mathbb{R}^n ; $\mathbf{0}$ denotes the zero vector from \mathbb{R}^n ; $\text{diag}\{\sigma_i\}_{i=1}^n$ is the diagonal matrix with elements σ_i ; $P \succ 0$ ($\prec 0$, $\succeq 0$, $\preceq 0$) for $P \in \mathbb{R}^{n \times n}$ means that the matrix P is symmetric and positive (negative) definite (semidefinite); $C(X, Y)$ denotes the space of continuous functions $X \rightarrow Y$, where X, Y are subsets of normed vector spaces; $C^p(X, Y)$ is the space of functions continuously differentiable at least up to the order p ; $\lambda_{\min}(P)$ and $\lambda_{\max}(P)$ represent the minimal and maximal eigenvalue of a matrix

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$P = P^\top$; for $P \succeq 0$ the square root of P is a matrix $M = P^{\frac{1}{2}}$ such that $M^2 = P$.

II. PROBLEM STATEMENT

In this paper, we consider a linear system with perturbations as:

$$\dot{x} = Ax + Bu + g(t, x) \quad (1)$$

where $x \in \mathbb{R}^n$ is the state vector, $u \in \mathbb{R}^m$ is the control input and $g(t, x)$ is the generalized perturbation. The pair of $\{A, B\}$ is controllable.

A memoryless continuous state feedback control can stabilize the system (1) when $g(t, x)$ is a vanishing perturbation. However, it cannot stabilize the system when $g(t, x)$ is a constant or other non-vanishing perturbation. Hence, we aim to design an integral control to reject a class of matched non-vanishing perturbations. The goal of this paper is to design a generalized homogeneous PI controller to stabilize the system (1) with a finite or nearly fixed-time convergence rate by using a *strict Lyapunov function*.

III. HOMOGENEOUS SYSTEMS

A. Linear dilations in \mathbb{R}^n

By definition, the homogeneity is a dilation symmetry [29], [10], [9], [4], [21]. A dilation [6] is a one-parameter group $\mathbf{d}(s)$, $s \in \mathbb{R}$ of transformations satisfying the limit property $\lim_{s \rightarrow s^\infty} \|\mathbf{d}(s)x\| = e^{s^\infty}$, $s^\infty = \pm\infty, \forall x \neq \mathbf{0}$.

Examples of dilations in \mathbb{R}^n are

- Uniform dilation (L. Euler, 18th century): $\mathbf{d}(s) = e^s I$, where I is the identity matrix \mathbb{R}^n ;
- Weighted dilation (Zubov 1958) : $\mathbf{d}(s) = \begin{pmatrix} e^{r_1 s} & \cdots & 0 \\ \cdots & \cdots & \cdots \\ 0 & \cdots & e^{r_n s} \end{pmatrix}$, where $r_i > 0, i = 1, 2, \dots, n$.
- Geometric dilation is a flow generated by unstable C^1 vector field in \mathbb{R}^n (see [10], [8]).

In this paper we deal only with the so-called linear (geometric) dilation in \mathbb{R}^n is defined as follows

$$\mathbf{d}(s) = e^{sG_d} := \sum_{i=0}^{+\infty} \frac{s^i G_d^i}{i!}, \quad s \in \mathbb{R}^n, \quad (2)$$

where $G_d \in \mathbb{R}^{n \times n}$ is an anti-Hurwitz matrix called the generator of the dilation \mathbf{d} .

Definition 1: A dilation \mathbf{d} is monotone if $s \rightarrow \|\mathbf{d}(s)x\|$ is a monotone increasing function for any $x \neq \mathbf{0}$.

It is worth noting that monotonicity of the dilation may depend of the norm in \mathbb{R}^n . Also, any linear dilation in \mathbb{R}^n is monotone [20] provided that the norm in \mathbb{R}^n is defined as follows

$$\|x\| = \sqrt{x^\top P x}, \quad PG_d + G_d^\top P \succ 0, P \succ 0. \quad (3)$$

B. Canonical Homogeneous Norm

The linear dilation introduces an alternative norm topology in \mathbb{R}^n by means of a homogeneous norm (see, e.g., [5] for an example of a homogeneous norm induced by the weighted dilation).

Definition 2: [20] The functional $\|\cdot\|_d : \mathbb{R}^n \rightarrow [0, +\infty)$ defined as $\|\mathbf{0}\|_d = 0$ and

$$\|u\|_d = e^{s_u}, \quad \text{where } s_u \in \mathbb{R} : \|\mathbf{d}(-s_u)u\| = 1,$$

is called the canonical homogeneous norm in \mathbb{R}^n , where \mathbf{d} is a monotone dilation in \mathbb{R}^n .

For any linear monotone dilation in \mathbb{R}^n , the canonical homogeneous norm is continuous on \mathbb{R}^n and locally Lipschitz continuous on $\mathbb{R}^n \setminus \{\mathbf{0}\}$. Moreover, it is differentiable on $\mathbb{R}^n \setminus \{\mathbf{0}\}$ provided that $\|\cdot\|$ is given by (3) (see, [20]):

$$\frac{\partial \|x\|_d}{\partial x} = \|x\|_d \frac{x^\top \mathbf{d}^\top (-\ln \|x\|_d) P}{x^\top \mathbf{d}^\top (-\ln \|x\|_d) P G_d \mathbf{d} (-\ln \|x\|_d) x}. \quad (4)$$

C. Homogeneous Systems

Definition 3: A vector field $f : \mathbb{R}^n \rightarrow \mathbb{R}^n$ (resp. a function $h : \mathbb{R}^n \rightarrow \mathbb{R}$) is said to be \mathbf{d} -homogeneous of degree $\mu \in \mathbb{R}$ if

$$f(\mathbf{d}(s)) = e^{\mu s} \mathbf{d}(s) f(x), \quad \forall x \in \mathbb{R}^n, \quad \forall s \in \mathbb{R},$$

$$\text{(resp. } h(\mathbf{d}(s)) = e^{\mu s} h(x), \quad \forall x \in \mathbb{R}^n, \quad \forall s \in \mathbb{R}),$$

where \mathbf{d} is a linear dilation in \mathbb{R}^n .

In [20] it is shown that any \mathbf{d} -homogeneous system

$$\dot{x} = f(x), \quad t > 0, \quad x(0) = x_0 \in \mathbb{R}^n \quad (5)$$

is diffeomorphic on $\mathbb{R}^n \setminus \{\mathbf{0}\}$ to a standard homogeneous system. This means that many important results known for standard and weighted homogeneous systems hold for linear homogeneous systems as well. Following theorem is the straightforward corollary of Zubov-Rosier theorem on homogeneous Lyapunov function [29], [23].

Theorem 1: Let f be a continuous \mathbf{d} -homogeneous vector field of degree $\mu \in \mathbb{R}$. The system (5) is globally asymptotically stable if and only if there exists a positive definite \mathbf{d} -homogeneous function $V : \mathbb{R}^n \rightarrow [0, +\infty)$ such that $V \in C(\mathbb{R}^n) \cap C^1(\mathbb{R}^n \setminus \{\mathbf{0}\})$ and

$$\dot{V}(x) \leq -\rho V^{1+\mu}(x), \quad \forall x \neq \mathbf{0}.$$

The latter theorem immediately implies that asymptotically stable homogeneous system (5) is

- globally uniformly finite-time stable¹ for $\mu < 0$, and $T(x_0) \leq \frac{1}{-\rho^\mu} V_0^{-\mu}$, where $V_0 = V(x_0)$;
- globally uniformly exponentially stable for $\mu = 0$;
- globally uniformly nearly fixed-time stable² for $\mu > 0$, $T_{\max} = \frac{1}{\rho \mu r^\mu}$.

D. Proportional Homogeneous Control for Linear Plants

Let us consider the special linear control system of (1) as

$$\dot{x} = Ax + Bu(x) + g(t, x), \quad t > 0, \quad x(0) = x_0 \quad (6)$$

The disturbance-free (i.e., $g = \mathbf{0}$) system (6) is \mathbf{d} -homogeneously stabilizable with a degree $\mu \neq 0$ if and only if the pair $\{A, B\}$ is controllable [28].

¹The system (5) is finite-time stable if it is Lyapunov stable and $\exists T(x_0) : \|x(t)\| = 0, \forall t \geq T(x_0), \forall x_0 \in \mathbb{R}^n$.

²The system (5) is uniformly nearly fixed-time stable if it is Lyapunov stable and $\forall r > 0, \exists T_r > 0 : \|x(t)\| < r, \forall t \geq T_r$ independently of $x_0 \in \mathbb{R}^n$.

Theorem 2: [28] If the linear equation

$$AG_0 + BY_0 = G_0A + A, \quad G_0B = \mathbf{0}. \quad (7)$$

has a solution $G_0 \in \mathbb{R}^{n \times n}$ and $Y_0 \in \mathbb{R}^{m \times n}$ such that $G_0 - I_n$ is invertible, then for any $\mu \neq 0$ such that $G_d = I_n + \mu G_0$ is anti-Hurwitz, the *disturbance-free* system (6) can always be homogeneously stabilized by the following control

$$u(x) = K_0x + \|x\|_{\mathbf{d}}^{1+\mu} K \mathbf{d} (-\ln \|x\|_{\mathbf{d}}) x, \quad K = YX^{-1} \quad (8)$$

with any $\rho > 0$, $\mu \geq -1$, $K_0 = Y_0(G_0 - I_n)^{-1}$ any $X \in \mathbb{R}^{n \times n}$, $Y \in \mathbb{R}^{m \times n}$ by solving the following algebraic system

$$\begin{cases} XA_0^\top + A_0X + Y^\top B^\top + BY + \rho(XG_d^\top + G_dX) = \mathbf{0} \\ XG_d^\top + G_dX \succ 0, \quad X \succ 0 \end{cases} \quad (9)$$

$A_0 = A + BK_0$, where the canonical homogeneous norm $\|\cdot\|_{\mathbf{d}}$ is induced by the norm $\|x\| = \sqrt{x^\top X^{-1}x}$. Moreover, if

$$2 \frac{g^\top(t,x) \mathbf{d}^\top X^{-1} \mathbf{d} (-\ln \|x\|_{\mathbf{d}}) x}{x^\top \mathbf{d}^\top (-\ln \|x\|_{\mathbf{d}}) X^{-1} G_d \mathbf{d} (-\ln \|x\|_{\mathbf{d}}) x} < \rho \|x\|_{\mathbf{d}}^\mu, \quad \forall t \geq 0, \quad (10)$$

then the perturbed system (6) is

- globally uniformly finite-time stable for $\mu < 0$;
- globally uniformly exponentially stable for $\mu = 0$;
- globally nearly fixed-time stable for $\mu > 0$.

□

The proof of this theorem is based on the use of the canonical homogeneous norm as a Lyapunov function of the closed-loop system (6), (8) with $g = \mathbf{0}$:

$$\frac{d}{dt} \|x(t)\|_{\mathbf{d}} = -\rho \|x(t)\|_{\mathbf{d}}^{1+\mu}. \quad (11)$$

The disturbance g rejected by the control law is characterized by the inequality (10), which is obtained from (4) and (11) using

$$\begin{aligned} \frac{d\|x(t)\|_{\mathbf{d}}}{dt} &= -\rho \|x(t)\|_{\mathbf{d}}^{1+\mu} \\ &+ 2\|x\|_{\mathbf{d}} \frac{g^\top(t,x) \mathbf{d}^\top X^{-1} \mathbf{d} (-\ln \|x\|_{\mathbf{d}}) x}{x^\top \mathbf{d}^\top (-\ln \|x\|_{\mathbf{d}}) X^{-1} G_d \mathbf{d} (-\ln \|x\|_{\mathbf{d}}) x}. \end{aligned}$$

The formula (11) implies that the canonical homogeneous norm is a Lyapunov function for the closed-loop system. The feasibility of the algebraic system is proven in [22]. The existence of an appropriate solution for (7) is studied in [28]. It can be shown that for any solution of (7) the matrix $G_0 - I$ is invertible. Moreover, for a sufficiently small $|\mu|$ we have $G_d = I + \mu G_0$ is anti-Hurwitz.

Remark 1: If the matrix A is nilpotent then $K_0 = \mathbf{0}$. In this case, for $\mu = -1$ any solution $x(t, x_0)$ of the closed loop system (6), (8) with the initial condition $x(x) = x_0$ satisfies

$$\begin{aligned} \|u(x)\| &= \|YX^{-1} \mathbf{d} (-\ln \|x\|_{\mathbf{d}}) x\| \\ &\leq \|YX^{-1}\| \cdot \|\mathbf{d} (-\ln \|x\|_{\mathbf{d}}) x\| \\ &= \|YX^{-1}\| < +\infty \end{aligned} \quad (12)$$

This means that the homogeneous proportional control solves the stabilization problem without an unbounded "peaking effect" (see [21, Chapter 1] for more details).

IV. MAIN RESULT: ANALYSIS OF HOMOGENEOUS PI CONTROLLER

We consider a more general class of perturbations. The disturbance function g is assumed to have the following representation

$$g(t, x) = g_1(t, x) + Bp + \int_0^t Bg_2(s, x(s)) ds, \quad t \geq 0 \quad (13)$$

where $g_1 : \mathbb{R}_+ \times \mathbb{R}^n \rightarrow \mathbb{R}^n$ and $g_2 : \mathbb{R}_+ \times \mathbb{R}^n \rightarrow \mathbb{R}^m$ are assumed to be locally measurable unknown functions and $p \in \mathbb{R}^m$ is a constant unknown vector.

Let us consider the following homogeneous PI controller for linear system (6):

$$u(x) = K_0x + u_{\text{hom}}(x) + \int_0^t u_{\text{int}}(x(s)) ds \quad (14)$$

The first step, the proportional part design according to Theorem 2:

$$u_{\text{hom}}(x) = \|x\|_{\mathbf{d}}^{1+\mu} K \mathbf{d} (-\ln \|x\|_{\mathbf{d}}) x \quad (15)$$

where K_0 and K are given in Theorem 2.

In the second step, in the integral controller design, we adopt the resemble form of the integral part, which has been studied in [26]:

$$u_{\text{int}}(x) = \frac{\|x\|_{\mathbf{d}}^{1+2\mu} \tilde{K} \mathbf{d} (-\ln \|x\|_{\mathbf{d}}) x}{x^\top \mathbf{d}^\top (-\ln \|x\|_{\mathbf{d}}) P G_d \mathbf{d} (-\ln \|x\|_{\mathbf{d}}) x} \quad (16)$$

$\tilde{K} \in \mathbb{R}^{m \times n}$ is the gain to be defined.

With the notation

$$x_{n+1} = p + \int_0^t u_{\text{int}}(x(s)) + g_2(s, x(s)) ds$$

the closed-loop system becomes

$$\begin{aligned} \dot{x} &= Ax + B(K_0x + u_{\text{hom}}(x) + x_{n+1}) + g_1(t, x) \\ \dot{x}_{n+1} &= u_{\text{int}}(x) + g_2(t, x). \end{aligned} \quad (17)$$

The system (17) is \mathbf{d} -homogeneous of degree μ for the dilation $\tilde{\mathbf{d}} = \begin{pmatrix} e^{sG_d} & 0 \\ 0 & e^{s(1+\mu)} \mathbf{I}_m \end{pmatrix}$ when $g_1 = 0$ and $g_2 = 0$.

Theorem 3 (The case of constant perturbation): Let $g_1 = \mathbf{0}$, $g_2 = \mathbf{0}$ and the matrices G_d , K_0 , $K = YX^{-1}$, $P = X^{-1}$ be defined as in Theorem 2 for some $\mu \geq -0.5$, $\mu \neq 0$ and some $\rho > 0$, then the closed-loop system (6) and (14) is globally uniformly asymptotically stable provided that $\tilde{K} = Q^{-1} \tilde{Y}$, where the matrix $\tilde{Y} \in \mathbb{R}^{m \times n}$ and the symmetric matrix $Q \in \mathbb{R}^{m \times m}$ satisfy the following system of LMIs:

$$W_1 = \begin{pmatrix} \frac{P}{1+\mu} & \tilde{Y}^\top \\ \tilde{Y} & Q \end{pmatrix} \succ 0, \quad \gamma > 0, \quad (18)$$

$$\begin{pmatrix} -\rho P & \frac{PB + \tilde{Y}^\top}{q_i} + \frac{(\hat{F} - \rho \tilde{F})^\top \tilde{Y}^\top}{2} & \tilde{Y}^\top & \mathbf{0} \\ * & \frac{\gamma B^\top PB}{q_i} + \frac{\tilde{Y} B + B^\top \tilde{Y}^\top}{2} & \mathbf{0} & \tilde{Y} \tilde{F} \\ * & * & -q_i Q & \mathbf{0} \\ * & * & * & -\gamma q_i P \end{pmatrix} \prec 0, \quad (19)$$

where $R = PG_{\mathbf{d}} + G_{\mathbf{d}}^{\top}P \succ 0$, $\hat{F} = A_0 + BK$, $\tilde{F} = ((1 + \mu)I_n - G_{\mathbf{d}})$, $i = 1, 2$ and $q_1 = \lambda_{\min}(P^{-1/2}RP^{-1/2})$, $q_2 = \lambda_{\max}(P^{-1/2}RP^{-1/2})$, then a Lyapunov function of the system (6) and (14) is given by

$$V(\xi) = \frac{1}{2}\xi^{\top} \begin{pmatrix} \frac{P}{1+\mu} & \tilde{Y}^{\top} \\ \tilde{Y} & Q \end{pmatrix} \xi. \quad (20)$$

where $\xi = \begin{pmatrix} \|x\|_{\mathbf{d}}^{1+\mu} \mathbf{d}(-\ln \|x\|_{\mathbf{d}})x \\ x_{n+1} \end{pmatrix}$ and

$$\dot{V}(\xi) \leq -\tilde{\rho}\|x\|_{\mathbf{d}}^{\mu}V(\xi), \quad x \neq 0, \quad (21)$$

where $\tilde{\rho} > 0$ is a positive number dependent of μ, ρ, P, Q and \tilde{Y} .

Remark 2: u_{int} is globally bounded and discontinuous at $x = 0$ if $\mu = -0.5$. For $\mu > -0.5$, the considered system has the continuous right-hand side.

The main idea of the proof of this theorem is to construct a quadratic (with respect to a special vector dependent of using the canonical homogeneous norm) Lyapunov function. In the previous work [26], it was shown that for $\tilde{Y} = 0$ the function (20) is weak Lyapunov function ($\dot{V} \leq 0$) of the closed-loop system with $\tilde{K} = -Q^{-1}B^{\top}P$, so the stability analysis in this case can be based on the LaSalle invariance principle [13].

For $n = 1$ and $\mu = -0.5$ the function (20) coincides with the Lyapunov function introduced in [17] for the super-twisting system, since $\|x\|_{\mathbf{d}} = |x|$ in the scalar case.

For $\mu < 0$ the function (20) is a strict Lyapunov function of the closed-loop system due to (21). Hence, it can be utilized for advanced analysis. For instance, we can estimate the settling time based on (21).

Corollary 1 (Finite-time Stability for $\mu < 0$): Under conditions of Theorem 3 with $\mu < 0$, the closed-loop system is finite-time stable and the setting-time admits the estimate $T : \mathbb{R}^n \rightarrow \mathbb{R}_+$ as

$$T(x) \leq \frac{r^{-\frac{\mu}{2+2\mu}} V^{-\frac{\mu}{2+2\mu}}(\xi_0)}{\tilde{\rho}^{\frac{-\mu}{2+2\mu}}} \quad (22)$$

where $r = \lambda_{\max}(P)/\tilde{\lambda}$ with

$$\tilde{\lambda} = \frac{1}{2}\lambda_{\min} \begin{pmatrix} \frac{P}{1+\mu} & \tilde{Y}^{\top} \\ \tilde{Y} & Q \end{pmatrix}$$

and

$$\xi_0 = \begin{pmatrix} \|x_0\|_{\mathbf{d}}^{1+\mu} \mathbf{d}(-\ln \|x_0\|_{\mathbf{d}})x_0 \\ p \end{pmatrix}.$$

The settling time is a function of the initial condition ξ_0 . Hence the settling time estimate needs to know the maximum magnitude of the constant perturbation.

In most practice, perturbations are always time-varying. Homogeneous control could further minimize the effect of the disturbance. The homogeneous proportional controller has shown that it can reject a class of vanishing-perturbation. The homogeneous PI controller can reject more classes of non-vanishing perturbations. The case of the nonzero disturbances is studied below.

Corollary 2 (The case non-constant perturbations): Let under conditions of Theorem 3 the following inequalities hold:

$$\frac{2|x^{\top} \mathbf{d}^{\top}(-\ln \|x\|_{\mathbf{d}})P\mathbf{d}(-\ln \|x\|_{\mathbf{d}})g_1(t, x)|}{x^{\top} \mathbf{d}^{\top}(-\ln \|x\|_{\mathbf{d}})R\mathbf{d}(-\ln \|x\|_{\mathbf{d}})x} \leq \gamma_1 \|x\|^{\mu} \quad (23)$$

$$\frac{|g_1^{\top}(t, x)\mathbf{d}^{\top}(-\ln \|x\|_{\mathbf{d}})P\mathbf{d}(-\ln \|x\|_{\mathbf{d}})g_1(t, x)|}{4} \leq \tilde{\gamma}_1^2 \|x\|_{\mathbf{d}}^{2\mu} \quad (24)$$

$$|x^{\top} \mathbf{d}^{\top}(-\ln \|x\|_{\mathbf{d}})PBg_2(t, x)| \leq \gamma_2 \|x\|_{\mathbf{d}}^{1+2\mu}, \quad (25)$$

$$q(x) \frac{g_2^{\top}(t, x)Q(B^{\top}PB)^{-1}Qg_2(t, x)}{4} \leq \tilde{\gamma}_2^2 \|x\|_{\mathbf{d}}^{2+4\mu}, \quad (26)$$

where the parameters $\gamma_1, \tilde{\gamma}_1, \gamma_2, \tilde{\gamma}_2 \geq 0$ satisfy the systems of LMIs (18-19) and

$$\begin{pmatrix} (\sum - \rho)P, & \frac{PB + \tilde{Y}^{\top} + (\tilde{F} - \rho\tilde{F} \pm 2\tilde{\gamma}_1)\tilde{F}^{\top}\tilde{Y}^{\top}}{q_i} & \tilde{Y}^{\top} & \mathbf{0} & \mathbf{0} \\ * & \frac{(\gamma + \tilde{\gamma}_1)B^{\top}PB + \tilde{Y}B + B^{\top}\tilde{Y}^{\top}}{q_i} & \mathbf{0} & \tilde{Y}\tilde{F} & \mathbf{0} \\ * & * & -q_iQ & \mathbf{0} & \mathbf{0} \\ * & * & * & -\gamma q_i P & \tilde{Y} \\ * & * & * & * & -\frac{P}{\tilde{\gamma}_2} \end{pmatrix} \prec 0 \quad (27)$$

where $\sum = 2\gamma_1 + \gamma_2 + \tilde{\gamma}_1 + \tilde{\gamma}_2$, $i = 1, 2$. Then the closed-loop system (1), (14) is globally uniformly

- globally uniformly finite-time stable for $\mu < 0$;
- globally uniformly exponentially stable for $\mu = 0$;
- globally uniformly nearly fixed-time stable $\mu > 0$.

Based on the strict Lyapunov function, using the property of canonical homogeneous norm, we can embed the perturbation information into new LMIs, which conserve the finite/fixed-time convergence rate.

According to Remark 1 and Remark 2, the terms u_{hom} and u_{int} are locally bounded, and the settling time when $\mu < 0$ is estimated in Corollary 2, so we can estimate the maximum magnitude of the control signal dependently of the initial condition and the magnitude of the constant perturbation/

Corollary 3 (The estimate of the control magnitude): Under conditions of Theorem 3 (or Corollary 2) one has

$$\|u(x)\|_m \leq \|K_0\| \cdot \|x\| + \|K\| \cdot \|x\|_{\mathbf{d}}^{1+\mu} + \sqrt{\frac{V(\xi_0)}{\tilde{\lambda}}} + \|p\|, \quad (28)$$

where $\tilde{\lambda}$ and ξ_0 are defined in Corollary 1, the vector norm in \mathbb{R}^m is defined as

$$\|v\|_m = \sqrt{v^{\top}v},$$

the vector norm in \mathbb{R}^n is given by

$$\|y\| = \sqrt{y^{\top}Py}$$

and the matrix norm for $Z \in \mathbb{R}^{m \times n}$ is defined as follows

$$\|Z\| = \sqrt{\lambda_{\max}(P^{-1/2}Z^{\top}ZP^{-1/2})}.$$

Remark 3: The integral part x_{n+1} is bounded by $\sqrt{\frac{V(\xi_0)}{\tilde{\lambda}}} + \|p\|$, when the initial state and the constant perturbation are bounded, x_{n+1} is bounded.

Compared to homogeneous proportional control, the admissible value of the homogeneity degree of the homogeneous PI algorithm is restricted to $\mu \geq -0.5$, since for $\mu < -0.5$ the term u_{int} becomes unbounded at $x = 0$.

V. EXAMPLE

A simulation on a twin rotor system is implemented. The twin rotor system (TRMS 33-220 platform) model can be represented in the following form [28]:



Fig. 1. TRMS 33-220 twin rotor MIMO system

$$\begin{aligned}
 x &= (\psi \quad \dot{\psi} \quad \tau_1 \quad \phi \quad \dot{\phi} \quad \tau_2 \quad M_R)^T \\
 A &= \begin{pmatrix} 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & \frac{-B_1\psi}{l_1} & \frac{b_1}{l_1} & 0 & 0 & 0 & 0 \\ 0 & 0 & \frac{-T_{10}}{T_{11}} & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & \frac{-B_1\phi}{l_2} & \frac{b_2}{l_2} & \frac{-1}{l_2} \\ 0 & 0 & 0 & 0 & 0 & \frac{-T_{20}}{T_{21}} & 0 \\ 0 & 0 & \frac{k_c(-T_0T_{10}+T_{11})}{T_pT_{11}} & 0 & 0 & 0 & \frac{-1}{T_p} \end{pmatrix} \\
 B &= \begin{pmatrix} 0 & 0 & \frac{k_1}{T_{11}} & 0 & 0 & 0 & \frac{k_cT_0k_1}{T_pT_{11}} \\ 0 & 0 & 0 & 0 & 0 & \frac{k_2}{T_{21}} & 0 \end{pmatrix}^T
 \end{aligned} \quad (29)$$

where ψ is the pitch angle, ϕ is the yaw angle, τ_1, τ_2 are the vertical and horizontal motor moments, M_R is the cross reaction momentum. With $\mu = -0.02$, $\rho = 1$, Then, by solving the LMIs (9) and (18-19) we obtain:

$$K_0 = \begin{pmatrix} 0 & 0 \\ 0.0012 & -0.0063 \\ 0.0807 & 2.6835 \\ 0 & 0 \\ 0 & -6.9444 \\ 0 & 7.500 \\ -4.0476 & -56.5131 \end{pmatrix}^T$$

$$K = 10^3 \begin{pmatrix} -0.1591 & -0.0067 \\ 0.0798 & 0.0134 \\ -0.9316 & -0.0401 \\ -0.0080 & -0.0053 \\ -0.0150 & -0.0100 \\ 0.0034 & 0.0057 \\ -2.6709 & -0.1779 \end{pmatrix}^T$$

$$G_d = 10^{-2} \begin{pmatrix} 106 & -4.86 & 30.8 & -0 & 0 & 0 & 88 \\ 0 & 104.43 & -15.40 & 0 & 0 & 0 & -44 \\ 0.13 & 104.67 & 0 & 0 & 0 & 0 & 13.33 \\ -0.26 & 0.64 & -4.03 & 104 & 0 & 0 & -11.51 \\ 0 & -0.32 & 2.02 & 0 & 102 & 0 & 5.76 \\ 0 & -0.59 & -10.02 & 0 & 2.22 & 100 & -28.63 \\ 0 & -0.02 & -1.08 & 0 & 0 & 0 & 96.9 \end{pmatrix}$$

$$P = 10^3 \begin{pmatrix} 0.65 & -0.50 & 4.55 & -0.02 & 0 & -0.01 & 13 \\ -0.5 & 0.6 & -4.24 & -0.01 & 0 & 0 & -12.12 \\ 4.55 & -4.24 & 34.96 & -0.14 & 0 & -0.07 & 99.82 \\ -0.02 & -0.01 & -0.14 & 0.01 & 0 & 0 & -0.39 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0.01 \\ -0.01 & 0 & -0.07 & 0 & 0 & 0 & -0.19 \\ 13 & -12.12 & 99.82 & -0.39 & 0.01 & -0.19 & 285 \end{pmatrix}$$

$$\tilde{K} = \begin{pmatrix} -159.1 & -6.7 \\ -79.8 & 13.4 \\ -931.6 & 40.1 \\ -8 & -5.3 \\ -15 & -10 \\ 3.4 & 5.7 \\ -2670.9 & -177.9 \end{pmatrix}^T, \tilde{Y} = \begin{pmatrix} 0.1024 & -0.3513 \\ -0.9187 & 0.4149 \\ 0.9008 & 10.1486 \\ -0.3336 & 0.0903 \\ -8.6533 & -3.8911 \\ 0 & 4.3103 \\ -0.3688 & -3.5183 \end{pmatrix}^T$$

$$Q = \begin{pmatrix} 0.1496 & -0.0464 \\ -0.0464 & 0.3041 \end{pmatrix}, \gamma = 0.0094$$

The initial state is $[0.5, 0, 0, 0.5, 0, 0, 0]^T$, the constant perturbation $p = 1$. Simulation results are presented in Fig. 2 and Fig. 3. From the result, the system has a static error under the homogeneous P controller, but the system with the homogeneous PI controller can well reject the constant perturbation. Moreover, the system has a non-asymptotic convergence rate.

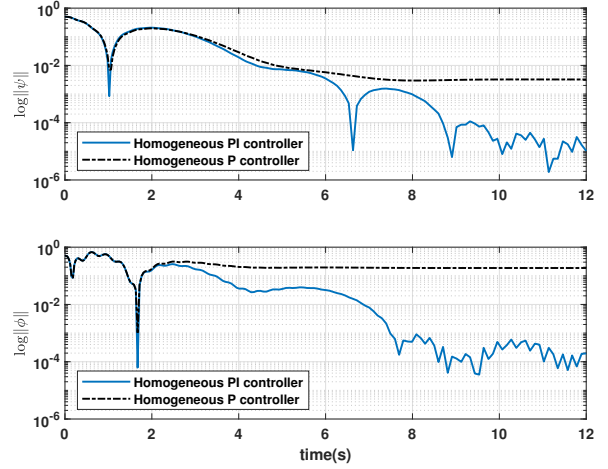


Fig. 2. Angular position under homogeneous PI and P controller

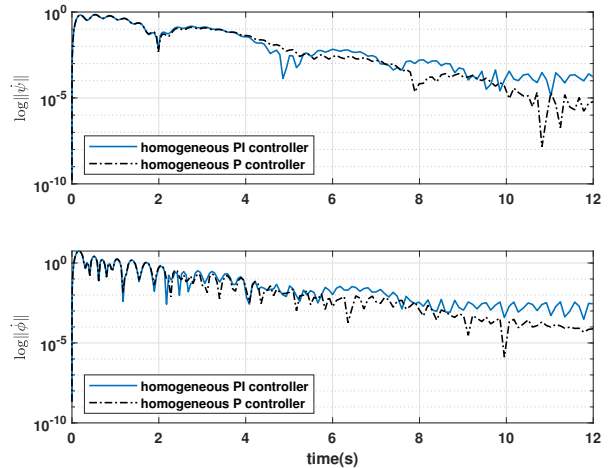


Fig. 3. Angular velocity under homogeneous PI and P controller

VI. CONCLUSION

A strictly Lyapunov function for an analysis of the generalized homogeneous PI controller with negative homogeneity degree is designed. A class of perturbations to be rejected by the mentioned controller is characterized. Moreover, the settling time and the magnitude of the control signal are estimated dependently of the initial condition and the magnitude of the perturbation. A further study about the case of a positive homogeneity degree will need to be done to obtain the nearly fixed time stability property.

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