

# An information-theoretic framework for optimal design: analysis of protocols for estimating soft tissue parameters in biaxial experiments

Ankush Aggarwal, Damiano Lombardi, Sanjay Pant

### ▶ To cite this version:

Ankush Aggarwal, Damiano Lombardi, Sanjay Pant. An information-theoretic framework for optimal design: analysis of protocols for estimating soft tissue parameters in biaxial experiments. Axioms, 2021. hal-03187110

## HAL Id: hal-03187110 https://inria.hal.science/hal-03187110

Submitted on 31 Mar 2021

**HAL** is a multi-disciplinary open access archive for the deposit and dissemination of scientific research documents, whether they are published or not. The documents may come from teaching and research institutions in France or abroad, or from public or private research centers. L'archive ouverte pluridisciplinaire **HAL**, est destinée au dépôt et à la diffusion de documents scientifiques de niveau recherche, publiés ou non, émanant des établissements d'enseignement et de recherche français ou étrangers, des laboratoires publics ou privés.



### Article An information-theoretic framework for optimal design: analysis of protocols for estimating soft tissue parameters in biaxial experiments

Ankush Aggarwal <sup>1,†</sup>, Damiano Lombardi <sup>2,†</sup> and Sanjay Pant <sup>3,†,\*</sup>

- <sup>1</sup> Glasgow Computational Engineering Centre, James Watt School of Engineering, University of Glasgow, Glasgow, UK
- <sup>2</sup> Centre de Recherche INRIA de Paris & Laboratoire Jacques-Louis Lions, France
- <sup>3</sup> Zienkiewicz Centre for Computational Engineering, College of Engineering, Swansea University, Swansea, UK
- \* Correspondence: Sanjay.Pant@swansea.ac.uk
- + These authors contributed equally to this work.
- 1 Abstract: A new framework for optimal design based on the information-theoretic measures of
- 2 mutual information, conditional mutual information, and their combination is proposed. The
- <sup>3</sup> framework is tested on the analysis of protocols—combination of angles along which strain
- 4 measurements can be acquired—in a biaxial experiment of soft tissues for the estimation of
- 5 hyperelastic constitutive model parameters. The proposed framework sees information gain about
- 6 the parameters from the experiment as the key criterion to be maximised which can be directly
- <sup>7</sup> used for optimal design. Information gain is computed through *k*-nearest neighbour algorithms
- applied to the joint samples of the parameters and measurements produced by the forward and
- observation models. For biaxial experiments, the results show that low angles have relatively low
- <sup>10</sup> information content compared to high angles. They also show that fewer number of angles with
- suitably chosen combinations can result in higher information gains when compared to a larger
- number of angles which are poorly combined. Finally, it is shown that the proposed framework is
- 13 consistent with classical approaches, particularly the D-optimal design.

**Keywords:** optimal design; soft tissue mechanics; mutual information; biaxial experiment; inverse problems; information theory.

#### 16 1. Introduction

14

15

17

18

19

20

21

22

23

24

25 26

27

28

29

30

31

32

Soft tissues exhibit complex biomechanical behaviour, including nonlinearity, anisotropy and heterogeneity [1]. Moreover, the tissues also demonstrate inelastic properties, such as rate-dependence, hysteresis and permanent set. The important link between the biomechanics and their physiological function have motivated a large number of ex-vivo studies aimed at characterizing their biomechanical properties. Given the complex interplay between the different aspects of their biomechanical properties, the experimental design of ex-vivo soft tissues is extremely challenging and has been a subject of investigation with a variety of experiments been proposed [2–6].

Since a variety of soft tissues are thin, e.g., blood vessels, heart valves and skin, biaxial testing is a widely used experimental technique that allows independently stretching the tissue in two orthogonal directions and measuring the corresponding forces [7,8]. Applying different stretches in two directions allows characterization of the in-plane anisotropic behavior of a given tissue, while a range of stretches provides us its nonlinear elastic response. However, even with this relatively simple set of options, the choices of what stretches to apply are unclear. Moreover, it is not obvious what these choices will depend on.

**Citation:** Aggarwal, A.; Lombardi, D.; Pant, S. An information-theoretic framework for optimal design: analysis of protocols for estimating soft tissue parameters in biaxial experiments. *Axioms* **2021**, *1*, 0. https://doi.org/

Received: Accepted: Published:

**Publisher's Note:** MDPI stays neutral with regard to jurisdictional claims in published maps and institutional affiliations.

**Copyright:** © 2021 by the authors. Submitted to *Axioms* for possible open access publication under the terms and conditions of the Creative Commons Attribution (CC BY) license (https://creativecommons.org/licenses/by/ 4.0/).

Version March 31, 2021 submitted to Axioms

38

A variety of hyperelastic models have been developed to describe the anisotropic and nonlinear elastic properties of specific soft tissues [4,9–11]. The biaxial experimental data is commonly fit to these models in order to determine the model parameters. As the

unknown parameters depend on specific model, the choice of experimental setup—the
 problem of optimal design—might depend on the choice of model. However, in practice,

a predetermined set of experimental protocols are used.

In the present work, an optimal design problem is defined as finding the most 39 suitable protocol in view of estimating the parameters of the material model. A compre-40 hensive overview of the optimal design problem can be found in [12,13], and several 41 criteria for optimal design have been proposed in the literature, often based on the 42 minimisation of the variance of the parameters and sensitivities [14,15]. In the present work, we investigate a criterion based on information theoretic quantities, in the spirit of what has been proposed in the work [16] (from a Bayesian point of view) and [17]. The goal is to characterise the amount of information the measurements convey about the 46 parameters we would like to estimate and then maximise that information. Estimating 47 information theoretic quantities is in general a challenging problem, and this is especially 48 the case in high-dimensional settings. In the present work, a model reduction method is coupled with a non-parametric sample based mutual information estimation in order to 50 provide a pertinent estimation of the information theoretic quantities involved in the 51 optimal design problem and then applied to the biaxial testing of soft tissues. 52

The structure of the work is as follows: in Section 2 the model and information theoretical aspects of the problem are introduced. In particular, in Section 2.1 we detail the mathematical model of the biaxial experiments for soft tissues: after having introduced the notation and the non-linear elasticity model, in Section 2.1.1 we particularise it to the biaxial testing experimental setup. In Section 2.1.2 we introduce the experimental protocol definition.

The second part of the Section is devoted to the description of the informationtheoretic framework for solving the optimal design problem. In Section 2.2.1 we introduce the problem, in Sections 2.2.2 and 2.2.3 the information-theoretic quantities and their numerical estimation are detailed. We then present the reduce order modeling method used and how to validate the results obtained by the proposed approach. The section ends with an overview of the method.

The results and the discussion are presented in Section 3, followed by the conclusion and the perspectives.

#### 67 2. Methods

The methodological aspects are divided into two broad categories: the mathematical model of the biaxial experiments; and the information-theoretic optimal design framework.

#### 71 2.1. Mathematical model of the biaxial experiments

<sup>72</sup> We begin by defining the notation: a material point at its reference position  $X \in \mathbb{R}^3$ <sup>73</sup> moves to  $x \in \mathbb{R}^3$  after deformation. The elastic behavior of soft tissues is described using <sup>74</sup> hyperelastic strain energy density  $\Psi$  which depends on the deformation gradient tensor <sup>75</sup>  $\mathbf{F} = \nabla_X x$ . The ratio of volume after deformation to that before deformation is given by <sup>76</sup>  $J = \det(\mathbf{F})$ . Soft tissues are commonly regarded as incompressible due to high water <sup>77</sup> content, i.e. *J* is constrained to be unity.

We consider the hyperelastic model proposed by Gasser et al.[18] which defines the
strain energy density

$$\Psi = \frac{k_1}{2k_2} \Big[ e^{k_2(\kappa I_1 + (1 - 3\kappa)I_4 - 1)} - 1 \Big] + \mu(I_1 - 3), \tag{1}$$

- where  $I_1 = tr(\mathbf{F}^{\top}\mathbf{F})$  is the first invariant of the right Cauchy-Green strain tensor  $\mathbf{C} = \mathbf{F}^{\top}\mathbf{F}$
- and  $I_4 = M \cdot CM$  is the fourth invariant representing stretch along fiber direction *M*.
- 82 The resulting Cauchy stress is given by

$$\sigma = 2\mathbf{F} \cdot \frac{\partial \Psi}{\partial \mathbf{C}} \cdot \mathbf{F}^{\top} - p\mathbf{I}, \qquad (2)$$

where *p* acts as the Lagrange multiplier to enforce incompressibility and **I** is the identity matrix.

For this model, the set of unknown parameters can be written as  $\{k_1, k_2, \kappa, \mu\}$ assuming that the fiber direction M is known a priori (based on another experiment, e.g., light scattering [6]). In this paper, in order to simplify the problem, we assume that  $\kappa = 0.1$  and  $\mu = 0.1$  kPa are known and fixed. Thus, the aim of an ex-vivo biomechanical experiment is to determine parameters  $k_1 \in [5, 100]$  kPa and  $k_2 \in [5, 80]$  robustly and with high confidence [19,20]. A commonly used experiment called the biaxial testing is described next.

#### 92 2.1.1. Biaxial experiments for soft-tissues

Many of the soft tissue types are planar with small thickness. In a biaxial experiment, a square-shaped tissue sample is mounted via clamps or rakes and stretched along two orthogonal directions aligned with the sample edges (Fig. 1a). If these directions are used as the two coordinate axes and incompressibility is assumed, the stretching results in a diagonal deformation gradient tensor

$$\mathbf{F} = \operatorname{diag}\left[\lambda_1, \lambda_2, \frac{1}{\lambda_1 \lambda_2}\right],\tag{3}$$

where  $\lambda_1$  is the stretch along first in-plane direction and  $\lambda_2$  is the stretch along second in-plane direction. The fiber direction M is generally aligned with the first coordinate axis, which results in only normal stress components. As no force is applied along the thickness of the tissue,  $\sigma_{33} = 0$  is used to determine the Lagrange multiplier p. Thus, we get

$$\sigma_{11} = 2\frac{\partial \Psi}{\partial I_1} \left[ \lambda_1^2 - \frac{1}{\lambda_1^2 \lambda_2^2} \right] + 2\frac{\partial \Psi}{\partial I_4} \lambda_1^2 \tag{4}$$

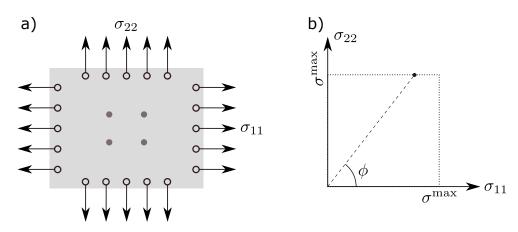
$$\sigma_{22} = 2 \frac{\partial \Psi}{\partial I_1} \left[ \lambda_2^2 - \frac{1}{\lambda_1^2 \lambda_2^2} \right].$$
(5)

The applied stresses  $\sigma_{11}$ ,  $\sigma_{22}$  are controlled using load cells. The resulting strains defined as  $e_1 := \lambda_1 - 1$  and  $e_2 := \lambda_2 - 1$  are measured from the marker positions<sup>1</sup>. It is important to note that a homogeneous stress and strain state is assumed in the middle of the sample (Fig. 1a). Therefore, an implicit assumption is that the material properties and sample thickness are homogeneous. Moreover, these measurement techniques carry an error due to the limitations in measurement tools and/or the deviation from homogeneity, incompressiblity and material direction.

#### 110 2.1.2. Protocol definition

In practice, there are two approaches to the biaxial experiment: 1) displacement controlled where known stretches are imposed and forces are measured and 2) force controlled where known forces are applied and stretches are measured. Generally, the force controlled approach is used as it is easier to implement. Therefore, in the force controlled approach, different values of stresses  $\sigma_{11}$  and  $\sigma_{22}$  can be applied.

Although  $e_1$  and  $e_2$  are not the usual strain measures, we use these as our observations



**Figure 1.** a) A schematic of a biaxial experimental setup where a thin planar tissue sample (in light gray) is mounted via rakes and two orthogonal forces are applied to induce stresses  $\sigma_{11}$  and  $\sigma_{22}$ , and the resulting strains are measured by tracking the locations of the markers (in dark gray). b) The  $\sigma_{11} - \sigma_{22}$  space, where the applied stresses lie on the dotted line with a finite number of protocol angles  $\phi$  used.

A single-angle biaxial protocol is defined as a straight line in the  $\sigma_{11}$ - $\sigma_{22}$  space (Fig. 1b). That is, the ratio between the two stresses is kept constant while the applied forces are increased until a maximum value  $\sigma^{max} = 200$  kPa. Thus, for a chosen angle  $\phi$ , we apply:

$$\sigma_{11} = \begin{cases} \sigma & \text{if } \phi \le \frac{\pi}{4} \\ \tan(\phi)\sigma & \text{else} \end{cases}$$
(6)

$$\sigma_{22} = \begin{cases} \cot(\phi)\sigma & \text{if } \phi \le \frac{\pi}{4} \\ \sigma & \text{else} \end{cases}$$
(7)

where  $\sigma \in [0, \sigma^{\text{max}}]$ . For  $\sigma$ , 100 linearly spaced observation points between zero and the maximum stress ( $\sigma^{\text{max}} = 200$  kPa) are used. The resulting strains are calculated by iteratively solving equation (5) for  $\lambda_{1,2}$  and thereby obtaining  $e_{1,2}$ . In practice, a combination of angles can be successively tested. We refer to this combination as the experimental protocol that needs to be optimally designed.

#### 125 2.2. Information-theoretic framework for optimal design

The problem of optimal design typically refers to the choice of a design of ex-126 periments such that the design is optimal with respect to a pre-determined statistical 127 criterion. We propose that the information-theoretic measures naturally define such 128 statistical criteria. The central idea is that information gain [21,22] from an experiment 129 or protocol—as quantified by the information-theoretic quantities of mutual information 130 and conditional mutual information-can be directly used as a reasonable statistical 131 criterion for optimal design. These quantities are described next after presenting the 132 framework for optimal design. 133

134 2.2.1. Optimal design problem

Consider the following general model:

$$\mathbf{y} = \mathcal{M}(\boldsymbol{\theta}),\tag{8}$$

where  $\mathcal{M}$  denotes for the forward model that takes  $\theta \in \mathbb{R}^m$  and outputs  $\mathbf{y} \in \mathbb{R}^n$ . Note

that  $\theta$  may contain initial and boundary conditions of the model and that y may subsume

the output at many time-points in the case of a dynamical system. Subsequently, considerthat the measurement model is as follows

$$\mathbf{z} = \mathcal{H}_p(\mathbf{y}, \boldsymbol{\theta}) + \boldsymbol{\varepsilon},\tag{9}$$

where  $\mathcal{H}_p$  represents the observation operator,  $\mathbf{z} \in \mathbb{R}^d$  represents the measurement vector, and  $\varepsilon$  represents the vector of measurement error/noise. Note that the the observation operator  $\mathcal{H}_p$  depends on the design of experiments, which specifies which quantities are measured. Given a set of possible  $\mathcal{H}_p = \{\mathcal{H}_1, \mathcal{H}_2, \cdots, \mathcal{H}_h\}$ , and a statistical criterion  $\mathcal{S}(\mathcal{H}_p)$  to be maximised, the optimal design is given by

$$\hat{\mathcal{H}}_p = \operatorname*{arg\,max}_{\mathcal{H}_p} \mathcal{S}(\mathcal{H}_p). \tag{10}$$

In the case of the biaxial experiments, the model  $\mathcal{M}$  represents the model for the force controlled experiment (sections 2.1.1 and 2.1.2) and  $\mathcal{H}_p$  essentially denotes the experimental protocol, see section 2.1.2, representing the combination of angles—each representing a straight line in the  $\sigma_{11}$ - $\sigma_{22}$  plane—along which the strain measurements of  $e_1$  and  $e_2$  are acquired. With the possible variation of each angle between 0 and  $\pi/2$ , the set  $\Phi$  of possible angles  $\phi$  are constructed through a uniform discretisation of the space between 0 and  $\pi/2$  into  $\alpha$  levels, thus

$$\Phi = \{\phi_0, \phi_1, \cdots, \phi_\alpha\}. \tag{11}$$

The possible set of protocols is then given by any combination of elements in  $\Phi$  with the restriction that the number of elements in a protocol be limited to C. Thus, if  $\overline{\Phi} \subset \Phi$  is a subset of angles representing a protocol, our set of protocols is given by

$$\mathcal{H}_{p} = \left\{ \overline{\Phi} \subset \Phi \, | \, 1 \le |\overline{\Phi}| \le \mathcal{C} \right\},\tag{12}$$

where  $|\cdot|$  represents the number of elements in the set. In other words, we choose at least 1 and up to C elements from  $\Phi$ , with the total elements in  $\mathcal{H}_p$  being

$$|\mathcal{H}_p| = {\alpha \choose 1} + {\alpha \choose 2} \dots + {\alpha \choose C}.$$
 (13)

156 2.2.2. Information-theoretic quantities for optimal design

In the framework of section 2.2.1, we propose that information-theoretic quantities of mutual information and conditional mutual information are a natural choice for the statistical criterion S. Denoting the random variables associated with  $\theta$  and z as  $\Theta$ and Z, respectively, the mutual information (MI) between the parameters  $\Theta$  and the measurements Z is defined as [21]

$$\mathcal{I}(\mathbf{\Theta}; \mathbf{Z}) = \int_{\mathcal{X}_{\mathbf{\Theta}} \times \mathcal{X}_{\mathbf{Z}}} p_{\mathbf{\Theta}, \mathbf{Z}}(\boldsymbol{\theta}, \mathbf{z}) \frac{p_{\mathbf{\Theta}, \mathbf{Z}}(\boldsymbol{\theta}, \mathbf{z})}{p_{\mathbf{\Theta}}(\boldsymbol{\theta}) p_{\mathbf{Z}}(\mathbf{z})} d\boldsymbol{\theta} d\mathbf{z},$$
(14)

where  $p_X(x)$  represents the probability density of a random variable X with a realisation 162 X = x and support  $\mathcal{X}_{X}$ . The mutual information  $\mathcal{I}(\Theta; \mathbf{Z})$  quantifies the amount of 163 information that can be gained on average by knowing one random variable, say Z, 164 about the other, say  $\Theta$ . Indeed, with this interpretation, MI is a good candidate for the 165 statistical criterion S for optimal design. For an individual parameter,  $\Theta_i$ , or indeed 166 for any combination of parameters  $\{\Theta_i, \Theta_i\}$ , the corresponding information gains can 167 be similarly computed through  $\mathcal{I}(\Theta_i; \mathbf{Z})$  and  $\mathcal{I}(\{\Theta_i, \Theta_i\}; \mathbf{Z})$ , respectively. Thus, while 168  $\mathcal{I}(\Theta_i; \mathbf{Z})$  quantifies the information gain individually for the parameter  $\Theta_i$ , the quantity 169  $\mathcal{I}(\{\Theta_i, \Theta_i\}; \mathbf{Z})$  quantifies information gain for the pair  $\{\Theta_i, \Theta_i\}$  jointly. A measure of 170 correlation between the parameters  $\Theta_i$  and  $\Theta_i$  is, however, missing, and is provided by 171 conditional mutual information (CMI) defined as 172

$$\underbrace{\mathcal{I}(\Theta_i;\Theta_j|\mathbf{Z})}_{\mathrm{I}} = \underbrace{\mathcal{I}(\Theta_i;\{\Theta_j,\mathbf{Z}\})}_{\mathrm{II}} - \underbrace{\mathcal{I}(\Theta_i;\mathbf{Z})}_{\mathrm{III}}.$$
(15)

The CMI  $\mathcal{I}(\Theta_i; \Theta_j | \mathbf{Z})$  represents the additional information gained about the parameter  $\Theta_i$  when both  $\Theta_j$  and Z are known (term II) relative to when only the measurements  $\Theta_i$  alone are known (term III). Note that CMI is symmetric, i.e.  $\mathcal{I}(\Theta_i; \Theta_j | \mathbf{Z}) = \mathcal{I}(\Theta_j; \Theta_i | \mathbf{Z})$ , and can be interpreted as a measure of dependence between the parameters given the measurements  $\mathbf{Z}$ . Also note that both MI and CMI are non-negative.

With the above background, many statistical measures can be constructed. For example:

1. The mutual information for any single parameter may be maximised, giving  $S = \mathcal{I}(\Theta_i; \mathbf{Z})$ . This approach only concerns with the posterior of the parameter  $\Theta_i$  and ignores all other parameters.

<sup>183</sup> 2. The joint mutual information may be maximised, giving  $S = \mathcal{I}(\Theta; \mathbf{Z})$ . In the sense <sup>184</sup> of classical optimal design this can be interpreted as the D-optimal design. This is <sup>185</sup> because D-optimal designs minimise the determinant of the Fisher Information <sup>186</sup> Matrix inverse, and  $S = \mathcal{I}(\Theta; \mathbf{Z})$  measures the information gain in the joint  $\Theta$ <sup>187</sup> space.

<sup>188</sup> 3. The sum of individual parameter mutual information may be be maximised, giving <sup>189</sup>  $S = \sum_{i=1}^{m} \mathcal{I}(\Theta_i; \mathbf{Z})$ . In the sense of classical optimal design this can be interpreted <sup>190</sup> as the A-optimal design. This is because the the A-optimal design minimises the <sup>191</sup> trace of the Fisher Information Matrix inverse, and  $S = \sum_{i=1}^{m} \mathcal{I}(\Theta_i; \mathbf{Z})$  measures <sup>192</sup> the sum of the information gains for all the parameters.

Alternatively, one may seek to maximise individual parameter information gain
 while minimising pairwise CMI, thus seeking both small posterior variances and
 minimising pairwise correlations between the parameters. In this case, the statistical
 criterion is

$$S = \sum_{i=1}^{m} \mathcal{I}(\Theta_i; \mathbf{Z}) - \tau \sum_{i=1}^{m} \sum_{j=i}^{m} \mathcal{I}(\Theta_i; \Theta_j | \mathbf{Z}),$$
(16)

where  $\tau > 0$  is a regularisation parameter.

Note that the above list is not exhaustive, and based on the interpretations of MIand CMI, other criteria may be constructed based on the desired sense of optimality.

#### 200 2.2.3. Estimating mutual information

In general, the forward model in equation (8) is non-linear, and hence even if the 201 observation operator is linear (implying linear combinations of the state are measured), 202 the analytical computation of mutual information is intractable. Thus, the information-203 theoretic quantities of MI and CMI must be estimated. A common method is to generate 204 samples of  $\Theta$  through specification of an appropriate prior probability density  $p_{\Theta}(\theta)$ . 205 Denoting these  $N_s$  samples as  $\theta^{(i)}$ ,  $i = \{1, 2, \dots, N_s\}$ , each  $\theta^{(i)}$  can be propagated through 206 the forward and observation models of equations (8) and (9) to produce corresponding 207 samples of **Z**, denoted as  $\mathbf{z}^{(i)}$ . The samples of  $\boldsymbol{\theta}^{(i)}$  and  $\mathbf{z}^{(i)}$  can subsequently be used on 208 non-parametric estimators of MI and CMI. Such non-parametric estimators can broadly 209 be classified into two categories: kernel density estimators (KDE) [23] and k-nearest 210 neighbour (kNN) estimators [24,25]. For an overview of such methods, we refer to [26]. 211 While the estimator proposed by Kraskov et. al. [24] is widely used and performs very 212 well across a range of scenarios, one of its drawbacks is that it suffers from higher errors 213 when extreme correlations are present between the variables and/or when the the data 214 effectively lives in a lower-dimensional manifold. Since we are working with models that 215 specify explicit relationships between the variables through the forward and observation 216 model, this is likely to be true for the data-set of  $(\theta^{(i)}, \mathbf{z}^{(i)})$ . Thus, in this study, we 217

- employ the local non-uniformity correction (LNC) proposed in [27], which includes a
- correction term to the original estimator by Kraskov et. al. [24]. This term accounts for
- <sup>220</sup> strong dependencies between the variables through local principle component analysis
- [27]. The method of [27] is used for estimation of all MIs, and CMIs are estimated from
- the difference of two MIs, see equation (15).

223 2.2.4. Dimensionality reduction for the biaxial experiment

One of the main difficulties in estimating information theoretic quantities is re-224 lated to the data dimension. The non-parametric estimation is particularly challenging 225 whenever the data are close to manifolds embedded in high-dimensional spaces. This is 226 indeed the case when a physical model relates parameters and observable quantities. 227 One of the possible ways to overcome this difficulty or, at least, to mitigate it, is (dimen-228 sion or) model reduction, which aims at discovering the underlying low-dimensional 229 structure of a set of data (a comprehensive review of the topic can be found in [28–31]). 230 A large spectrum of methods have been proposed in the literature. In the present con-231 tribution, we adopt a local reduced-basis method (similar, in the spirit, to the methods 232 proposed in [32,33]). Let the strains computed by the model be  $e_{1,2}(\sigma;\phi;k_1,k_2)$ , where 233  $k_1$  and  $k_2$  are the model parameters  $(k_1, k_2) \in \Omega_k \subset \mathbb{R}^2$ , and  $\sigma \in \Omega_\sigma \subset \mathbb{R}$  is the variable 234

defined in section 2.1.2. Let  $n \in \mathbb{N}^*$ , we introduce the following approximation:

$$e_{1,2} \approx \sum_{i=1}^{n} \eta_i r_i(\sigma, \phi) s_i(k_1, k_2, \phi),$$
 (17)

which is well defined by virtue of the Eckart-Young theorem. First, let us observe that a given protocol consists in a set of known angles  $\overline{\Phi}$ . An efficient way to construct the

<sup>238</sup> local reduced basis is hence to introduce a Proper Orthogonal Decomposition (POD) for

each of the angles  $\phi_j \in \overline{\Phi}$ . This corresponds to looking for an approximation of the form:

$$e_{1,2}^{(j)}(\sigma;\phi_j;k_1,k_2) \approx \sum_{i=1}^n \eta_i^{(j)} r_i^{(j)}(\sigma) s_i^{(j)}(k_1,k_2),$$
(18)

where  $\langle r_i^{(j)}, r_k^{(j)} \rangle_{\Omega_{\sigma}} = \delta_{ik}$  and  $\langle s_i^{(j)}, s_k^{(j)} \rangle_{\Omega_k} = \delta_{ik} (\langle \cdot, \cdot \rangle_{\Omega_{\sigma},\Omega_k}$  being the standard  $L^2$  scalar product). The error in the approximation is related to the number *n* of modes retained:

$$\|e_{1,2}^{(j)} - \sum_{i=1}^{n} \eta_i^{(j)} r_i^{(j)}(\sigma) s_i^{(j)}(k_1, k_2)\|_{L^2(\Omega_\sigma \times \Omega_k)}^2 = \sum_{i=n+1}^{\infty} \eta_i^{(j)^2}$$
(19)

In the present work, a number n = 4 modes proved to be sufficient in order to get errors smaller than  $10^{-3}$  in  $L^2$  norm on the solution reconstruction. This means that the set of elements  $e_{1,2}(\sigma; \phi_j; k_1, k_2)$  are close to the linear subspace spanned by the first n = 4 modes  $r_i^{(j)}$ . Henceforth, instead of considering the discretised  $e_{1,2}$  we will consider their coordinates in the subspace, given by:

$$z_{1,2}^{(j)}|_i = \langle e_{1,2}, r_i^{(j)} \rangle_{\Omega_\sigma} = \eta_i^{(j)} s_i^{(j)}(k_1, k_2).$$
<sup>(20)</sup>

242 2.2.5. Validation of results against existing methods

Several methods and criteria to define and reach an optimal design of experiments 243 were proposed [12]. Among them, D-optimality criterion attempts at maximising 244 the determinant of the information matrix. In the present case, this is equivalent to 245 minimize the determinant of the inverse of the average Hessian of the loss function we 246 would introduce in a classical parameter estimation method. In a noisy setting, and, 247 in particular, when the noise is Gaussian, this cost function is equivalent to minus the 248 logarithm of the likelihood function. Let the misfit function be  $f(\theta)$  and  $\mathbb{E}_{\Theta}$  denote the 249 expectation operator. The average of the Hessian reads: 250

$$H = \mathbb{E}_{\Theta}[\partial_{\theta}^2 f|_{\theta_*}], \tag{21}$$

where  $\theta_*$  is the value of the parameter minimising the loss function.

252 2.2.6. Overview of approach for the biaxial experiments

In the context of the biaxial experiments, the parameters are  $k_1$  and  $k_2$ , represented 253 as random variables  $K_1$  and  $K_2$ , respectively. The variability in these parameters is 254 considered to be uniform (thus imposing a uniform prior distribution) in the following 255 intervals:  $k_1 \in [5, 100]$  kPa and  $k_2 \in [5, 80]$ . For a single value of angle  $\phi$ , the measure-256 ments are the strain values  $e_1$  and  $e_2$  and measured at 100 points along the line defined 257 by the angle  $\phi$ . Here, we consider  $\alpha = 16$  discrete values of possible measurement angles 258  $\phi$  uniformly distributed between, and including, 0° and 90°. For each angle  $\phi$ , separate 259 reduced bases of 4 modes for  $e_1$  and  $e_2$  are constructed through POD over 400 values 260 of  $(K_1, K_2)$  sampled uniformly in the aforementioned parametric space. Thus, for any 261 angle  $\phi$ , the dimensionality reduction approach projects  $e_1$  and  $e_2$  measured at 100 points along the line defined by  $\phi$  to a basis of 4+4 modes. For a given protocol consisting of 263 multiple angles, the measurement vector  $\mathbf{z}$  (with corresponding random variable  $\mathbf{Z}$ ), is 264 the collection of all the reduced basis representation of  $e_1$  and  $e_2$  along the angles in the 265 protocol. Lastly, the maximum number of angles in a protocol is restricted to  $\mathcal{C} = 5$ , giving a total of 6,884 unique combinations of the  $\alpha = 16$  angles. 267

For the estimation of MI and CMI, a total of N = 10,000 values of  $(K_1, K_2)$  are uniformly distributed in the parametric space. For each such sample  $(k_1^{(i)}, k_2^{(i)})$ , the numerical model of the biaxial experiment is run to produce  $e_1^{(i)}$  and  $e_2^{(i)}$ , which are then projected on to the reduced basis, giving  $\mathbf{z}^{(i)}$ . The *N* triplets of  $(k_1^{(i)}, k_2^{(i)}, \mathbf{z}^{(i)})$  are subsequently used for estimation of MI and CMI through the LNC estimator (see section 2.2.3). In equation (16) we use  $\tau = 1$ .

#### 274 3. Results and discussion

For all the 6,884 combinations of angles, three statistical criteria are evaluated: (i) 275  $\mathcal{I}(A; \mathbf{Z})$ ; (ii)  $\mathcal{I}(B; \mathbf{Z})$ ; and (iii)  $\mathcal{I}(K_1; \mathbf{Z}) + \mathcal{I}(K_2; \mathbf{Z}) - \mathcal{I}(K_1; K_2 | \mathbf{Z})$ . While the first two 276 criteria aim to maximise information gain about A and B individually, the third criterion 277 aims to maximise information gain about A and B simultaneously while minimising 278 the information dependence between them. Figures 2-4 show the variation in these 279 three criterion when grouped by the number of angles in a protocol. In these Figures the 280 values of information criterion when using two approaches to uniformly discretise the 281 angular space within protocols is also presented. Observations from these plots are as 282 follows: 283

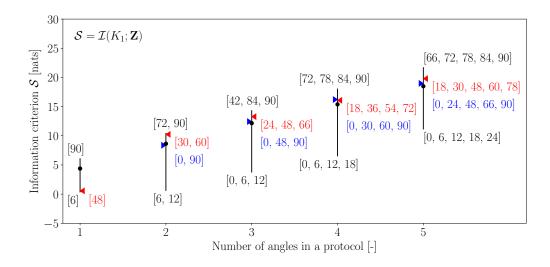
 Generally, all the three information criteria increase with increasing number of angles in the protocol. Intuitively, this is expected as higher number of angles imply more measurement data and hence a higher potential for improved estimation of the parameters. This observation is true for the maximum information gain, minimum information gain, and the mean information gain.

Across all the three criteria, it is observed that the uniform discretisation is not necessarily reflective of the best protocol for estimating the parameters. In fact, in most cases, the performance of uniform discretisation is close to the mean information gain observed across all the angle combinations.

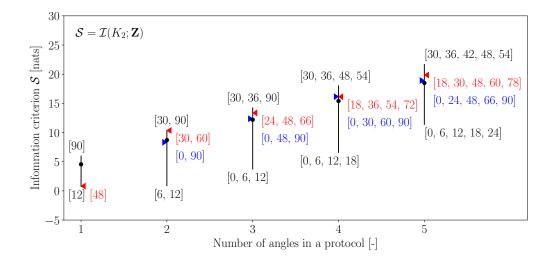
<sup>203</sup> 3. From Figures 2 and 3 it is observed that the angular combinations that maximise <sup>204</sup> information gain for  $K_1$  are not identical—and vary significantly when more than 2 <sup>205</sup> angles are simultaneously used—to those that maximise information gain for  $K_2$ . <sup>206</sup> This further motivates the use of a criterion that balances information gains in both <sup>207</sup> the parameters while minimising their interdependence.

Figure 4 shows that the best combinations that maximises a balanced criterion such as  $\mathcal{I}(K_1; \mathbf{Z}) + \mathcal{I}(K_2; \mathbf{Z}) - \mathcal{I}(K_1; K_2 | \mathbf{Z})$  are a trade-off between the combinations of

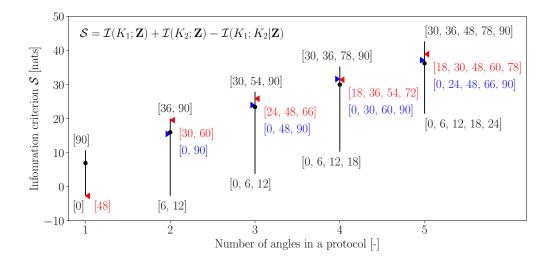
- angles that maximises  $\mathcal{I}(K_1; \mathbb{Z})$  and  $\mathcal{I}(K_2; \mathbb{Z})$  individually. For example, when 5 angles are considered, the angles that maximise  $\mathcal{I}(K_1; \mathbb{Z})$  are  $\phi_a = [66, 72, 78, 84, 90]$ , those that maximise  $\mathcal{I}(K_2; \mathbb{Z})$  are  $\phi_b = [30, 36, 42, 48, 54]$ , while the combination that maximises  $\mathcal{I}(K_1; \mathbb{Z}) + \mathcal{I}(K_2; \mathbb{Z}) - \mathcal{I}(K_1; K_2 | \mathbb{Z})$  is [30, 36, 48, 78, 90], which has two angles from  $\phi_a$  and three angles from  $\phi_b$ . It should be noted that such a trade-off between maximising individual parameter gains is still significantly different than a uniform discretisation.
- Finally, it is observed that the worst combinations are all low angles: [0, 6, 12, 18, 24].
  This can be related to the fact that at low angles, the applied stress is largely aligned along the stiff fibers of the tissue, thus resulting in lower strain values. Thus, the lower angles provide a small range of the observations, while the larger angles provide a larger range (Fig. 9a), thereby containing more information about the parameters.



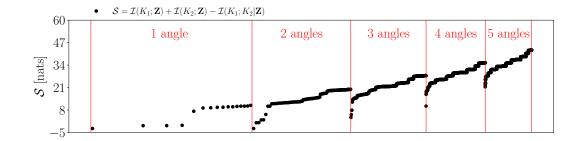
**Figure 2.** The variation of information criterion  $S = \mathcal{I}(K_1; \mathbf{Z})$  across the 6,884 combinations grouped by the number of angles in a protocol. The vertical lines represent the variation around the mean value, which is shown in black circles. Black text shows the combinations that produce maximum and minimum values of S. The red and blue pointers show S for angle combinations that follow a uniform discretisation of the angular space between 0 and 90 degrees. Red and blue texts show the associated angle combinations.



**Figure 3.** The variation of information criterion  $S = \mathcal{I}(K_2; \mathbf{Z})$  across the 6,884 combinations grouped by the number of angles in a protocol. The vertical lines represent the variation around the mean value, which is shown in black circles. Black text shows the combinations that produce maximum and minimum values of S. The red and blue pointers show S for angle combinations that follow a uniform discretisation of the angular space between 0 and 90 degrees. Red and blue texts show the associated angle combinations.



**Figure 4.** The variation of information criterion  $S = \mathcal{I}(K_1; \mathbf{Z}) + \mathcal{I}(K_2; \mathbf{Z}) - \mathcal{I}(K_1; K_2 | \mathbf{Z})$  across the 6,884 combinations grouped by the number of angles in a protocol. The vertical lines represent the variation around the mean value, which is shown in black circles. Black text shows the combinations that produce maximum and minimum values of *S*. The red and blue pointers show *S* for angle combinations that follow a uniform discretisation of the angular space between 0 and 90 degrees. Red and blue texts show the associated angle combinations.



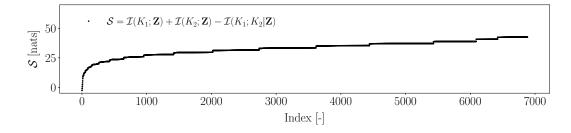
**Figure 5.** The variation of information criterion  $S = \mathcal{I}(K_2; \mathbf{Z}) + \mathcal{I}(K_2; \mathbf{Z}) - \mathcal{I}(K_1; K_2 | \mathbf{Z})$  across the 6,884 combinations. The vertical red lines show the groupings with respect to the number of angles in a protocol and *S* values are sorted in increasing order within each such grouping. The x-axis is represents the index associated with the protocol and is in logarithmic scale to capture the spread between 1 angle in a protocol (16 values) vs 5 angles in a protocol (4,368 values).

From this point onward, we present results only for the balanced information 313 criterion  $\mathcal{S} = \mathcal{I}(K_1; \mathbf{Z}) + \mathcal{I}(K_2; \mathbf{Z}) - \mathcal{I}(K_1; K_2 | \mathbf{Z})$ . Figure 5 shows the variation in  $\mathcal{S}$ 314 across all the combinations (x-axis, and in log-scale to capture the spread) grouped 315 by the number of angles in a protocol and sorted in increasing order of S within each 316 such group. Within each group, when observing the minimum and maximum values 317 of S, it shows that a better choice of angles can lead to more than 100% increase in the information gain compared to a poor choice. Furthermore, it shows that good 319 combinations of a lower number of angles can lead to higher information gain compared 320 to higher number of angles with bad combinations. For example, the maximum  $\mathcal{S}$ 321 when only one angle is used is higher than many combinations with 2-4 angles. This 322 emphasises the utility of optimal design and the proposed framework. 323

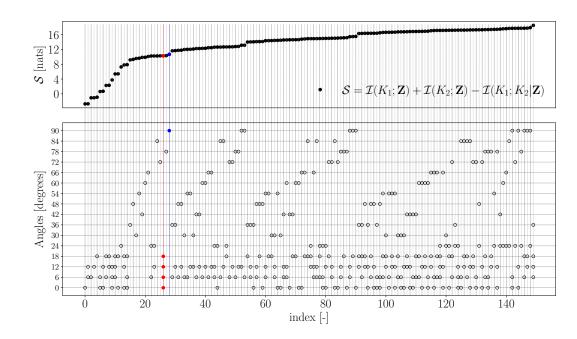
Figure 6 shows S for all the 6,884 combinations in increasing order of magnitude and 324 Figure 7 shows a zoomed plot for the first 150 combinations along with the corresponding 325 combinations of angles. Observing index values of 26 (red) and 28 (blue) in Figure 7 326 shows that even though four combinations are used in index 26 protocol, it produces a 327 lower S compared to only a single angle used in index 28 protocol. Furthermore, since 328 Figure 7 shows the first 150 out of 6,884 combinations of Figure 6 (which is sorted in 329 creasing order of S), all combinations here are relatively low S producing protocols. 330 Observing the high density of angles in the region  $\phi < 24^{\circ}$ , is indicative that lower 331 values of angles, in particular those less than  $24^\circ$  are relatively less informative when 332 compared to higher values of angles. This behaviour is also apparent in Figure 8, which 333 shows S values for protocols that use only one angle, and where a sharp jump can be 334 observed when transitioning from  $18^{\circ}$  to  $24^{\circ}$ . This peculiar behaviour may be explained by the physics of the biaxial experiment. Looking at the resulting strains  $e_1$  and  $e_2$  at this 336 transition (Fig. 9b), we observe that the  $e_1$  changes from positive to negative values. This 337 behavior captures the important coupling between the two normal stresses and strains 338 and is also related to the fiber dispersion in our constitutive model (equation (1), [18]). It 339 is remarkable and encouraging that the information-theoretic framework captures the 340 physics of the problem without explicitly considering it in the framework. While for 341 simpler low-dimensional models the association between physics and optimal design 342 may be relatively easy to see, inferring such behaviour is, in general, not trivial for more 343 complex and higher-dimensional models. 344

Similarly to Figure 8, the results of the information-theoretic optimal design and further be analysed for higher number of angles. When two angles are considered, the Svalues in increasing order of magnitude and the corresponding angle combinations are shown in Figure 10. This figure re-iterates observations made previously: i) the choice of combinations significantly affects the information gain, the best combination gives

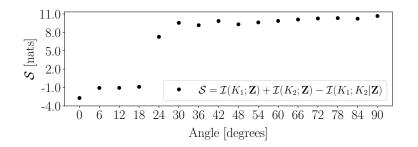
- approximately 20 nats more information compared to the worst combination; and ii)
- <sup>351</sup> generally speaking, higher angles are more informative compared to lower angles, in
- $_{\tt 352}$  particular angles below 24°. While similar analysis for more than two angle combinations
- can be easily performed, efficient visual representation of such results is cumbersome
- and avoided in this manuscript.



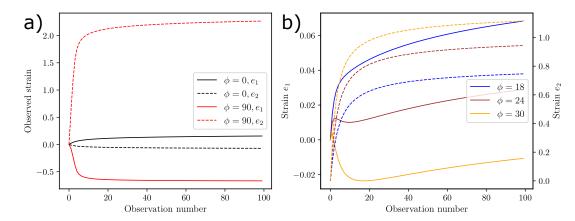
**Figure 6.** The variation of information criterion  $S = I(K_1; \mathbf{Z}) + I(K_2; \mathbf{Z}) - I(K_1; K_2 | \mathbf{Z})$  across the 6,884 combinations sorted in increasing order of *S* 



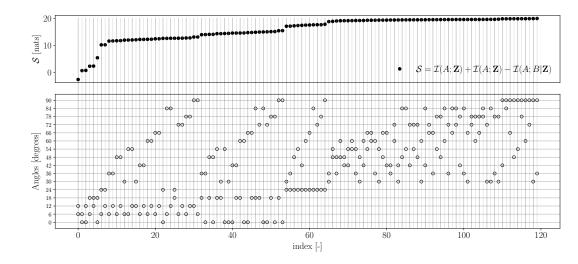
**Figure 7.** Zoomed view into the first 150 protocols from Figure 6. The upper panel shows *S* and the lower panel shows the angles (by circles) in the corresponding protocol.



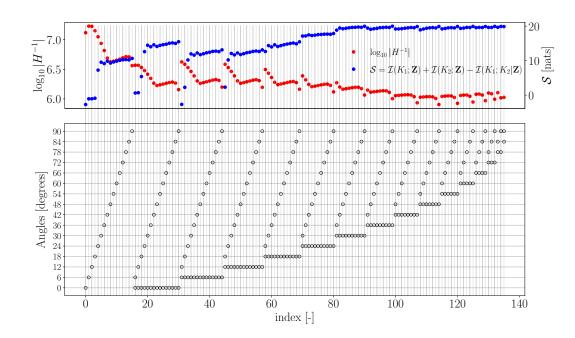
**Figure 8.** Information criterion against the angle when the protocols are restricted to a maximum of one angle.



**Figure 9.** Representative observations from the model with  $k_1 = 40$  kPa and  $k_2 = 40$ . a) The observations using angles  $\phi = 0$  and 90 degrees, with the latter covering a significantly larger range. b) The change in observations the angle is changed from 18, 24, to 30 degrees shows a transition in  $e_1$  from positive to negative values, indicating a coupling between the two directions.



**Figure 10.** Information criterion against the angles when the protocols are restricted to only two angles. The upper panel shows S and the lower panel shows the angles (by circles) in the corresponding protocol.



**Figure 11.** Information criterion S (in blue) and the log of the determinant of the Fisher Information Matrix inverse  $\log_{10} |H^{-1}|$  (in red) against the angles when the protocols are restricted to a maximum of two angles. The upper panel shows S and  $\log_{10} |H^{-1}|$ , while the lower panel shows the angles (by circles) in the corresponding protocol. Note that here  $e_1$  is shown in solid lines (left y-axis) and  $e_2$  is shown in dashed lines (right y-axis).

To further illustrate the validity of the information-theoretic approach, comparison 355 with a classical method, see section 2.2.5, is presented. For one and two angles in a 356 protocol, Figure 11 shows a comparison between  $\mathcal S$  and the log of the determinant of 357 the Fisher Information Matrix inverse,  $\log |H^{-1}|$ . It is encouraging that a high corre-358 spondence between the two metrics is observed. In particular, increases in S, implying 359 higher information gains, are accompanied by corresponding decreases in  $\log |H^{-1}|$ , 360 implying a smaller volume of the parameter posteriors. A Pearson correlation coefficient 361 of r = -0.76 is observed between S and log  $|H^{-1}|$  implying a high similarity between the 362 two metrics, and validating the information-theoretic approach in part. Let us remark 363 that, when the number of the parameters become large, evaluating the Hessian would 364 imply a non-negligible computational cost. On the contrary, the method used to evaluate 365 the Mutual Information, being a primarily Monte Carlo based estimation, is less severely 366 dependent on the number of parameters. Furthermore, computation of derivatives 367 (either numerically or through adjoint based methods) may be cumbersome for certain 368 type of models. Finally, we note that the effect of noise on information gain, and hence 36 optimal design, can be easily assessed in the proposed framework by adding noise to 370 the samples of  $\mathbf{Z}$ , see equation (9). 371

#### 372 4. Conclusion

A framework for optimal design based on information-theoretic quantities of mu-373 tual information and conditional mutual information is proposed. The framework treats 374 information gain as the central criterion for inverse problems and proposes several 375 information-theoretic frameworks for desired sense of optimality. The capabilities of 376 this framework are tested on the optimal design problem for biaxial experiments, where 377 the effect of angle combinations along which the strains are measured is assessed on 378 parameter estimation through information gain. Without including any physics based 379 reasoning and purely through the information-theoretic measures, it is found that low 380 angles  $\leq 24^{\circ}$  are not very informative about the parameters relative to high angles. 381

- These observations are then found to be consistent based on physics-based reasoning,
- thereby showing the efficacy of the proposed framework. Furthermore, it is demon-
- strated measurements for a low total number of angles which are carefully chosen can
- be more informative compared to the case when measurements along a high number
   of poorly chosen angles are acquired, thus highlighting both the importance of optimal
- design for biaxial experiments and the utility of the proposed framework in uncovering
- good angle combinations. Relation of the proposed framework to classical optimal
- design is performed and shown that the results produced by the new framework are
- <sup>390</sup> consistent with classical frameworks.

#### <sup>391</sup> 5. Limitations and future work

While the proposed framework is shown to perform well on a two-parameter 392 problem, its performance in higher parameter problems is not assessed. This assessment 393 forms the the primary limitation and area of future assessment. In particular, the 394 problems envisaged are largely related to the performance of the MI and CMI estimators 395 in higher dimensions of both parameters and the measurements. While a dimensionality 396 reduction approach was adopted in this study to minimise the adverse effects of the 307 latter, this may not be possible in many forward and inverse problems. Thus, a large area 398 of future work relates to the development of efficient and robust MI and CMI estimators. 399 Lastly, a thorough comparison against classical optimal design methods (C–, E–, T–, 400 V–optimal designs, etc.) needs to be performed, along with the construction and analysis 401 of corresponding information-theoretic metrics. 402

- **Author Contributions:** All authors contributed equally to writing, editing, and reviewing the manuscript. SP and DL conceptualised the information-theoretic framework. AA and SP con-
- ceptualised the application to the biaxial experiments. AA wrote the numerical code for the
- biaxial experiment. SP and DL wrote the code for dimensionality reduction and estimation of
- information-theoretic measures. All authors contributed equally to the analysis of the results.

Funding: This research was funded by the Engineering and Physical Sciences Research Council of the UK (Grant reference EP/R010811/1 to SP) and (Grant reference EP/P018912/1 and EP/P018912/2 to AA).

411 **Conflicts of Interest:** The authors declare no conflict of interest.

#### References

- 1. Holzapfel, G.A. *Nonlinear solid mechanics*; Vol. 24, Wiley Chichester, 2000.
- 2. Zhang, W.; Feng, Y.; Lee, C.H.; Billiar, K.L.; Sacks, M.S. A generalized method for the analysis of planar biaxial mechanical data using tethered testing configurations. *Journal of biomechanical engineering* **2015**, *137*, 064501.
- 3. Labrosse, M.R.; Jafar, R.; Ngu, J.; Boodhwani, M. Planar biaxial testing of heart valve cusp replacement biomaterials: Experiments, theory and material constants. *Acta Biomaterialia* **2016**, *45*, 303–320.
- 4. Humphrey, J.; Yin, F. On constitutive relations and finite deformations of passive cardiac tissue: I. A pseudostrain-energy function. *Journal of biomechanical engineering* **1987**, *109*, 298–304.
- Laurence, D.; Ross, C.; Jett, S.; Johns, C.; Echols, A.; Baumwart, R.; Towner, R.; Liao, J.; Bajona, P.; Wu, Y.; Lee, C.H. An investigation of regional variations in the biaxial mechanical properties and stress relaxation behaviors of porcine atrioventricular heart valve leaflets. *Journal of Biomechanics* 2019, *83*, 16–27. doi:https://doi.org/10.1016/j.jbiomech.2018.11.015.
- Jett, S.V.; Hudson, L.T.; Baumwart, R.; Bohnstedt, B.N.; Mir, A.; Burkhart, H.M.; Holzapfel, G.A.; Wu, Y.; Lee, C.H. Integration of polarized spatial frequency domain imaging (pSFDI) with a biaxial mechanical testing system for quantification of load-dependent collagen architecture in soft collagenous tissues. *Acta Biomaterialia* 2020, 102, 149–168. doi:https://doi.org/10.1016/j.actbio.2019.11.028.
- 7. Billiar, K.L.; Sacks, M.S. Biaxial mechanical properties of the native and glutaraldehyde-treated aortic valve cusp: part II–a structural constitutive model. *Journal of biomechanical engineering* **2000**, *122*, 327–335.
- 8. Ross, C.; Laurence, D.; Wu, Y.; Lee, C.H. Biaxial Mechanical Characterizations of Atrioventricular Heart Valves. *Journal of visualized experiments : JoVE* 2019. doi:10.3791/59170.
- 9. Maurel, W.; Thalmann, D.; Wu, Y.; Thalmann, N.M., Constitutive Modeling. In *Biomechanical Models for Soft Tissue Simulation*; Springer Berlin Heidelberg: Berlin, Heidelberg, 1998; pp. 79–120.
- 10. Holzapfel, G.A.; Gasser, T.C.; Ogden, R.W. A new constitutive framework for arterial wall mechanics and a comparative study of material models. *Journal of elasticity and the physical science of solids* **2000**, *61*, 1–48.

- 11. May-Newman, K.; Yin, F.C.P. A constitutive law for mitral valve tissue. *Journal of Biomechanical Engineering* **1998**, *120*, 38–47. doi:10.1115/1.2834305.
- 12. Pukelsheim, F. Optimal design of experiments; SIAM, 2006.
- 13. Banks, H.T.; Holm, K.; Kappel, F. Comparison of optimal design methods in inverse problems. *Inverse problems* 2011, 27, 075002.
- 14. Banks, H.T.; Dediu, S.; Ernstberger, S.L.; Kappel, F. Generalized sensitivities and optimal experimental design 2010.
- Banks, H.T.; Rubio, D.; Saintier, N.; Troparevsky, M.I. Optimal design techniques for distributed parameter systems. 2013 Proceedings of the Conference on Control and its Applications. SIAM, 2013, pp. 83–90.
- 16. Sebastiani, P.; Wynn, H.P. Maximum entropy sampling and optimal Bayesian experimental design. *Journal of the Royal Statistical Society: Series B (Statistical Methodology)* **2000**, *62*, 145–157.
- 17. Capellari, G.; Chatzi, E.; Mariani, S.; others. Parameter identifiability through information theory. Proceedings of the 2nd ECCOMAS Thematic Conference on Uncertainty Quantification in Computational Sciences and Engineering (UNCECOMP), Rhodes Island, Greece, 2017, pp. 15–17.
- 18. Gasser, T.C.; Ogden, R.W.; Holzapfel, G.A. Hyperelastic modelling of arterial layers with distributed collagen fibre orientations. *Journal of The Royal Society Interface* **2006**, *3*, 15–35. doi:10.1098/rsif.2005.0073.
- 19. Aggarwal, A. An improved parameter estimation and comparison for soft tissue constitutive models containing an exponential function. *Biomechanics and Modeling in Mechanobiology* **2017**, *16*, 1309–1327. doi:10.1007/s10237-017-0889-3.
- 20. Aggarwal, A. Effect of Residual and Transformation Choice on Computational Aspects of Biomechanical Parameter Estimation of Soft Tissues. *Bioengineering* **2019**, *6*. doi:10.3390/bioengineering6040100.
- 21. Pant, S.; Lombardi, D. An information-theoretic approach to assess practical identifiability of parametric dynamical systems. *Mathematical biosciences* **2015**, *268*, 66–79.
- 22. Pant, S. Information sensitivity functions to assess parameter information gain and identifiability of dynamical systems. *Journal of The Royal Society Interface* **2018**, *15*, 20170871.
- 23. Moon, Y.I.; Rajagopalan, B.; Lall, U. Estimation of mutual information using kernel density estimators. *Physical Review E* **1995**, 52, 2318.
- 24. Kraskov, A.; Stögbauer, H.; Grassberger, P. Estimating mutual information. *Physical Review E* 2004, 69, 066138.
- 25. Lombardi, D.; Pant, S. Nonparametric k-nearest-neighbor entropy estimator. Physical Review E 2016, 93, 013310.
- 26. Beirlant, J.; Dudewicz, E.J.; Györfi, L.; Van der Meulen, E.C. Nonparametric entropy estimation: An overview. *International Journal of Mathematical and Statistical Sciences* **1997**, *6*, 17–39.
- 27. Gao, S.; Ver Steeg, G.; Galstyan, A. Efficient estimation of mutual information for strongly dependent variables. Artificial intelligence and statistics. PMLR, 2015, pp. 277–286.
- Benner, P.; Gugercin, S.; Willcox, K. A survey of projection-based model reduction methods for parametric dynamical systems. SIAM review 2015, 57, 483–531.
- 29. Benner, P.; Ohlberger, M.; Cohen, A.; Willcox, K. Model reduction and approximation: theory and algorithms; SIAM, 2017.
- 30. Quarteroni, A.; Rozza, G.; others. Reduced order methods for modeling and computational reduction; Vol. 9, Springer, 2014.
- 31. Ma, Y.; Fu, Y. Manifold learning theory and applications; CRC press, 2011.
- 32. Amsallem, D.; Haasdonk, B. PEBL-ROM: Projection-error based local reduced-order models. *Advanced Modeling and Simulation in Engineering Sciences* **2016**, *3*, 1–25.
- 33. Maday, Y.; Stamm, B. Locally adaptive greedy approximations for anisotropic parameter reduced basis spaces. *SIAM Journal on Scientific Computing* **2013**, *35*, A2417–A2441.