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Stability of Sampled-Data Control for Lurie Systems with Slope-Restricted Nonlinearities ^{*}

Mathias Giordani Tilton ^{*} João Manoel Gomes da Silva Jr. ^{*}
Giórgio Valmórbida ^{**}

^{*} *Programa de Pós-Graduação em Engenharia Elétrica (PPGEE),
Universidade Federal do Rio Grande do Sul (UFRGS).*
(e-mails: mathias.tilton@ufrgs.br; jmgomes@ufrgs.br)

^{**} *Laboratoire des Signaux et Systèmes, CentraleSupélec,
CNRS, Université Paris-Saclay.*
(e-mail: giorgio.valmorbida@l2s.centralesupelec.fr)

Abstract: This paper deals with the stability analysis of aperiodic sampled-data Lurie systems, where the nonlinearity is assumed to be both sector and slope restricted. The proposed method is based on the use of a new class of looped-functionals whose derivative is negative along the trajectories of the continuous-time system. In addition, it contains a generalized Lurie-type function that is quadratic on both the states and the nonlinearity and has a Lurie-Postnikov integral term, which provides some advantages in comparison to simpler candidate functions. On this basis, stability conditions in the form of linear matrix inequalities (LMIs) are formulated. It is shown that the proposed conditions guarantee that the Lurie function is strictly decreasing at the sampling instants, which also implies that the continuous-time trajectories converge asymptotically to the origin. We then formulate some optimization problems for computing the maximal intersampling interval or the maximal sector bounds for which the stability of the sampled-data closed-loop system is guaranteed. A numerical example to illustrate the results is provided.

Resumo: Este artigo trata da análise de estabilidade de sistemas do tipo Lurie com controle amostrado aperiódicamente, onde assume-se que a não linearidade é limitada em setor e em derivada. O método proposto é baseado no uso de uma nova classe de funcionais em *loop* cuja derivada é negativa ao longo das trajetórias do sistema em tempo contínuo. Além disso, contém uma função generalizada do tipo Lurie que é quadrática tanto nos estados quanto na não linearidade e possui um termo integral de Lurie-Postnikov, oferecendo algumas vantagens em comparação com funções candidatas mais simples. A partir destes elementos, são formuladas condições de estabilidade na forma de inequações lineares matriciais (LMIs). É demonstrado que as condições propostas garantem que a função Lurie seja estritamente decrescente nos instantes de amostragem, o que também implica que as trajetórias em tempo contínuo convergem assintoticamente para a origem. São então formulados alguns problemas de otimização para obter o intervalo máximo entre amostragens ou os limites máximos do setor para os quais a estabilidade do sistema em malha-fechada com controle amostrado é garantida. Os resultados são ilustrados em um exemplo numérico.

Keywords: Sampled-data control; Lurie systems; stability analysis; sector bounded nonlinearities; *looped-functional* approach.

Palavras-chaves: Controle amostrado; sistemas Lurie; análise de estabilidade; não-linearidades limitadas em setor; abordagem *looped-functional*.

1. INTRODUCTION

The study of the stability and stabilization of systems evolving in continuous-time whereas the controller deliver

inputs at discrete-time instants, *i.e.*, sampled-data control, has been the subject of many works in the literature.

In (Åström and Wittenmark, 2013) linear sampled-data control systems updated at constant sampling periods were extensively studied. However, with the recently growth of networked control applications, asynchronous sampling has been receiving a lot of attention in the literature (Hetel et al., 2017). On the other hand, the fact that for nonlinear systems the exact discretization does not hold, makes the

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stability analysis difficult even in the periodic sampling case. To conclude about the stability of the sampled-data control of nonlinear systems, its hybrid behavior has to be taken into account. Then, it is clear the motivation for developing stability conditions for sampled-data control systems which take into account the variations on the intersampling time as well as nonlinear dynamics.

Different techniques have been proposed in the literature to model sampled-data systems, like the lifting approach (Bamieh et al., 1991), where the problem is transformed into an equivalent finite-dimensional discrete-time problem while keeping the intersampling information of the system; the impulsive modeling, in which a time-varying Lyapunov function is used (Hu et al., 2002), (Naghshabrizi et al., 2008); the modeling with a continuous-time system with time-varying delay on the plant control input (Fridman et al., 2004), (Fridman, 2010); and the looped-functional approach (Seuret, 2012), (Seuret and Gomes da Silva Jr., 2012) that focus on the behavior in the intersampling interval, ensuring that a positive definite function is strictly decreasing at the sampling instants. For a general overview of these approaches and other ones, the reader can refer to (Hetel et al., 2017).

Much research has been dedicated to Lurie-type nonlinear systems, which consists of a linear time-invariant (LTI) plant connected with a nonlinearity that satisfies some sector restrictions. Considering this class of nonlinear systems, we can mention, for example, works focusing on stabilization (Castelan et al., 2008), Event-Triggered Control (ETC) (Zhang et al., 2019) and synchronization of chaotic systems (Park et al., 2018). Lurie systems with network delays are dealt with in (Hao and Zhao, 2010), (Zeng et al., 2011). Sampled-data systems, which are the focus of this work, were addressed in (Seifullaev and Fradkov, 2013), which uses a Lyapunov-Krasovskii functional and state feedback control law, with extension for robust control in (Seifullaev and Fradkov, 2016). In (Seifullaev and Fradkov, 2015), the authors use an approach from the standpoint of systems passification, with control by linear output feedback.

In these contexts, different classes of Lyapunov Functions (LFs), *e.g.* quadratic ones (associated to the Circle criterion) (Khalil, 2002), Lurie-Postnikov LFs (associated to the Popov criterion) (Yakubovich, 1965), (Suykens et al., 1998), (Park, 2002) and composite LFs (Hu et al., 2004) have been considered. To deal with sampled-data control systems, Lyapunov-Krasovskii functionals, as proposed in (Fridman, 2010), are in general used. These functionals are required to be positive definite and does not depend on the nonlinearity.

This paper focus on the stability analysis of the sampled-data closed-loop Lurie system. Our approach combines a generalized Lurie function (as Valmorbidia et al. (2018)) that does not require the positivity-definiteness of the quadratic part nor the positivity of the Lurie-Postnikov coefficients, with a particular looped-functional (similar to the one used in Seuret and Gomes da Silva Jr. (2012) for input saturated systems).

From these elements, we propose LMI conditions to assess the global asymptotic stability of the origin of the system. In particular, these conditions ensure that a generalized

Lurie function is strictly decreasing at sampling instants. Hence, from the Lurie-type system structure we show that this fact implies the asymptotic convergence of the continuous-time trajectories of the plant to the origin. The LMI conditions can therefore be incorporated as constraints in optimization problems that allow us to compute bounds for the maximal intersampling interval or the maximal sector bounds for which the stability of the Lurie-type system under aperiodic sampled-data control can be ensured.

This paper is organized as follows. The next section describes the problem formulation. Section 3 presents preliminary lemmas for the sector conditions and generalized Lurie-type functions, as well as the functional approach, which will be used to develop the LMI conditions. In Section 4 we derive a theorem to evaluate the asymptotic stability of the closed-loop system under aperiodic sampled-data control. Section 5 features some optimization problems and Section 6 gives a numerical example to highlight the potentialities of the method. Section 7 summarizes at the main points covered in the article.

Notation: The set of diagonal matrices of dimension n is denoted \mathbb{D}^n and $\mathbb{D}_{\geq 0}^n$ means that the matrix is also positive semi-definite. To express diagonal matrices in a compact form, we write ‘diag(e_1, \dots, e_n)’, where e_i , $i = 1, \dots, n$ are, respectively, the elements in position (i, i) . The set of symmetric matrices of dimension n is denoted \mathbb{S}^n and $\mathbb{S}_{\geq 0}^n$ means that the matrix is also positive semi-definite. A^T denotes the transpose of matrix A . $\text{He}(A) := A + A^T$, I_m and 0_m are, respectively, the identity and zero square matrices of order m . For a given positive scalar, \mathcal{J}_2 , define \mathbb{K} as the set of continuous functions from an interval $[0, Z]$ to \mathbb{R}^n , where Z is a positive scalar less than \mathcal{J}_2 . The notations $|\cdot|$ and $\|\cdot\|$ represents the absolute value of a scalar and the Euclidean norm, respectively. The i th element of a vector v is denoted by v_i . $P \succ 0$ ($P \succeq 0$) means that P is positive (semi-)definite and $P \prec 0$ ($P \preceq 0$) means that P is negative (semi-)definite. We denote the time-derivative of a time function, x by \dot{x} and we use ∂ to denote the sub-differential operator. The symmetric terms in a symmetric matrix are denoted by $*$. We drop the arguments of some functions when it is clear from the context.

2. PROBLEM STATEMENT

Consider the continuous-time plant described by the following Lurie system:

$$\begin{cases} \dot{x}(t) = Ax(t) + B_u u(t) + B_\phi \phi(y(t)) \\ y(t) = Cx(t) \end{cases}, \quad (1)$$

where $x \in \mathbb{R}^n$ represents the states of the plant, $u \in \mathbb{R}^q$ represents its input and $y \in \mathbb{R}^m$ is the output vector. Matrices $A \in \mathbb{R}^{n \times n}$, $B_u \in \mathbb{R}^{n \times q}$, $B_\phi \in \mathbb{R}^{n \times m}$, $C \in \mathbb{R}^{m \times n}$, are known and supposed to be constant.

The nonlinearity $\phi : \mathbb{R}^m \rightarrow \mathbb{R}^m$, is assumed to be time-invariant, memoryless, Lipschitz on \mathbb{R}^m , decentralized, sector bounded and slope restricted, *i.e.*, $\phi(y) = [\phi_1(y_1) \dots \phi_m(y_m)]^T$, with $\phi_i(y_i)$ satisfying, $\forall i = 1, \dots, m$

$$\phi_i(0) = 0 \quad (2a)$$

$$\frac{\phi_i(y_i)}{y_i} \in [\underline{\delta}_i, \bar{\delta}_i] \quad \forall y \in \mathbb{R}^m \quad (2b)$$

$$\partial\phi_i(y_i) \in [\underline{\gamma}_i, \bar{\gamma}_i], \quad \forall y \in \mathbb{R}^m, \quad (2c)$$

where $\underline{\delta}_i \in \mathbb{R}$, $\bar{\delta}_i \in \mathbb{R}$, $\underline{\delta}_i \leq \bar{\delta}_i$ are, respectively, the lower and upper sector bounds for the i th nonlinearity and $\underline{\gamma}_i \in \mathbb{R}$, $\bar{\gamma}_i \in \mathbb{R}$, $\underline{\gamma}_i \leq \bar{\gamma}_i$ are, respectively, the lower and upper slope bounds for the i th nonlinearity. Let us also introduce the matrices $\underline{\Delta} := \text{diag}(\underline{\delta}_1, \dots, \underline{\delta}_m)$, $\bar{\Delta} := \text{diag}(\bar{\delta}_1, \dots, \bar{\delta}_m)$, $\underline{\Gamma} := \text{diag}(\underline{\gamma}_1, \dots, \underline{\gamma}_m)$, $\bar{\Gamma} := \text{diag}(\bar{\gamma}_1, \dots, \bar{\gamma}_m)$ to express the sector and slope conditions in matrix format. The Lipschitz assumption on ϕ implies that $\partial\phi_i(y_i) = \frac{d\phi_i}{dy_i}$ almost everywhere, relaxing the requirement for the nonlinearity to be continuously differentiable.

We suppose that the control signal u comes from a digital controller and it is updated at sampling instants $t = t_k$, remaining constant between two successive sampling instants through a zero-order hold (ZOH). Thus, $\{t_k\}_{k \in \mathbb{N}}$ is an increasing sequence of positive scalars such that $\bigcup_{k \in \mathbb{N}} [t_k, t_{k+1}) = [0, +\infty)$. Since we are considering the generic case of aperiodic sampling, assume that there exist two positive scalars $\mathcal{T}_1 \leq \mathcal{T}_2$ such that the difference between two successive sampling instants $T_k = t_{k+1} - t_k$ satisfies

$$0 < \mathcal{T}_1 \leq T_k \leq \mathcal{T}_2, \quad \forall k \in \mathbb{N}. \quad (3)$$

Note that in periodic sampling we assume in particular that T_k must have the same value $\forall k \in \mathbb{N}$, i.e., $T_k = \mathcal{T}_1 = \mathcal{T}_2, \forall k$.

In particular, we consider the following generic sampled-data control law:

$$\begin{aligned} u(t) &= K_x x(t_k) + K_\phi \phi(y(t_k)) \\ &= K_x x(t_k) + K_\phi \phi(Cx(t_k)), \quad \forall t \in [t_k, t_{k+1}), \end{aligned} \quad (4)$$

where $K_x \in \mathbb{R}^{q \times n}$, $K_\phi \in \mathbb{R}^{q \times m}$. This control law allows to use information about the nonlinearities (Castelan et al., 2008). If nonlinearities cannot be measured or if the control law is simply a state-feedback, just consider $K_\phi = 0$.

In this paper, we are interested in formulating conditions that allow us to evaluate the global asymptotic stability of the system (1) with nonlinearities satisfying sector and slope restrictions (2), subject to aperiodic sampling (3) and control law given by (4).

3. PRELIMINARIES

In this section, we present the inequalities verified by the sector and slope bounded nonlinearity. These inequalities will play a very important role to obtain conditions to assess the stability of the closed-loop system (1)-(4).

3.1 Sector Conditions

Define $S_\Delta : \mathbb{R}^{m \times m} \times \mathbb{R}^m \times \mathbb{R}^m \rightarrow \mathbb{R}$, $S_\Gamma : \mathbb{R}^{m \times m} \times \mathbb{R}^m \times \mathbb{R}^m \rightarrow \mathbb{R}$ as

$$\begin{aligned} S_\Delta(U, \phi, \kappa) &:= (\phi - \underline{\Delta}\kappa)^T U (\bar{\Delta}\kappa - \phi) \\ S_\Gamma(U, \phi, \kappa) &:= (\phi - \underline{\Gamma}\kappa)^T U (\bar{\Gamma}\kappa - \phi). \end{aligned}$$

Lemma 1. (Khalil, 2002). If $U_1 \in \mathbb{D}_{\geq 0}^m$ and $\phi : \mathbb{R}^m \rightarrow \mathbb{R}^m$ satisfies (2), then

$$S_\Delta(U_1, \phi(\kappa), \kappa) \geq 0 \quad (5)$$

for all $\kappa \in \mathbb{R}^m$.

Lemma 2. (Valmorbida et al., 2018). If $U_2 \in \mathbb{D}_{\geq 0}^m$ and $\phi : \mathbb{R}^m \rightarrow \mathbb{R}^m$ satisfies (2), then

$$S_\Gamma(U_2, \dot{\phi}(\kappa), \dot{\kappa}) \geq 0 \quad (6)$$

almost everywhere for $\kappa \in \mathbb{R}^m$.

3.2 Looped-Functional Approach

Define, as in (Seuret, 2012), $x_k(\tau) := x(t_k + \tau)$, $y_k(\tau) := y(t_k + \tau)$ and $\phi_k(\tau) := \phi(y_k(\tau))$. Hence, the behavior of the closed-loop system in the interval $[t_k, t_{k+1})$ can be described by:

$$\begin{cases} \dot{x}_k(\tau) = Ax_k(\tau) + B_\phi \phi_k(\tau) + B_u(K_x x_k(0) + K_\phi \phi_k(0)) \\ y_k(\tau) = Cx_k(\tau) \end{cases} \quad \forall \tau \in [0, T_k), \quad (7)$$

where $\dot{x}_k(\tau) = \frac{d}{d\tau} x_k(\tau)$. Using representation (7), and inspired by the results in Seuret and Gomes da Silva Jr. (2012) considering linear sampled-data control systems subject to actuator saturation, the following theorem regarding the looped-functional approach to assess the closed-loop stability of a Lurie-type system can be stated.

Theorem 1. Let $V : \mathbb{R}^n \rightarrow \mathbb{R}^+$ be a differentiable function such that

$$\mu_1 \|x\|^p \leq V(x) \leq \mu_2 \|x\|^p, \quad \forall x \in \mathbb{R}^n, \quad (8)$$

with $\mu_1, \mu_2 > 0$, $p > 0$, and let $\mathcal{W}_0 : [0, \mathcal{T}_2] \times \mathbb{K} \times [\mathcal{T}_1, \mathcal{T}_2] \rightarrow \mathbb{R}$ be a continuous and differentiable functional, called a looped-functional, that satisfies for all $z \in \mathbb{K}$ and for all $T_k \in [\mathcal{T}_1, \mathcal{T}_2]$

$$\mathcal{W}_0(T_k, z, T_k) = \mathcal{W}_0(0, z, T_k). \quad (9)$$

If for all $k \in \mathbb{N}$, $T_k \in [\mathcal{T}_1, \mathcal{T}_2]$ and $\tau \in [0, T_k]$ one has

$$\dot{\mathcal{W}}(\tau, x_k, T_k) = \frac{d}{d\tau} [V(x_k(\tau)) + \mathcal{W}_0(\tau, x_k, T_k)] < 0, \quad (10)$$

then considering the solutions of the system (1) with the sampled-data control law (4) it follows that

- (i) $\Delta V(k) = V(x_{k+1}(0)) - V(x_k(0)) = V(x(t_{k+1})) - V(x(t_k)) < 0, \forall k \in \mathbb{N}$;
- (ii) $x(t) \rightarrow 0$ as $t \rightarrow \infty, \forall x(0) \in \mathbb{R}^n$, i.e. the origin is globally asymptotically stable (GAS).

Proof. First note that, by continuity of the system trajectories $x_k(T_k) = x_{k+1}(0)$. Integrating now (10) in the interval $[0, T_k]$ and using (9), we conclude that this inequality implies that $\Delta V(k) = V(x_{k+1}(0)) - V(x_k(0)) = V(x(t_{k+1})) - V(x(t_k)) < 0, \forall k \in \mathbb{N}$. Thus, we can conclude that $x_k(0) = x(t_k) \rightarrow 0$ as $k \rightarrow \infty$.

To conclude the proof, we need to show that the continuous-time trajectories also converge to the origin, i.e., $x(t) \rightarrow 0$ as $t \rightarrow \infty$ and that $x(t)$ is uniformly bounded for all $t \in [t_k, t_{k+1})$, $\forall k$.

For this, note that as $\frac{\phi_i(y_i)}{y_i} \in [\underline{\delta}_i, \bar{\delta}_i]$, it follows that, $\forall t$, there exists a scalar $\alpha(t)$, $0 \leq \alpha(t) < 1$ such that

$$\begin{aligned} \phi_i(y_i(t)) &= [\alpha(t)\underline{\delta}_i + (1 - \alpha(t))\bar{\delta}_i] y_i(t) \\ &= v_i(t) y_i(t), \quad \text{with } v_i(t) \in [\underline{\delta}_i, \bar{\delta}_i]. \end{aligned} \quad (11)$$

Thus, we can write $\phi(y(t)) = \Upsilon(v(t))y(t)$, with $\Upsilon(v(t)) = \text{diag}(v_1(t), v_2(t), \dots, v_m(t))$, $v(t) \in \mathcal{U}_v = \{v \in \mathbb{R}^m \mid \underline{\delta}_i < v_i < \bar{\delta}_i, i = 1, \dots, m\}$. Hence, the closed-loop system can be represented by the following linear time-varying system:

$$\begin{aligned} \dot{x}(t) = & Ax(t) + B_u(K_x x(t_k) + K_\phi \phi(y(t_k))) \\ & + B_\phi \Upsilon(v(t))Cx(t), \forall t \in [t_k, t_{k+1}). \end{aligned} \quad (12)$$

Considering the lifted-variables one has

$$\begin{aligned} \dot{x}_k(\tau) = & (A + B_\phi \Upsilon(v_k(\tau))C)x_k(\tau) \\ & + B_u(K_x x_k(0) + K_\phi \phi_k(0)). \end{aligned} \quad (13)$$

For each admissible $v(t) \in \mathcal{U}_v$, we can define a transition matrix $\Psi_v(t, t_0)$ for system (12). Defining $v_k(\tau) := v(t_k + \tau)$, $\Psi_{v_k}(\tau) := \Psi_v(t_k + \tau, t_k)$ as the restriction of $\Psi_v(t, t_0)$ to the interval $[t_k, t_{k+1})$, and the state transition matrix $\Psi_{v_k}(\tau, s) := \Psi_v(t_k + \tau, t_k + s)$, it follows that

$$x_k(\tau) = \Psi_{v_k}(\tau, 0)x_k(0) + \int_0^\tau \Psi_{v_k}(\tau, s)B_u \begin{bmatrix} K_x & K_\phi \end{bmatrix} \begin{bmatrix} x_k(0) \\ \phi_k(0) \end{bmatrix} ds. \quad (14)$$

Thus, we have that

$$\begin{aligned} \|x_k(\tau)\| & \leq \|\Psi_{v_k}(\tau, 0)\| \|x_k(0)\| + \left\| \int_0^\tau \Psi_{v_k}(\tau, s) ds \right\| \times \\ & \quad \left\| B_u \begin{bmatrix} K_x & K_\phi \end{bmatrix} \begin{bmatrix} x_k(0) \\ \phi_k(0) \end{bmatrix} \right\| \\ & \leq \left(\|\Psi_{v_k}(\tau, 0)\| + \left\| \int_0^\tau \Psi_{v_k}(\tau, s) ds \right\| (\|B_u K_x\| \right. \\ & \quad \left. + \|B_u K_\phi\| \|\bar{\Delta} C\|) \right) \|x_k(0)\| \\ & \leq \left(\|\Psi_{v_k}(\tau, 0)\| + \int_0^{\mathcal{J}_2} \|\Psi_{v_k}(\tau, s) ds\| (\|B_u K_x\| \right. \\ & \quad \left. + \|B_u K_\phi \bar{\Delta} C\|) \right) \|x_k(0)\|. \end{aligned} \quad (15)$$

As $v_k(\tau) \in \mathcal{U}_v, \forall \tau \in [0, \mathcal{J}_2]$, there exists a scalar μ_Ψ , such that

$$\|x_k(\tau)\| \leq \mu_\Psi \|x_k(0)\|, \quad (16)$$

where

$$\begin{aligned} \mu_\Psi = & \sup_{v_k(\tau) \in \mathcal{U}_v} \left(\|\Psi_{v_k}(\tau, 0)\| + \int_0^{\mathcal{J}_2} \|\Psi_{v_k}(\tau, s) ds\| \times \right. \\ & \left. (\|B_u K_x\| + \|B_u K_\phi\| \|\bar{\Delta}\| \|C\|) \right). \end{aligned}$$

Hence, if $x_k(0) \rightarrow 0$ as $k \rightarrow \infty$, i.e., $x(t_k) \rightarrow 0$ as $k \rightarrow \infty$, then $x(t_k + \tau) = x_k(\tau) \rightarrow 0$ as $k \rightarrow \infty, \forall \tau \in [0, T_k]$, that is $x(t) = x(t_k + \tau) \rightarrow 0$ as $t \rightarrow \infty$. \square

3.3 Generalized Lurie Function

Consider a generalized Lurie function $V : \mathbb{R}^n \rightarrow \mathbb{R}$ defined as follows

$$V(x) = V_0(x) + \sum_{i=1}^m \lambda_i \int_0^{y_i} (\phi_i(s) - \underline{\delta}_i s) ds, \quad (17)$$

where $y_i = (Cx)_i, i = 1, \dots, m$ and

$$V_0(x) = \begin{bmatrix} x \\ \phi(y) \end{bmatrix}^T \begin{bmatrix} P_{11} & P_{12} \\ P_{12}^T & P_{22} \end{bmatrix} \begin{bmatrix} x \\ \phi(y) \end{bmatrix}. \quad (18)$$

This function is an extended version of the traditional Lurie function, where the matrix P and the coefficients λ_i (also known as Lurie-Postnikov terms), $\Lambda := \text{diag}(\lambda_1, \dots, \lambda_i), i = 1, \dots, m$, are necessarily positive-definite. Note that this form does not require the positive-definiteness of P , nor the non-negativity of the coefficients λ_i (Valmorbida et al., 2018). In this case, the positivity-definiteness of V should be ensured by other means, as stated in the following lemma.

Lemma 3. (Valmorbida et al., 2018). Consider V in (17) where ϕ satisfies (2a)-(2b). If there exists a matrix $\tilde{\Lambda} \in \mathbb{D}_{\geq 0}^m$ such that

$$\Lambda \succeq -\tilde{\Lambda}, \quad (19)$$

$$V_0(x) - \frac{1}{2} y^T (\bar{\Delta} - \underline{\Delta}) \tilde{\Lambda} y > 0, \quad \forall x \in \mathbb{R}^n, \quad (20)$$

then $V(x) > 0, \forall x \in \mathbb{R}^n$.

4. ASYMPTOTIC STABILITY CONDITIONS

In this section, we derive conditions in the form of linear matrix inequalities (LMIs) to assess the asymptotic stability of the sampled-data closed-loop system (1)-(4). The approach is based on the use of looped-functionals (Seuret and Gomes da Silva Jr., 2012) and a generalized Lurie-type function (Valmorbida et al., 2018). With this aim, we apply *Theorem 1*, considering the function $V(x)$ defined in (17) and the functional

$$\begin{aligned} \mathcal{W}_0(\tau, x_k, T_k) = & (T_k - \tau) \left\{ \int_0^\tau \dot{x}_k^T(\theta) R_x \dot{x}_k(\theta) d\theta \right. \\ & \left. + (x_k(\tau) - x_k(0))^T [F_x(x_k(\tau) - x_k(0)) + 2G_x x_k(0)] \right\} \\ & + (T_k - \tau) \left\{ \tau \begin{bmatrix} x_k(0) \\ \phi_k(0) \end{bmatrix}^T X \begin{bmatrix} x_k(0) \\ \phi_k(0) \end{bmatrix} + \int_0^\tau \dot{\phi}_k^T(\theta) R_\phi \dot{\phi}_k(\theta) d\theta \right. \\ & \left. + (\phi_k(\tau) - \phi_k(0))^T [F_\phi(\phi_k(\tau) - \phi_k(0)) + 2G_\phi \phi_k(0)] \right\} \end{aligned} \quad (21)$$

with $F_x \in \mathbb{S}^n, G_x \in \mathbb{R}^{n \times n}, X \in \mathbb{S}^{n+m}, F_\phi \in \mathbb{S}^m, G_\phi \in \mathbb{R}^{m \times m}, R_x \in \mathbb{S}_{>0}^n$ and $R_\phi \in \mathbb{S}_{>0}^m$.

The following theorem provides LMI conditions to verify the stability of the closed-loop system under aperiodic sampling.

Theorem 2. Assume that there exist a matrix $P \in \mathbb{S}^{n+m}$, matrices $\Lambda \in \mathbb{D}^m, \tilde{\Lambda} \in \mathbb{D}_{\geq 0}^m$, matrices $U_j, j = 0, \dots, 3 \in \mathbb{D}_{\geq 0}^n$, matrices $F_x \in \mathbb{S}^n, G_x \in \mathbb{R}^{n \times n}, F_\phi \in \mathbb{S}^m, G_\phi \in \mathbb{R}^{m \times m}, R_x \in \mathbb{S}_{>0}^n, R_\phi \in \mathbb{S}_{>0}^m, Q_x \in \mathbb{R}^{(3n) \times n}, Q_\phi \in \mathbb{R}^{(3m) \times m}, X \in \mathbb{S}^{n+m}, Y_1, Y_2 \in \mathbb{R}^{n \times n}$ that satisfy, for $i = 1, 2$:

$$\Psi_1(\mathcal{J}_i) = \Pi_1 + \mathcal{J}_i \Pi_2 + \mathcal{J}_i \Pi_3 < 0 \quad (22)$$

$$\Psi_2(\mathcal{J}_i) = \begin{bmatrix} \Pi_1 - \mathcal{J}_i \Pi_3 & \mathcal{J}_i M_{135}^T Q_x & \mathcal{J}_i M_{246}^T Q_\phi \\ * & -\mathcal{J}_i R_x & 0 \\ * & * & -\mathcal{J}_i R_\phi \end{bmatrix} < 0 \quad (23)$$

$$\Lambda \succeq -\tilde{\Lambda} \quad (24)$$

$$P - \frac{1}{2} \begin{bmatrix} C^T \\ 0 \end{bmatrix} (\bar{\Delta} - \underline{\Delta}) \tilde{\Lambda} \begin{bmatrix} C & 0 \end{bmatrix} + \text{He} \left\{ \frac{1}{2} \begin{bmatrix} (\underline{\Delta} C)^T \\ -I_m \end{bmatrix} U_0 [\bar{\Delta} C \quad -I_m] \right\} \succ 0, \quad (25)$$

with

$$\begin{aligned} \Pi_1 &= \text{He}\{M_{12}^T P M_{34}\} - M_{15}^T F_x M_{15} - \text{He}\{M_{15}^T G_x M_5\} \\ &\quad - \text{He} \left\{ \frac{1}{2} (M_1^T (\underline{\Delta} C)^T - M_2^T) \Lambda C M_3 \right\} \\ &\quad - M_{26}^T F_\phi M_{26} - \text{He}\{M_{26}^T G_\phi M_6\} \\ &\quad + \text{He}\{M_2^T - M_1^T (\underline{\Delta} C)^T\} U_1 (\bar{\Delta} C M_1 - M_2) \\ &\quad + \text{He}\{M_4^T - M_3^T (\underline{\Gamma} C)^T\} U_2 (\bar{\Gamma} C M_3 - M_4) \\ &\quad + \text{He}\{M_6^T - M_5^T (\underline{\Delta} C)^T\} U_3 (\bar{\Delta} C M_5 - M_6) \\ &\quad - \text{He}\{M_{135}^T Q_x M_{15}\} - \text{He}\{M_{246}^T Q_\phi M_{26}\} \\ &\quad + \text{He}\{(M_1^T Y_1^T + M_3^T Y_2^T) M_0\} \\ \Pi_2 &= M_3^T R_x M_3 + \text{He}\{M_3^T (F_x M_{15} + G_x M_5)\} \\ &\quad + M_4^T R_\phi M_4 + \text{He}\{M_4^T (F_\phi M_{26} + G_\phi M_6)\} \\ \Pi_3 &= M_{56}^T X M_{56}, \end{aligned}$$

where¹

$$\begin{aligned} M_0 &= [A \quad B_\phi \quad -I \quad 0 \quad B_u K_x \quad B_u K_\phi] \\ M_1 &= [I \quad 0 \quad 0 \quad 0 \quad 0 \quad 0] \quad M_2 = [0 \quad I \quad 0 \quad 0 \quad 0 \quad 0] \\ M_3 &= [0 \quad 0 \quad I \quad 0 \quad 0 \quad 0] \quad M_4 = [0 \quad 0 \quad 0 \quad I \quad 0 \quad 0] \\ M_5 &= [0 \quad 0 \quad 0 \quad 0 \quad I \quad 0] \quad M_6 = [0 \quad 0 \quad 0 \quad 0 \quad 0 \quad I] \\ M_{15} &= M_1 - M_5 \quad M_{26} = M_2 - M_6 \\ M_{12} &= [M_1^T \quad M_2^T]^T \quad M_{34} = [M_3^T \quad M_4^T]^T \\ M_{56} &= [M_5^T \quad M_6^T]^T \quad M_{135} = [M_1^T \quad M_3^T \quad M_5^T]^T \\ M_{246} &= [M_2^T \quad M_4^T \quad M_6^T]^T. \end{aligned}$$

Then the origin of the sampled-data closed-loop system (1)-(4) is GAS.

Proof. Considering the result of *Theorem 1*, the idea is to prove that (9) and (10) are satisfied, $\forall k \in \mathbb{N}$, considering V and W_0 as given in (17) and (21), respectively.

It is straightforward to proof the positivity of V given by the inequalities (24) and (25) using *Lemma 1* and *Lemma 3*. The next step of the proof focuses on the fact that the functional W_0 given in (21) satisfies the condition (9). Since $(T_k - \tau) = 0$ when $\tau = T_k$ and $x_k(\tau) - x_k(0) = 0$ when $\tau = 0$, it follows that the functional W_0 satisfies (9). Moreover, it is continuous at all sampling instants and differentiable over $[0, T_k]$. The rest of the proof consists in showing that (22)-(23) implies (10). With this aim, the expression of \dot{W} is given as follows:

$$\begin{aligned} \dot{W}(\tau, x_k, T_k) &= 2 \begin{bmatrix} x_k(\tau) \\ \phi_k(\tau) \end{bmatrix}^T P \begin{bmatrix} \dot{x}_k(\tau) \\ \dot{\phi}_k(\tau) \end{bmatrix} \\ &\quad - [(x_k^T(\tau) (\underline{\Delta} C)^T - \phi_k^T(\tau) \Lambda C) \dot{x}_k(\tau) \\ &\quad - (x_k(\tau) - x_k(0))^T [F_x(x_k(\tau) - x_k(0)) + 2G_x x_k(0)] \\ &\quad + (T_k - \tau) \dot{x}_k^T(\tau) [R_x \dot{x}_k(\tau) + 2F_x(x_k(\tau) - x_k(0)) \\ &\quad + 2G_x x_k(0)] + (T_k - 2\tau) \begin{bmatrix} x_k(0) \\ \phi_k(0) \end{bmatrix}^T X \begin{bmatrix} x_k(0) \\ \phi_k(0) \end{bmatrix} \\ &\quad - (\phi_k(\tau) - \phi_k(0))^T [F_\phi(\phi_k(\tau) - \phi_k(0)) + 2G_\phi \phi_k(0)] \\ &\quad + (T_k - \tau) \dot{\phi}_k^T(\tau) [R_\phi \dot{\phi}_k(\tau) + 2F_\phi(\phi_k(\tau) - \phi_k(0)) \\ &\quad + 2G_\phi \phi_k(0)] - \int_0^\tau \dot{x}_k^T(\theta) R_x \dot{x}_k(\theta) d\theta \\ &\quad - \int_0^\tau \dot{\phi}_k^T(\theta) R_\phi \dot{\phi}_k(\theta) d\theta. \end{aligned} \quad (26)$$

Using the sector conditions defined in *Lemma 1* and *Lemma 2*, we have that

$$\begin{aligned} \dot{W}(\tau, x_k, T_k) &< \dot{W}(\tau, x_k, T_k) + 2S_\Delta(U_1, \phi_k(\tau), y_k(\tau)) \\ &\quad + 2S_\Gamma(U_2, \dot{\phi}_k(\tau), \dot{y}_k(\tau)) + 2S_\Delta(U_3, \phi_k(0), y_k(0)), \end{aligned}$$

or equivalently

$$\begin{aligned} \dot{W}(\tau, x_k, T_k) &< \dot{W}(\tau, x_k, T_k) \\ &\quad + 2(\phi_k^T(\tau) - x_k^T(\tau) (\underline{\Delta} C)^T) U_1 (\bar{\Delta} C x_k(\tau) - \phi_k(\tau)) \\ &\quad + 2(\dot{\phi}_k^T(\tau) - \dot{x}_k^T(\tau) (\underline{\Gamma} C)^T) U_2 (\bar{\Gamma} C \dot{x}_k(\tau) - \dot{\phi}_k(\tau)) \\ &\quad + 2(\phi_k^T(0) - x_k^T(0) (\underline{\Delta} C)^T) U_3 (\bar{\Delta} C x_k(0) - \phi_k(0)). \end{aligned} \quad (27)$$

Consider the vector $\eta_k(\tau) = [x_k^T(\tau) \quad \phi_k^T(\tau) \quad \dot{x}_k^T(\tau) \quad \dot{\phi}_k^T(\tau) \quad x_k^T(0) \quad \phi_k^T(0)]^T$, the vector $\zeta_k(\tau) = M_{135} \eta_k(\tau)$ and a matrix $Q_x \in \mathbb{R}^{(3n) \times n}$. Since R_x is assumed to be positive definite, it follows that $(\dot{x}_k(\theta) - R_x^{-1} Q_x^T \zeta_k(\tau))^T R_x (\dot{x}_k(\theta) - R_x^{-1} Q_x^T \zeta_k(\tau)) > 0$. Integrating this expression over $[0, \tau]$, the following inequality is obtained

$$\begin{aligned} \int_0^\tau \dot{x}_k^T(\theta) R_x \dot{x}_k(\theta) d\theta - 2\zeta_k^T(\tau) Q_x (x_k(\tau) - x_k(0)) \\ + \tau \zeta_k^T(\tau) Q_x R_x^{-1} Q_x^T \zeta_k(\tau) \geq 0. \end{aligned} \quad (28)$$

Consider now a new vector $\psi_k(\tau) = M_{246} \eta_k(\tau)$ and a matrix $Q_\phi \in \mathbb{R}^{(3m) \times m}$. Following the same reasoning as above, we have that:

$$\begin{aligned} \int_0^\tau \dot{\phi}_k^T(\theta) R_\phi \dot{\phi}_k(\theta) d\theta - 2\psi_k^T(\tau) Q_\phi (\phi_k(\tau) - \phi_k(0)) \\ + \tau \psi_k^T(\tau) Q_\phi R_\phi^{-1} Q_\phi^T \psi_k(\tau) \geq 0. \end{aligned} \quad (29)$$

On the other hand, from (7), there exists a coupling relation between the components of the vector $\eta_k(\tau)$. Hence, $\forall Y_1 \in \mathbb{R}^{n \times n}$ and $\forall Y_2 \in \mathbb{R}^{n \times n}$ the following equality is satisfied:

$$\begin{aligned} 2(x_k^T(\tau) Y_1^T + \dot{x}_k^T(\tau) Y_2^T) (A x_k(\tau) + B_\phi \phi_k(\tau) \\ - \dot{x}_k(\tau) + B_u (K_x x_k(0) + K_\phi \phi_k(0))) = 0. \end{aligned} \quad (30)$$

This null term can be added to (27). Hence, combining (27), (28), (29) and (30), one obtains that

$$\begin{aligned} \dot{W} \leq \eta_k^T(\tau) [\Pi_1 + (T_k - \tau) \Pi_2 + \tau (M_{135}^T Q_x R_x^{-1} Q_x^T M_{135} \\ + M_{246}^T Q_\phi R_\phi^{-1} Q_\phi^T M_{246}) + (T_k - 2\tau) \Pi_3] \eta_k(\tau). \end{aligned}$$

Thus, to prove that $\dot{W} < 0$, it suffices to guarantee that

¹ The matrices M_i are not of the same dimension. The notations 0 and I correspond to the zero and identity matrices of appropriate dimension.

$$\begin{aligned} & \Pi_1 + (T_k - \tau)\Pi_2 + \tau(M_{135}^T Q_x R_x^{-1} Q_x^T M_{135} \\ & + M_{246}^T Q_\phi R_\phi^{-1} Q_\phi^T M_{246}) + (T_k - 2\tau)\Pi_3 \prec 0. \end{aligned}$$

As this matrix inequality is affine with respect to τ , and $\tau \in [0, T_k]$, a necessary and sufficient condition to satisfy it, is given by

$$\begin{cases} \Pi_1 + T_k(\Pi_2 + \Pi_3) \prec 0 & (31) \\ \Pi_1 - T_k\Pi_3 + T_k(M_{135}^T Q_x R_x^{-1} Q_x^T M_{135} \\ + M_{246}^T Q_\phi R_\phi^{-1} Q_\phi^T M_{246}) \prec 0. & (32) \end{cases}$$

Finally, as (31) and (32) are affine in T_k and $T_k \in [\mathcal{T}_1, \mathcal{T}_2]$, applying the same reasoning and the Schur complement to (32), we conclude that $\Psi_1(\mathcal{T}_i) \prec 0$ and $\Psi_2(\mathcal{T}_i) \prec 0$, $i = 1, 2$, are sufficient to ensure $\dot{W} < 0$. Hence, by virtue of *Theorem 1* the satisfaction of conditions (22)-(25) ensures the global asymptotic convergence of the trajectories to the origin. \square

5. OPTIMIZATION PROBLEMS

From the conditions stated in *Theorem 2*, we can formulate three optimization problems as follows.

P1. Given \mathcal{T}_1 , the sector and slope bounds, find the maximal \mathcal{T}_2 such that global stability of the closed-loop system (7) is ensured.

P2. Given a nominal sampling time \mathcal{T}_{nom} , the sector and slope bounds, find the maximum symmetrical boundaries (Jitter) denoted by σ , *i.e.*, $\mathcal{T}_1 = \mathcal{T}_{nom} - \sigma$, $\mathcal{T}_2 = \mathcal{T}_{nom} + \sigma$, such that global stability of the closed-loop system (7) is ensured.

P3. Given \mathcal{T}_1 and \mathcal{T}_2 , compute the maximum sector and slope bounds, such that the global stability of the closed-loop system (7) is ensured.

Note that, as (22), (23), (24), (25) are LMIs, once \mathcal{T}_1 , \mathcal{T}_2 and the sector bounds are fixed, these optimization problems can be straightforwardly solved by considering feasibility LMI problems and bisection techniques, where we interactively increase/decrease and test \mathcal{T}_2 , σ or a parameter defining the sector.

6. NUMERICAL EXAMPLE

Consider system (1) given by the following matrices

$$\begin{aligned} A &= \begin{bmatrix} -0.5 & -6.2 & -0.105 & -1.2 \\ 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix}, B_u = \begin{bmatrix} 1 \\ 0 \\ 0 \\ 0 \end{bmatrix}, B_\phi = \begin{bmatrix} 0.5 \\ 0 \\ 0 \\ 0 \end{bmatrix} \\ C &= [0 \ 0.2 \ 0 \ 0], \end{aligned}$$

and the control law (4) with the following gains

$$K_x = [0.1 \ 0.2 \ 0.005 \ 0.2], \quad K_\phi = [0.5],$$

with the bounds of ϕ given by $\underline{\delta} = 0$, $\bar{\delta} = \epsilon$, $\underline{\gamma} = -\epsilon$, $\bar{\gamma} = \epsilon$.

In order to show the potential advantage and the conservatism reduction induced by the generic Lurie type function, we consider different structures from the function V defined in (17). More specifically, we evaluate the

feasibility of the inequalities such that they also hold for V_0 (*i.e.* V with $\Lambda = 0$), for a quadratic function of the Circle Criterion $V_Q(x) = x^T P_{11} x$, which corresponds to V with $P_{12} = 0$, $P_{22} = 0$, $\Lambda = 0$ and for the function of the Popov Criterion

$$V_{LP}(x) = x^T P_{11} x + \sum_{i=1}^m \lambda_i \int_0^{y_i} (\phi_i(s) - \delta_i s) ds, \quad (33)$$

which corresponds to V with $P_{12} = 0$, $P_{22} = 0$ and $\lambda_i > 0$, $i = 1, \dots, m$. Note that for V_Q and V_{LP} we consider $P_{11} \succ 0$ and for V_0 we consider $P \succ 0$.

The obtained results for P1 are detailed in Table 1, for values of $\mathcal{T}_1 = 0.1$ ms and $\epsilon = \frac{1}{\sqrt{2}}$. For P2, we fixed $\mathcal{T}_{nom} = 1.5$ s and $\epsilon = \frac{1}{\sqrt{2}}$, which results are presented in Table 2 and for P3 we defined $\mathcal{T}_1 = 0.1$ ms and $\mathcal{T}_2 = 2.0$ s, which results are depicted in Table 3.

Table 1. Maximum value of \mathcal{T}_2 for different Lyapunov function structures.

	V_Q	V_0	V_{LP}	V
\mathcal{T}_2	1.1072	1.1087	2.1969	2.6169

Table 2. Maximum value of σ for different Lyapunov function structures.

	V_Q	V_0	V_{LP}	V
σ	1.0468	1.0475	1.0861	1.2183

Table 3. Maximum value of ϵ for different Lyapunov function structures.

	V_Q	V_0	V_{LP}	V
ϵ	0.5938	0.5938	0.7798	1.0886

In the first problem, using the generalized Lurie function V we achieve values for \mathcal{T}_2 that are greater 19.1%, 136.0% and 136.3% than the ones obtained with V_{LP} , V_0 and V_Q , respectively. For P2, we guaranteed the stability for $\mathcal{T}_1 = 0.2817$ s and $\mathcal{T}_2 = 2.7183$ s, with σ greater 12.1%, 16.3 % and 16.3 % than the ones obtained with V_{LP} , V_0 and V_Q , respectively. For the last feasibility problem, the sector bounds, represented by ϵ were 39.6%, 83.3% and 83.3% bigger than the ones obtained with V_{LP} , V_0 and V_Q , respectively.

To show that the achieved results support the global stabilization of the closed-loop system (7), we simulate the system considering the result from P1, *i.e.*, $T_k \in [0.0001, 2.6169]$, and the nonlinearity

$$\phi(y(t)) = 0.1 \sin(5y(t)) + 0.15y(t), \quad (34)$$

that satisfies (2) with $\underline{\delta} = 0$, $\bar{\delta} = \frac{1}{\sqrt{2}}$, $\underline{\gamma} = -\frac{1}{\sqrt{2}}$, $\bar{\gamma} = \frac{1}{\sqrt{2}}$. The control action and the states of the closed-loop system are presented in Figures 1 and 2. To obtain the values of T_k , we used a pseudo-random algorithm that generates its numbers from the standard uniform distribution on the interval previously defined.

It is easy to notice that when $t \rightarrow \infty$ the states and the control law converge to the origin, reinforcing the obtained results.

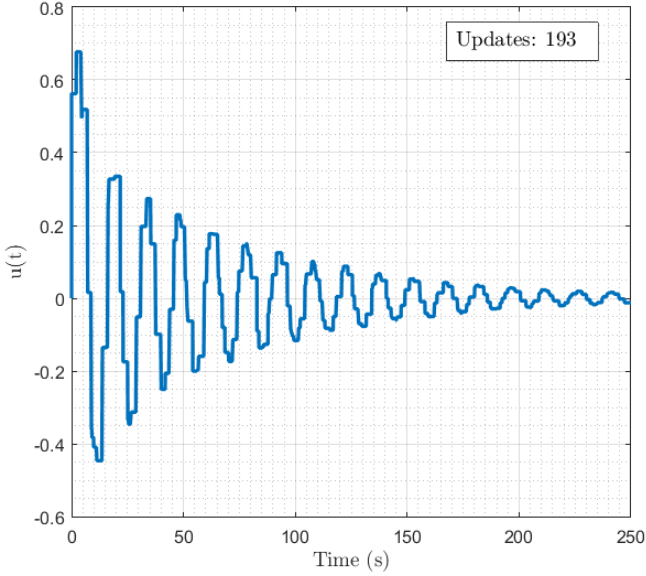


Figure 1. Control action of the closed-loop system with nonlinearity (34).

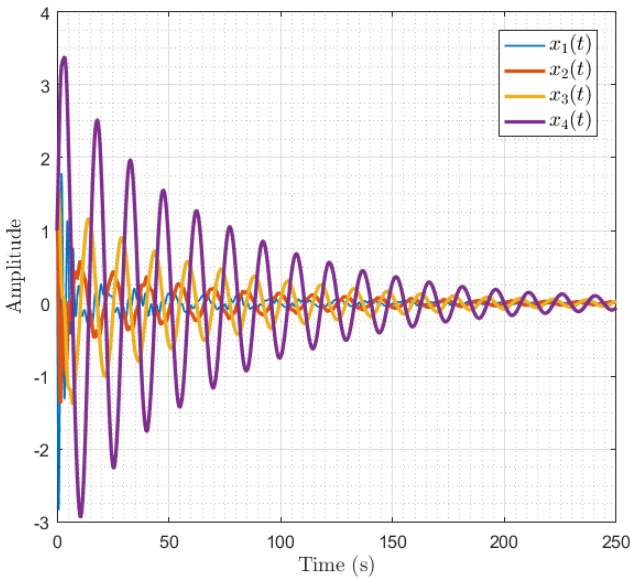


Figure 2. States of the closed-loop system with nonlinearity (34).

7. CONCLUSIONS

This article presents new convex conditions for global asymptotic stability of sampled-data controlled systems, subject to sector and slope-restricted nonlinearities. To develop the methods, we used the looped-functional approach and a generalized Lurie function that does not require the positivity of the matrix P (as in (18)) nor the positivity of the Lurie-Postnikov coefficients.

With the presented conditions, we may solve different types of optimization problems, such as maximizing the maximum sampling time, maximizing the sampling bounds over a nominal sampling time or maximizing the sector bounds for which the GAS of the closed-loop system can be ensured.

We are currently developing local stability conditions for Lurie systems using as basis the content of this paper and later we will develop synthesis conditions for the controller. Future work also includes the study of the problem taking into account communication delays.

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