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# Tridimensional nonhydrostatic transient rip currents in a wave-resolving model

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## Abstract

Flash rips and surfzone eddies are transient horizontal structures of order 10-100 m scale, that can be generated in the surfzone in the absence of bathymetric irregularities. They are traditionally assessed within a depth-averaged framework that involves intrinsic horizontal shear instabilities or/and direct short-crested wave vorticity generation. In this paper, we revisit surf eddy generation processes with a new tridimensional, wave-resolving model (CROCO). We first present a quick overview of a free-surface, compressible approach adapted to nearshore dynamics. Its ability to simulate surface gravity wave propagation and nearshore breaking is validated against laboratory experiments. Next, we present a full 3D, wave-resolving real-case simulation of nearshore currents in Grand Popo Beach, Benin, forced by waves with frequency and directional spreading. The generation of surfzone eddies by the 3D model is shown to differ considerably from that produced by depth-averaged models, owing to the vertical structure of currents produced by shallow breaking that prevents a strong inverse energy cascade. Processes of both horizontal shear instability and short-crested wave breaking are restricted. Instead, the vertical shear flow is prone to forced variability by wave groups and to a Kelvin-Helmholtz-type instability. The latter shows primary and secondary instabilities, that generate spanwise and streamwise vorticity connecting breaking-induced rolls to larger horizontal surfzone structures. Streamwise filaments, appearing as ribs or mini rips, can extend beyond the surfzone but with lower energy than depth-averaged model rips

(offshore mean EKE is reduced by a factor 2). Energy spectra and visual inspections of tracer and sediment concentration shows much better fit between the 3D model patterns and in-situ and aerial observations in Grand Popo Beach. Our results thus suggest that nearshore vortical motions are driven by nonhydrostatic dynamics, at least for moderate wave forcing.

*Keywords:* surfzone, transient rip, 3D instability, nonhydrostatic, wave-resolving model

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## 1. Introduction

Flash rips and surfzone eddies are generally defined as transient horizontal structures of size ranging between water depth and surfzone width, i.e., of order 10-100 m, which are generated in the surfzone in the absence of bathymetric irregularities. They are studied separately from stationary rip currents confined to deeper channels between sandbars (Marchesiello et al., 2015). They are also separated from breaking-induced rollers that scale with wave height (Cox and Anderson, 2001), and even smaller vortices of the fully developed turbulent bore (Svendsen and Madsen, 1984). However, the separation between surf eddies and turbulence is uncertain (Longo et al., 2002) and the possibility of intermediate scales and processes linking horizontal and vertical vorticity generation has been suggested — e.g., Short et al. (1993) describing ephemeral and shallow *mini rips* over Australian low tide terrace beaches — but not clearly demonstrated.

Because it is difficult to sample transient rip currents with sufficient spatial resolution (Henderson et al., 2017), our concepts largely rely on numerical models, mostly depth-averaged models. Three types of processes stand out:

- Horizontal (2DH) shear instability of longshore currents
- Short-crested wave vorticity generation (here called Peregrine process)
- Tridimensional (3D) shear instability

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19 Horizontal shear instability of longshore currents is the earliest process of eddy gener-  
20 ation, accounting for the intrinsic variability of wave-driven currents (Bowen and Holman,  
21 1989; Dodd et al., 1992; Allen et al., 1996; Slinn et al., 1998; Özkan-Haller and Kirby, 1999;  
22 Dodd et al., 2000; Uchiyama et al., 2009). This process was typically studied with wave-  
23 averaged shallow-water models, where momentum transfer from wave to current fields is  
24 entirely parametrized. Its importance has faded during the last decade due to prevalence of  
25 the Peregrine process, but also to conflicting results given by newly developed wave-averaged  
26 tridimensional models (Newberger and Allen, 2007; Splinter and Slinn, 2003).

27 The second process, largely due to Peregrine (1998), is the current nearshore community  
28 views of driving mechanisms for wave-averaged circulation in the surfzone (Kirby and De-  
29 rakhti, 2019). Boussinesq equations for weakly dispersive intermediate and shallow water  
30 waves provides a conceptual model for the action of spatially varying wave breaking, i.e.,  
31 short-crested waves (Johnson and Pattiaratchi, 2006; Bonneton et al., 2010; Feddersen et al.,  
32 2011; Clark et al., 2012; Feddersen, 2014). In this model, small vortices result from gener-  
33 ation by differential breaking, and combine over time into larger eddies through an inverse  
34 cascade mechanism, consistent with 2D turbulence. The surfzone is thus a production center  
35 for eddies with scales roughly ranging from 10 to 100 m. In addition, the coastal boundary  
36 imposes that eddies and associated filaments can only go offshore, providing a mechanism  
37 for enhanced cross-shore dispersion of various tracers.

38 The theoretical framework from depth-integrated models neglect the effect of verti-  
39 cal shear. Following the advent of robust 3D formulations of wave-averaged equations  
40 (McWilliams et al., 2004; Ardhuin et al., 2008), a number of 3D modeling studies have  
41 emerged in the last decade (Newberger and Allen, 2007; Uchiyama et al., 2010; Kumar  
42 et al., 2012; Marchesiello et al., 2015; Uchiyama et al., 2017; McWilliams et al., 2018; Akan  
43 et al., 2020). They show a modulation of nearshore circulation when wave breaking occurs  
44 in a shallow surface layer. However, short-crested wave breaking is generally neglected in  
45 these wave-averaged studies (or addressed in ad-hoc manners) and all real-scale applications  
46 to date are performed using hydrostatic assumption, thus neglecting horizontal vorticity  
47 motions.

48 Nonhydrostatic dynamics are essential in our third listed process of surf eddy generation.  
49 They are mostly studied in laboratory experiment (Nadaoka et al., 1989) and laboratory-  
50 scale Large-Eddy Simulations (LES) using 2.5D CFD models applied to individual wave  
51 breaking (Lin and Liu, 1998; Watanabe and Saeki, 1999; Watanabe et al., 2005; Kirby and  
52 Derakhti, 2019). These previous studies show that the spanwise (mostly alongshore) com-  
53 ponent of vorticity is an important aspect of the breaking process. It is associated with  
54 vertical shear generated by shallow breaking, which can produce traveling rolls through a  
55 primary instability (Watanabe et al., 2005). The rolls, typical of unsteady parallel shear  
56 flows, can subsequently evolve through a secondary instability to yield streamwise vorticity,  
57 transitioning toward fully tridimensional turbulence. However, 2.5D CFD models are ap-  
58 plied to individual breaking waves with only few alongshore wavelengths of the secondary  
59 instability, precluding any evaluation of eddy statistics.

60 3D nonhydrostatic processes are usually studied independently of the two others (by  
61 separate research communities) and rarely compared in terms of scales, magnitude and  
62 interaction. The only attempt was made by Splinter and Slinn (2003) in a proceeding report.  
63 Using a 3D nonhydrostatic model where breaking acceleration is introduced as a body force,  
64 they show that deep breaking reproduces 2D model solutions, while the more realistic shallow  
65 breaking process would hinder horizontal shear instability at the expense of vertical shear  
66 instability. However, their domain size do not allow statistical comparisons and the profile of  
67 breaking acceleration is imposed, not computed from a wave-resolving model. The present  
68 study is a step forward from this early work, also addressing the case of short-crested wave  
69 generation. Note that (Kumar and Feddersen, 2017) studied transient eddies produced by  
70 a 3D nearshore circulation model, forced by short-crested waves computed beforehand with  
71 a Boussinesq model. However, wave forcing is prescribed as a depth-uniform body force,  
72 i.e., deep breaking, and could not produce vertical shear of the cross-shore flow. Their  
73 hydrostatic assumption also precluded the model from vertical shear instabilities.

74 CROCO (Coastal and Regional Ocean Community model) is a new oceanic modeling  
75 system built upon ROMS (Shchepetkin and McWilliams, 2005; Debreu et al., 2012), with  
76 added non-Boussinesq kernel (Auclair et al., 2018). CROCO is designed for solving fine-scale

77 processes from the regional ocean to littoral zone with capabilities for LES in realistic config-  
78 urations. Particular attention is given to numerical accuracy, high-performance computing  
79 (optimization, scalability), portability and easy access ([www.croco-ocean.org](http://www.croco-ocean.org)). This pa-  
80 per presents a quick overview of the nonhydrostatic CROCO solver with a non-Boussinesq  
81 (compressible) approach, before addressing its application to nearshore dynamics. First,  
82 its ability to simulate surface gravity wave propagation and nearshore breaking is validated  
83 against laboratory experiment. Second, we analyse and validate a full 3D, wave-resolving,  
84 real-case simulation of transient rips, in the presence (or not) of short-crested waves and  
85 strong alongshore currents. We discuss fundamental differences in the generation of surf  
86 eddies by 3D wave-resolving models compared with depth-averaged models, with a focus on  
87 the vertical structure of currents produced by shallow breaking and associated turbulence.  
88 We conclude on the limitation of simplified vorticity evolution equations in which only the  
89 vertical part is considered when so much activity lies in horizontal vorticity, governed by 3D  
90 nonhydrostatic equations.

## 91 **2. Model description**

92 Because of limited computational resources, 3D wave-resolving models are still rarely  
93 used in realistic study of surfzone dynamics. LES applications appeared in the 1990s and  
94 are generally restricted to 2.5D laboratory-scale experiments of individual wave breaking.  
95 Early applications used the volume-of-fluid (VOF) method for free-surface tracking (e.g., Lin  
96 and Liu 1998; Watanabe and Saeki 1999; Watanabe et al. 2005; Derakhti and Kirby 2014).  
97 This model type with Cartesian coordinate, where the free surface crosses computational  
98 cells arbitrarily, fails to precisely apply the pressure boundary condition on the free surface,  
99 affecting the model accuracy.

100 More recently, several 3D wave-resolving, free-surface and terrain-following models have  
101 emerged for the nearshore zone, e.g., SWASH (Zijlema et al., 2011) and NHWAVE (Ma  
102 et al., 2012; Derakhti et al., 2016), based on earlier attempts (e.g., Lin and Li 2002). In this  
103 case, explicit free-surface overturning, occurring during breaking, is precluded and must be  
104 parametrized as a turbulent or a shock process. However, these models can be accurate as

105 well as computational efficient in the study of waves and wave-driven mean and transient  
106 circulation.

107 CROCO belongs to this class of models but, unlike other attempts, resolves the full  
108 compressible Navier-Stokes equations (Auclair et al., 2018). A compressible approach pre-  
109 serves the hyperbolic nature of Navier-Stokes equations and does not require a global elliptic  
110 solver with incremental pressure corrections to ensure the incompressible mass balance. As  
111 a result, it avoids splitting errors between pressure and velocity and approximations made  
112 on free-surface conditions (Zijlema et al., 2011), thereby preserving amplitude and disper-  
113 sion properties of nonhydrostatic surface waves. In the same time, the absence of global  
114 computations by an elliptic solver makes parallelization and optimization procedures much  
115 more efficient. The cost of solving acoustic waves is managed with a splitting technique  
116 introduced below.

### 117 *2.1. Free-surface, compressible ocean model equations*

118 The full set of Navier-Stokes equations for a free-surface ocean is explicitly integrated in  
119 the nonhydrostatic, non-Boussinesq (compressible) version of CROCO, built upon the code  
120 structure of the Regional Oceanic Modeling System (ROMS) primitive equations (Shchep-  
121 etkin and McWilliams, 2005). In the compressible approach (Auclair et al., 2018), acoustic  
122 waves are solved explicitly to avoid Boussinesq degeneracy, which inevitably leads to a 3D  
123 Poisson system in nonhydrostatic incompressible methods – detrimental to computational  
124 costs and accuracy of free-surface model implementation.

125 An advantage of a nearshore model built on a general circulation model, originally de-  
126 signed for larger scales ( $\sim 100\text{m}-100\text{km}$ ), is to bridge ocean sciences (and their communities)  
127 and reach otherwise unattainable objectives, such as addressing surf-shelf interactions in  
128 a rotating and stratified framework. It also gives access to capabilities long developed in  
129 oceanic models (high performance computing; high-order numerical schemes; coupling with  
130 biogeochemistry and sediment models). The wave-resolving version of the model can also be  
131 directly compared with wave-averaged equations, also implemented in ROMS and CROCO  
132 (Marchesiello et al., 2015; Uchiyama et al., 2010), which rely more heavily on parametriza-

133 tions.

134 Non-Boussinesq equations include the momentum and continuity equations, the surface  
 135 kinematic relation (for free surface), heat, salt or other tracer  $C$  conservation equations, and  
 136 the equation of state, which reads in Cartesian coordinates:

$$\frac{\partial \rho u}{\partial t} = -\vec{\nabla} \cdot (\rho \vec{v} u) + \rho f v - \rho \tilde{f} w - \frac{\partial P}{\partial x} + \mathcal{F}_u + \mathcal{D}_u + \lambda \frac{\partial \vec{\nabla} \cdot \vec{v}}{\partial x} \quad (1)$$

$$\frac{\partial \rho v}{\partial t} = -\vec{\nabla} \cdot (\rho \vec{v} v) - \rho f u - \frac{\partial P}{\partial y} + \mathcal{F}_v + \mathcal{D}_v + \lambda \frac{\partial \vec{\nabla} \cdot \vec{v}}{\partial y} \quad (2)$$

$$\frac{\partial \rho w}{\partial t} = -\vec{\nabla} \cdot (\rho \vec{v} w) + \rho \tilde{f} u - \frac{\partial P}{\partial z} - \rho g + \mathcal{F}_w + \mathcal{D}_w + \lambda \frac{\partial (\vec{\nabla} \cdot \vec{v})}{\partial z} \quad (3)$$

$$\frac{\partial \rho}{\partial t} = -\vec{\nabla} \cdot (\rho \vec{v}) \quad (4)$$

$$\frac{\partial \eta}{\partial t} = w_f|_{z=\eta} - \vec{v}|_{z=\eta} \cdot \vec{\nabla} \eta \quad (5)$$

$$\frac{\partial \rho C}{\partial t} = -\vec{\nabla} \cdot (\rho \vec{v} C) + \mathcal{F}_C + \mathcal{D}_C \quad (6)$$

137  $(u, v, w)$  are the  $(x, y, z)$  components of vector velocity  $\vec{v}$ ;  $\eta$  is the free surface;  $\phi(x, y, z, t)$   
 138 is dynamic pressure  $\phi = P/\rho_0$ , with  $P$  the total pressure;  $\rho_0 + \rho(x, y, z, t)$  is total *in situ*  
 139 density;  $f(x, y)$  and  $\tilde{f}(x, y)$  are the traditional and non-traditional Coriolis parameters,  
 140 function of latitude;  $g$  is acceleration of gravity;  $\mathcal{D}_u, \mathcal{D}_v, \mathcal{D}_C$  are diffusive terms;  $\mathcal{F}_u, \mathcal{F}_v, \mathcal{F}_C$   
 141 are forcing terms;  $\lambda$  is the second (bulk) viscosity, associated with compressibility (used to  
 142 damp acoustic waves).

## 143 2.2. Time-splitting principle

144 In the above set of equations, a relation between  $\rho$  and  $P$  is required. To that end, and  
 145 as part of a time-splitting approach, density is decomposed into slow and fast components



146 based on a first-order decomposition with respect to total pressure. In the following,  $s$  and  
 147  $f$  subscripts refer to slow and fast-mode components respectively:

$$\rho = \rho_s(T, S, P_s) + \overbrace{\frac{\partial \rho}{\partial P} \Big|_{T,S} \delta P + O(\delta P^2)}^{\rho_f = c_s^{-2} P_f} \quad (7)$$

$$P = \underbrace{P_{atm} + \int_z^\eta (\rho_s - \rho_0) g \, dz'}_{SLOW} + \underbrace{\rho_0 g (\eta - z) + \overbrace{\delta P}^{P_f}}_{FAST} \quad (8)$$

148  $c_s$  is the speed of sound and  $\delta P = P_f$  is the nonhydrostatic pressure.

149 The Navier-Stokes equations are then integrated with two different time steps within  
 150 the time-splitting approach inherited from ROMS. The slow-mode integration is similar to  
 151 ROMS with the addition of the slow part of vertical momentum equation, whereas fast-  
 152 mode integration is 3D and includes the compressible terms of momentum and continuity  
 153 equations. In vector form:

$$\begin{aligned} \frac{\partial \rho \vec{v}}{\partial t} = & \underbrace{-\vec{\nabla} \cdot (\rho \vec{v} \otimes \vec{v}) - 2\rho \vec{\Omega} \times \vec{v} - \vec{\nabla} \left( \int_z^{\eta_f} (\rho_s - \rho_0) g \, dz' \right) + \vec{\mathcal{F}}_{\vec{v}} + \vec{\mathcal{D}}_{\vec{v}}}_{SLOW} \\ & \underbrace{-\rho_0 g \vec{\nabla} \eta_f - \vec{\nabla} P_f + \rho \vec{g} + \lambda \vec{\nabla} (\vec{\nabla} \cdot \vec{v})}_{FAST} \end{aligned} \quad (9)$$

$$\frac{\partial \rho_f}{\partial t} = -\frac{\partial \rho_s}{\partial t} - \vec{\nabla} \cdot (\rho \vec{v}) \quad (10)$$

$$P_f = c_s^2 \rho_f \quad (11)$$

$$\frac{\partial \eta_f}{\partial t} = w_f|_{z=\eta} - \vec{v}_f|_{z=\eta} \cdot \vec{\nabla} \eta_f \quad (12)$$

$$\frac{\partial \rho C_s}{\partial t} = -\vec{\nabla} \cdot (\rho \vec{v} C_s) + \mathcal{F}_C + \mathcal{D}_C \quad (13)$$

$$\rho_s = \rho(T_s, S_s, \eta_f) \quad (14)$$

$$\rho = \rho_s + \rho_f \quad (15)$$

154 The momentum is integrated both in slow and fast modes but the right-hand-side of  
 155 the equation is split in two parts: a slow part, made of slowly varying terms (advection,  
 156 Coriolis force, baroclinic pressure force and viscous dissipation), and a fast part, made of fast-  
 157 varying terms (the surface-induced and compressible pressure force, weight, and dissipation  
 158 associated with bulk-viscosity). This momentum equation is numerically integrated twice,  
 159 once with a large time-step keeping the fast part constant, and once with a smaller time-step  
 160 keeping the slow part constant. This is much more computationally efficient than integrating  
 161 the whole set of equations at the same fast time step. More details can be found in Auclair  
 162 et al. (2018)<sup>1</sup>. Note that acoustic waves can become pseudo-acoustic if their phase speed  
 163  $c_s$  is artificially reduced ( $c_s$  is a model parameter). In this case, high-frequency processes  
 164 associated with bulk compressibility may be unphysical, but an accurate solution for slower  
 165 nonhydrostatic dynamics can be preserved, while relaxing CFL constraints.

### 166 2.3. Discretized equations for nearshore application

167 In this study, motions are produced by an offshore wave-maker in a non-rotating, ho-  
 168 mogeneous fluid. In this case, the Coriolis force, baroclinic pressure force and all surface  
 169 fluxes are null. There is no temperature and salinity stratification so that slow density  $\rho_s$  is  
 170 constant in time and space.

171 CROCO is discretized on a C-grid with finite-difference methods for slow and fast  
 172 modes that are detailed elsewhere (Shchepetkin and McWilliams, 2005; Soufflet et al., 2016).

---

<sup>1</sup>Auclair et al. (2018) presents a first implementation of the compressible approach involving a 3-level time splitting (internal, external and acoustic). CROCO was simplified to only retain a slow and a fast time level, where acoustic waves are solved together with the external (depth-averaged) mode. This procedure is more computationally efficient

173 In short, the slow-mode time-stepping algorithm is a Leapfrog Adams-Moulton predictor-  
 174 corrector scheme, that is third-order accurate for the integration of advective terms. The  
 175 fast mode is integrated with a generalized forward-backward scheme, which is also third-  
 176 order accurate. Vertical flux terms that do not require accuracy (vertical diffusion term in  
 177 the slow mode and all acoustic terms of  $w$  equation in the fast mode) are computed with an  
 178 implicit time stepping to increase computational stability.

179 Horizontal and vertical advection terms are discretized using the WENO5-Z improved  
 180 version of the 5th-order weighted essentially non-oscillatory scheme (Borges et al., 2008),  
 181 which is popular for hyperbolic problems containing both shocks and smooth structures.  
 182 WENO5-Z naturally takes care of dispersive numerical modes as well as shocks caused by  
 183 breaking waves. Additionally, a 3D Smagorinsky model is used for turbulent closure on  
 184 anisotropic grids:

$$\nu_t = (C_S \Delta)^2 |S| \quad (16)$$

185 where  $S$  is the 3D strain rate,  $\Delta$  the grid-characteristic length scale ( $\sqrt{d_x d_y}$  for horizontal  
 186 viscosity and  $d_z$  for vertical viscosity), and  $C_S$  the Smagorinsky coefficient. The standard  
 187 value of  $C_S = 0.1$  (Canuto and Cheng, 1997) is used and sensitivity to this value is discussed  
 188 along the paper.

#### 189 2.4. Wave maker at offshore boundary

190 The wave maker forces a spectrum of 3D linear waves at the offshore boundary, as in  
 191 Zijlema et al. (2011), rather than as an interior source term (Wei et al., 1999). The spectrum  
 192 has frequency and directional spreading similar to Feddersen et al. (2011):

$$\eta_{bc}(y, t) = \sum_i a_i \sum_j d_j \cos(k_{y,ij} y - \omega_i t - \phi_{ij}) \quad (17)$$

193

$$\text{with } d_j = \exp\left(-\frac{\theta_j - \theta_m}{\sigma_\theta^2}\right) \text{ and } \sum d_j = 1 \quad (18)$$

194

$$u_{bc}(y, t) = \eta_{bc}(y, t) \omega_p \cos(\theta_m) \frac{\cosh(k_p(z+h))}{\sinh(k_p h)} \quad (19)$$

195

$$v_{bc}(y, t) = \eta_{bc}(y, t) \omega_p \sin(\theta_m) \frac{\cosh(k_p(z + h))}{\sinh(k_p h)} \quad (20)$$

196 where  $(i, j)$  are indices of spectral distribution in frequency and direction respectively;  $a_i$  is  
 197 the amplitude at each frequency  $\omega_i$ ;  $k_{y,ij} = k_i \sin(\theta_j)$  is the alongshore wavenumber, where  
 198  $k_i$  is the linear theory wavenumber:  $\omega_i^2 = g k_i \tanh(k_i h)$ , and  $\theta_j$  is wave angle;  $\theta_m$  is the  
 199 mean wave direction and  $\sigma_\theta$  the directional spread around the mean;  $\omega_p$  and  $k_p$  are peak  
 200 frequency and wavenumber;  $d_j$  is a normalized frequency-dependent directional distribution;  
 201  $\phi_{ij}$  is a uniformly distributed random phase.

202 Here  $w_{bc}$  is set to zero and our tests show only weak sensitivity to this choice. Depth-  
 203 averaged (barotropic) velocities  $(\bar{u}, \bar{v})$  must be provided as well in the wave maker because  
 204 they are prognostic variables of our split-explicit model, advanced together with the fast  
 205 acoustic mode. For normal depth-averaged velocity  $\bar{u}$ , we do not impose the depth-averaged  
 206 value of  $u_{bc}$  directly but the value of the incoming characteristic of the shallow water system  
 207 as in Flather-type conditions (Marchesiello et al., 2001; Blayo and Debreu, 2005):

$$\bar{u} = \bar{u}_{bc} - \sqrt{\frac{g}{h}} (\eta - \eta_{bc}) \quad (21)$$

208 This allows infragravity waves generated inside the domain to propagate out as long waves,  
 209 while ensuring a near conservation of mass and energy through the open boundary.

### 210 **3. Validation in Flume experiment**

#### 211 *3.1. GLOBEX experiment*

212 As a first step towards 3D modeling, we present here a validation of wave propagation  
 213 and breaking using a wave flume experiment. The Gently sLOping Beach EXperiments  
 214 (GLOBEX) were performed in the Scheldt flume of Deltares (Delft, the Netherlands) in  
 215 2012, and described in Michallet et al. (2014). The project objective was to collect high-  
 216 resolution space-time data of the cross-shore evolution of short and infragravity waves on a  
 217 gentle slope for a range of wave conditions.

218 The flume is 110 m long, 1 m wide and 1.2 m high. The waves were generated with a  
219 piston-type wave maker equipped with Active Reflection Compensation to minimize reflec-  
220 tions from the wave paddle. A concrete beach with a 1:80 slope was constructed, with its  
221 toe at 16.57 m from the wave maker. All experiments were run with a still water depth of  
222 0.85 m and still-water shoreline at  $x = 84.57$  m. The material that was laying loose on the  
223 concrete bed before the flume was filled with water had a median grain size  $D_{50}=0.75$  mm  
224 (roughness length  $z_0 \sim D_{50}/12 = 0.0625$  mm).

225 Sea-surface elevation measurements were taken at 190 locations (repeating a experiment  
226 ten times while relocating the 21 wave gauges), together with velocity measurements at  
227 43 locations, mostly (but not always) at 1 cm above bed to focus on the undertow. The  
228 sampling frequency of the instruments during these experiments is 128 Hz. We will com-  
229 pare experiment B3 corresponding to second-order (Stokes) wave generation of bichromatic  
230 frequencies. The characteristics are as follows:  $a_1 = 0.09$  m;  $a_2 = 0.01$  m;  $f_1 = 0.420$   
231 Hz;  $f_2 = 0.462$  Hz (short-wave peak period  $T_p = 2/(f_1 + f_2) = 2.27$  s; and group period  
232  $T_g = 1/(f_2 - f_1) = 23.81$  s). The signal had a total duration of 75 minutes.

### 233 3.2. Model comparison

234 The model is set-up with the same conditions as the wave flume experiment. Second-  
235 order bichromatic waves are generated at the offshore boundary, with shore normal direction  
236 and zero directional spread.

237 Figure 1 compares an Hovmuller plot (x,time) of data and model sea level  $\eta$  and undertow  
238  $u_b$ . When data is missing in the measurements, it is also removed from the model output.  
239 The general structure reflecting wave speed and frequencies, wave packets, surf and swash  
240 zones are all very similar. Some scattering in the data is particularly noticeable in the mean  
241 undertown. As explained by Michallet et al. (2014), it may be attributed to the presence of  
242 secondary motions generated by transverse waves at the break point where the transverse  
243 mode-1 seiche can be excited at frequency  $f_1 + f_2$ .

244 A snapshot of wave field across the flume during runup condition is presented in Figure  
245 2. It highlights the main processes of propagation, nonlinear interaction, shoaling, breaking,

246 roller propagation and runup. Non-linearity is apparent in both model and data in the  
247 increasingly non-sinusoidal shape of short waves as they approach the shore (Elgar and  
248 Guza, 1985).

249 Wave statistics are shown in Figure 3: standard deviation (or  $H_s$ ), mean, skewness and  
250 kurtosis. The envelop of all statistics are well reproduced by the model. Details of skewness  
251 and kurtosis may differ due to irregular current measurement depth and transverse modes  
252 in surfzone measurement. Despite scattering in the mean offshore-directed undertown data,  
253 the model appears to reproduce the cross-shore undertow profile. In doing so, it obviously  
254 outperforms depth-averaged Boussinesq models (Michallet et al., 2014). The undertow is  
255 part of a vertical recirculation associated with breaking-induced surface onshore flow. Here,  
256 we call undertow the bottom return flow (10 cm/s in this experiment). There is also an  
257 Eulerian compensation flow for the onshore surface Stokes drift (continuity of total flow  
258 must be preserved), which is sometimes referred to as undertow. This compensation flow is  
259 the only cross-shore flow captured by depth-averaged models and is relatively weak (on the  
260 order of 1 cm/s in this simulation).

261 From sensitivity tests, it appears that a realistic reproduction of  $H_s$  cross-shore evolution  
262 in the breaker zone ( $x = 60 - 70$  m) is conditioned to using the shock capturing scheme  
263 WENO5-Z. Using only Smagorinsky (or alternatively a  $k - \epsilon$  model) would fail. This is in  
264 line with the representation of wave breaking as bores or hydraulic jumps that should be  
265 treated as a shock problem. On the other end, the WENO scheme is less efficient in the  
266 roller zone ( $x > 70$  m), where turbulent dissipation dominates over production (van der A  
267 et al., 2017). There, the turbulent closure scheme takes over as main dissipation process (but  
268 a Smagorinsky coefficient over 0.1 leads to overestimated dissipation in the breaker zone).  
269 Therefore, our combination of numerical and physical closure with off-the-box parameters  
270 provides a realistic framework for surfzone dynamics. The fact that no tuning was needed for  
271 these schemes indicates that the model can be confidently applied to other configurations.

## 272 4. Real-scale beach experiment

273 We now turn to a full 3D experiment with longshore-uniform bathymetry. The configu-  
274 ration is derived from Grand Popo Beach (6.2°N, 1.7°E, Benin, in the Gulf of Guinea; Fig.  
275 4). This stretch of coast presents a longshore-uniform, low tide terrace and steep upper  
276 shoreface (Almar et al., 2014, 2016) and a sandy wave-dominated and microtidal environ-  
277 ment, exposed to S-SW long period swells generated at high latitudes in the South Atlantic  
278 (Almar et al., 2015a). A field experiment was conducted at Grand Popo Beach from 10  
279 to 18 March 2014 (Almar et al., 2014; Derian and Almar, 2017). For our setup, we focus  
280 on conditions in the middle of the afternoon of March 13 2014. The weather, tides and  
281 wave conditions were ideal: weak winds and wind waves well separated from a narrow-band  
282 swell with significant wave height  $H_s = 1.15$  m, peak period  $Tp = 11$  s, and wave incidence  
283  $D = 10^\circ$  from shore normal direction. The water was at mid neap tide level (low-tide ter-  
284 race at about 1 m depth), promoting a narrow surfzone less than 50 m wide. A Nortek  
285 high-frequency acoustic Doppler velocimeter (ADV) was deployed in the surfzone and a dye  
286 release was conducted to monitor the dispersion induced by flash rips. This was coupled with  
287 UAV flights (STB DS6 hexacopter) at an elevation of 100 m. The Drone camera (NIKON  
288 D700) was looking down, with a vertical angle, and recorded  $4256 \times 2832$ -px scenes at 1 Hz  
289 (Almar et al., 2014; Derian and Almar, 2017).

### 290 4.1. Setup

291 The domain is 542 m alongshore by 240 m across-shore, with periodic alongshore bound-  
292 ary conditions. In order to prevent distortion when oblique waves are used with periodic  
293 conditions, the alongshore size is adjusted according to peak wavelength and mean wave  
294 direction. This method proved to perform well even with long-crested waves. The grid  
295 spacing is generally  $dx = dy = 1$  m but one simulation is run with higher resolution of 0.5  
296 m. There are 10 vertical levels regularly spaced between the free surface and bottom (a  
297 simulation with 20 levels did not change the results much). The model time step is  $dt =$   
298 0.025 s (0.0125 s at 0.5 m resolution). The model bathymetry is longshore-uniform and built  
299 with continuous functions to smoothly fit the low-tide terrace structure observed during the

300 survey of (Almar et al., 2014, 2018). Depth  $H$  is 8 m offshore to 1 cm at the shoreline, whose  
301 position varies with swash oscillation, relying on a wetting-drying scheme (Warner et al.,  
302 2013). Depth over the terrace is about 1 m according the afternoon mid-tide conditions of  
303 March 13 2014.

304 The wave maker is set with following parameters:  $H_s=1.15$  m,  $Tp=11$  s,  $D = 0^\circ$ ,  $10^\circ$   
305 or  $20^\circ$  ( $D = 10^\circ$  for comparison with data in Sec 4.3), and directional spread  $\sigma_\theta = 30^\circ$ . A  
306 JONSWAP spectrum is constructed with these parameters and a peak enhancement factor  
307  $\gamma$  of 3.3. The quasi-monotonic and shock-capturing WENO5-Z scheme is used again with  
308 Smagorinsky turbulence closure and  $C_S = 0.1$ . Bottom roughness is  $z_0 = 0.01$  mm, which  
309 may seem low but gives a drag coefficient  $C_D \sim 0.002$  in the surfzone ( $C_D = \kappa^2/\ln(z_1/z_0)^2$ ,  
310 with  $\kappa = 0.41$  and  $z_1 \sim H/10$  the first level height above bed), which is a usual value in  
311 depth-averaged models (Chen et al., 2003; Feddersen et al., 2011). We follow the practice  
312 of these models here to reproduce their results within the pseudo-2D approach described  
313 below. It is of little consequence for 3D simulations because, as will be shown, they are  
314 much less sensitive to bottom drag than 2D models (Sec. 5).

315 The model is run for an hour starting from rest and adjusting through a rapid spin-up  
316 phase. Figure 5 shows a snapshot of sea level that shows realistic features: short-crested  
317 waves generated at an angle refract and break, generating rollers, swash and some reflection.

318 CROCO comes with capabilities for water quality, marine ecosystem and sediment mod-  
319 eling. In the present study, some of these capabilities are used with simple setup. First, we  
320 introduce a passive tracer in the swash zone for comparison with dye releases made during  
321 the beach survey. Second, a suspended sediment model (Blaas et al., 2007; Warner et al.,  
322 2008) allows comparison of patterns with aerial photos taken during the survey and also  
323 between simulations. We use a single fine sand class with settling velocity of 1 cm/s. For  
324 resuspension, we consider only one layer of sediment for simplicity, then only two parameters  
325 are needed: critical shear stress and erosion rate at the seafloor, expressed in the erosion



326 flux (Blaas et al., 2007):

$$E = E_0(1 - p) \left( \frac{\tau_b}{\tau_{cr}} - 1 \right) \quad \text{for } \tau_b > \tau_{cr}$$
$$E = 0 \quad \text{otherwise}$$

327  $\tau_b$  is the bottom shear stress computed by the model.  $E_0$  is an empirical erosion rate set  
328 to  $10^{-5}$  kg/m<sup>2</sup>/s;  $p$  is the sediment porosity (0.41);  $\tau_{cr}$  is the critical shear stress, i.e., the  
329 threshold for initiation of sediment motion, set to 0.01 N/m<sup>2</sup>.

#### 330 4.2. Shallow vs. deep breaking (and a Boussinesq model)

331 The Peregrine vorticity generation process only requires short crested waves, with no  
332 need for unstable longshore currents generated by oblique waves. Boussinesq models are very  
333 efficient in this process, but an important question for us is whether a 3D model will remain  
334 so. An essential difference between the two types of model is depth penetration of wave  
335 breaking. In a 2D Boussinesq model, deep breaking is implicitly assumed as momentum is  
336 transferred instantaneously to the depth-averaged flow. However, this is a crude assumption  
337 as breaking-induced flow and turbulence is produced above trough level where the onshore  
338 flow is located (Grasso et al., 2012; Derakhti et al., 2016; van der A et al., 2017). Splinter  
339 and Slinn (2003) suggest that the deep breaking assumption of depth-averaged models is an  
340 essential component of their dynamics. The results presented here are in agreement with  
341 their study and we propose to assess the role of 3D dynamics on surf eddies by comparing  
342 simulations forced by shallow and deep breaking. Deep breaking will constitute a pseudo-2D  
343 model whose results can be compared with a Boussinesq model solution (Section 4.5).

344 Boussinesq-type models (see Barthelemy 2004, for a review) are common tools to simulate  
345 weakly dispersive waves and their transformations from the ocean to the swash zone. Several  
346 developments allowed their application to a wide range of scales, from surfzone processes to  
347 ocean basin-scale tsunami propagation (Kirby, 2016). Here, for a verification of our pseudo-  
348 2D CROCO version, we use FUNWAVE-TVD (Shi et al., 2012). It solves the fully nonlinear  
349 Boussinesq equations using a hybrid finite-volume finite-difference scheme. Parametrizations  
350 are similar to CROCO, with wave breaking handled by a shock capturing TVD scheme

351 (making the need of explicit criterion unnecessary) and a quadratic drag formulation with  
352  $Cd = 0.002$  for bottom friction.

353 To force deep breaking in a 3D wave-resolving model, we can artificially increase the  
354 vertical turbulent viscosity around the breaker zone. Figure 6 shows a time and longshore  
355 average of cross-shore and alongshore currents in the case of shallow and deep breaking.  
356 Shallow breaking is computed by the 3D model with no explicit constrain on penetration  
357 scale (but a parametrization of turbulence induced by breakers and currents). It drives a  
358 shallow onshore flow about 40 cm deep and an offshore near-bottom undertow, resulting  
359 in strong vertical shear of about 2 m/s within 1 m depth. With artificially strong vertical  
360 viscosity, momentum in the breaker zone is almost instantly mixed to the bottom and the  
361 cross-shore flow is reduced to nearly zero as required by mass-conservation (the residual  
362 flow is the Stokes drift compensation flow), and consistent with depth-averaged models.  
363 The longshore flow driven by oblique waves and a number of other simulations with shallow  
364 and deep breaking (Tab. 2) will be analyzed and compared in the following sections.

#### 365 *4.3. Reference simulations and comparison with data*

366 To introduce the 3D processes of flash rip generation, we present simulations with shal-  
367 low and deep breaking (3D\_SC\_D10 and 2D\_SC\_D10), representing mid-tides conditions on  
368 March 13 2014 in Grand Popo Beach. Figure 7 compares the vertical vorticity of surface  
369 flow:  $\omega_z = \frac{\partial v_s}{\partial x} - \frac{\partial u_s}{\partial y}$ , averaged over two peak periods (22 s). With deep breaking (left  
370 panel), the vortical field is rich with large filaments and surf eddies of 50-100 m scale that  
371 are generated from short-crested waves, similar to Boussinesq model solutions. However,  
372 the full 3D model with shallow breaking offers a radically new solution (Fig. 7, right panel).  
373 Some of the large-scale fluctuations are present but over-shadowed by shorter scales. This  
374 mode presents itself as rib structures (or mini rips following a relevant observation by Short  
375 et al. 1993, already mentioned) with short longshore wavelength of order 5-10 m and periods  
376 less than 5 min.

377 We now compare the two simulations with data collected during the survey of March  
378 2014. Flash rips did not strike the survey team as particularly imposing (Castelle et al.,

379 2014; Scott et al., 2018; Floc’h et al., 2018). Dye experiments revealed filament generation,  
380 but of relatively short scales. The survey was not extensive in terms of spatial resolution but  
381 ADV and dye observations suggested a dynamical regime much closer to 3D shallow-breaking  
382 than pseudo-2D deep-breaking simulations, as will be seen.

383 The dye experiment presented in Figure 8 illustrates both the structure of the alongshore  
384 flow and scales of flash rips emerging from the surfzone. Using sequential photos of the tracer  
385 from the Drone camera, it is possible to extract a simplified cross-shore profile of longshore  
386 drift velocities (see Derian and Almar 2017 for more extensive Lagrangian calculations).  
387 The result is presented in Figure 9 together with the model solutions with deep and shallow  
388 breaking. The estimated longshore flow has an asymmetric V-shape very similar to the  
389 full 3D model solution with a peak velocity of about 0.6 m/s in the inner surfzone. Deep  
390 breaking solutions have a more symmetric profile centered in the outer surfzone. The profiles  
391 in both simulations are a result of cross-shore advection. With deep breaking, advection is  
392 weak and the longshore flow remains centered in the breaker zone (Fig. 6).

393 Some information on flash rips can also be extracted from the dye experiment. Figure 8  
394 presents two consecutive aerial photos (at 154 s interval), and the corresponding snapshots  
395 of tracer simulations with the full 3D model. We do not expect an exact match, considering  
396 the chaotic nature of these phenomena, but scales and structures are meaningful. During  
397 the survey, a few attempts of dye release were made before obtaining a clear filament patch.  
398 Similarly for the model, we selected one occurrence among few tracer patches initialized  
399 at regular interval along the coast (in the swash zone). Even though all tracer patches  
400 eventually ended up with similar V-shape and similar scales of evolution, there was variability  
401 in the evolution and we selected the most visually comparable filament with Drone photos.  
402 In both cases, a thin filament of 5-10 m expands quickly seaward at a speed of 0.5-1 m/s,  
403 reaching about 70 m from shore.

404 Another qualitative comparison of patterns can be made, looking at surfzone suspended  
405 sediments in the aerial photo (Fig. 10, left panel). The contrasts in the photo is enhanced  
406 to better expose suspended sediments (brown color), which is seen weakly extending beyond  
407 the surfzone. Snapshots of the model’s surface sediment concentration is also shown after

408 15 min of simulation. With shallow breaking (center panel), sediments tend to resuspend  
409 in the breaker zone and mix efficiently within the surf zone, but only weakly extend to the  
410 innershelf. The rib structure is apparent at the seaward front of sediment concentration.  
411 Overall, the patterns are very similar to the observed suspended sediments, particularly  
412 evident in the upper part of the photo while the rest is partly masked by white foam or  
413 sunglint. The same suspended sediment simulation with deep breaking gives very different  
414 results (Fig. 10, right panel). Resuspension is now maximum in the inner surfzone (as for  
415 eddy energy; Sec. 4.5). Filaments and eddies are more coherent, larger, their growth slower,  
416 but they extend much further seaward. Mixing in the surfzone is less efficient than for the  
417 shallow-breaking case, but shelf-surf exchange is more intense, due to filament extension.  
418 This pattern may have better aesthetic values but does not fit visual observations of Grand  
419 Popo Beach.

420 For a more quantitative scale comparison, we used ADV measurements, looking at hor-  
421 izontal  $u_h = \sqrt{u^2 + v^2}$  and vertical  $w$  velocities, the latter being a good indicator of 3D  
422 motions. Figure 11 presents the Power Spectral Density (PSD) of  $u_h$  and  $w$  velocity fluctu-  
423 ations for the model and the ADV data at a similar location in middle of the terrace. The  
424 model short-wave spectrum around 11 s resulting from the wave maker is well represented  
425 considering that the forced wave spectrum is constructed from JONSWAP approximation.  
426 At lower frequency in both  $u_h$  and  $w$  PSD, a surprisingly good fit with data is given by the  
427 full 3D model, while the deep-breaking simulation has a clear energy deficit. Looking at  $u$   
428 PSD, there is a band of high energy around 30-100s period that is clearly missing in the  
429 pseudo-2D case. This frequency is consistent with visual inspection of rip structure oscilla-  
430 tion in animated vorticity fields. However, the difference between 3D and pseudo-2D cases  
431 can be seen at even lower frequency. This is best illustrated by  $w$  PSD and will be shown  
432 to result from nonlinear upscaling (Sec. 4.6). Interestingly, the energy range of 3D eddies  
433 encroaches on that of infragravity waves, making it hard to separate the two dynamics from  
434 observations alone.

435 At an offshore position, where unfortunately no data is available, the comparison be-  
436 tween model simulations shows a different relation at very low frequency, for time scales

437 between 3 and 15 min (Fig. 12). In this range, eddies produced by short-crested waves  
 438 have more energy in the deep-breaking case, as expected from visual inspection of vorticity  
 439 and suspended sediments. We conclude from this section that observations in Grand Popo  
 440 Beach are in much better agreement with a full 3D solution of surf eddies, which presents  
 441 a radically different dynamical regime. We will now analyze more closely the 3D structure  
 442 and generation process of rib structures.

#### 443 4.4. Structure and production of vertical shear instability

444 The surfzone eddy variability seen in the 3D model solution is truly three-dimensional.  
 445 Vertical vorticity is only one manifestation, but horizontal vorticity is the key player. For  
 446 better detection, we use a higher-resolution simulation (run for 15 minutes) that gives a  
 447 very similar solution to the lower resolution case. Figure 13 presents the  $Q$  field defined  
 448 by  $Q = -\frac{1}{2} \frac{\partial u_i}{\partial x_j} \frac{\partial u_j}{\partial x_i}$ , using Einstein summation convention over the three dimensions.  $Q$   
 449 is commonly used to enhance detection of vortical flows. Here, we split cross-shore and  
 450 alongshore  $Q$  components ( $Q_y = -\frac{\partial u}{\partial z} \frac{\partial w}{\partial x} - \frac{1}{2} \frac{\partial u^2}{\partial x}$  in red and  $Q_x = -\frac{\partial v}{\partial z} \frac{\partial w}{\partial y} - \frac{1}{2} \frac{\partial v^2}{\partial y}$  in green),  
 451 then normalize them and only plot positive isosurface values 0.02 for clarity (negative values  
 452 give counter-rotating features).

453 The result is strikingly consistent with instabilities of a transitional mixing layer (Met-  
 454 calfe et al., 1987; Lesieur, 1990), the transition being constrained by surfzone width.  $Q_y$   
 455 shows spanwise "rolls" created from the primary instability while  $Q_x$  identify streamwise  
 456 "ribs" that are transverse (counter-rotating) vortices from secondary instability (assumably  
 457 growing from perturbations generated between the rolls, in the braid region). Note that  
 458 streamwise designate the shear direction, which is cross-shore rather than (oblique) wave  
 459 direction. The reason is that the undertow aligns with surface flow in the alongshore di-  
 460 rection, forming only weak mean longshore vertical shear. (Fig. 6). However, the ribs can  
 461 take an oblique direction as they are advected by the mean longshore flow. They extend  
 462 seaward beyond the surfzone while stretching in the vertical direction. Filaments of verti-  
 463 cal vorticity (or  $Q_z$ , not shown) also have similar rib structures to  $Q_x$ , recognisable in the  
 464 surface vorticity plot of Figure 7.

465 The mean shear flow is composed of breaking-induced mean onshore flow and associated  
 466 seaward undertow (Fig. 6). The inflected velocity profile is inviscidly unstable to small per-  
 467 turbations and unstable modes of Kelvin-Helmholtz type can emerge. The spanwise rolls are  
 468 large vertical eddies that rapidly evolve into transverse (streamwise) rib vortices connected  
 469 by “braid” regions, and stretched seaward and downward. This picture is reminiscent of  
 470 descriptions based on laboratory-scale measurements and simulations (Nadaoka et al., 1989;  
 471 Watanabe et al., 2005; Kirby and Derakhti, 2019) — although here no air mixing by bubbles  
 472 is required for the secondary instability to occur.

473 According to linear stability analyses, the wavelength of primary shear instability setting  
 474 the distance between spanwise rolls is an order of magnitude larger than the mixing layer  
 475 width  $\delta$  — in free shear layers (Michalke, 1964, 1965), wavelength, frequency and growth  
 476 rate of the most unstable modes are  $14 \delta$ ,  $0.015 U/\delta$  and  $0.1 U/\delta$  respectively). The sec-  
 477 ondary instability wavelength is of the same order as that of the primary instability ( $2/3$   
 478 in Pierrehumbert and Widnall 1982). If the mixing layer width is taken as the vorticity  
 479 thickness  $\delta = \Delta U / [\frac{\partial u}{\partial z}]_{max} \sim 60$  cm, then the wavelength of both roll and rib structures is  
 480 5-10 m, consistent with our simulation. Note that given an effective resolution of 5-10  $dx$  for  
 481 CROCO (Soufflet et al., 2016), a simulation with 1-m grid resolution can only be considered  
 482 “eddy-permitting” for 3D instability in the present conditions. In terms of temporal modes,  
 483 the mixing layer size should produce modes of 0.01-0.04 Hz (25-100 s period), a range usually  
 484 reserved to surf beat. The model with 3D instability has energy in this range that is lacking  
 485 in the deep breaking case (see previous section and Fig. 11), but it has excess energy at  
 486 lower frequency as well, which results from upscaling through nonlinear interactions (the  
 487 same spectrum is produced with monochromatic wave forcing; see also Sec. 4.6).

488 In order to isolate the mechanism of eddy-mean flow interaction, we analyze a solution  
 489 forced with monochromatic, shore-normal, long-crested waves (3D\_MONO\_D0 in Tab. 2).  
 490 This simulation has constant wave forcing in both space and time when averaging over  
 491 the wave period (11 s). In this case, the same rib structure is generated (Fig. 14) but  
 492 without the large-scale alongshore variation seen in the full solution (Fig. 7, right panel).  
 493 A comparison of this simulation with other test cases will be presented in the next section.

494 Here, we analyse the mechanism and patterns of shear production. Figure 15 shows EKE  
 495 source terms  $-\overline{u'_i u'_j \frac{\partial \bar{u}_i}{\partial x_j}}$ , that results from eddy-mean flow interaction, i.e., the energy spent  
 496 by the mean flow to feed rolls and ribs. The largest term is vertical shear production  
 497  $-\overline{u' w' \frac{\partial \bar{u}}{\partial z}}$  (Metcalf et al., 1987), with some lesser contribution from cross-shore convergence  
 498  $-\overline{u' u' \frac{\partial \bar{u}}{\partial x}}$  (all other 7 combinations are negligible). The main production site is in the breaker  
 499 zone. A maximum value is located just beneath the inflection point in the mean velocity  
 500 profile (maximum shear represented in Fig. 15 by a thick blue line), consistent with mixing  
 501 layer instability. The figure also presents a cross-section of mean 3D eddy kinetic energy  
 502 ( $EKE = \frac{1}{2}(u'^2 + v'^2 + w'^2)$ , where  $u', v', w'$  are fluctuation velocities to the time-mean  
 503 flow presented in Fig. 6). EKE and shear production have a very similar spatial pattern,  
 504 although high EKE values extend from the production center in all directions: surface,  
 505 bottom, shoreward and seaward. The primary rolls are thus produced in the outer surfzone  
 506 and advected by the mean and eddy flow towards both the inner surfzone and innershelf.  
 507 EKE transport is stronger at the surface, so that the streamwise filaments extend farther  
 508 offshore at the surface than at the bottom (despite some amount of vertical stretching as  
 509 they leave the terrace).

#### 510 4.5. Short-crested waves and the Peregrine process

511 An important question of our study concerns the effect of wave variations (frequency and  
 512 directional spreading) on flash rip generation in a full 3D model. To address this question, it  
 513 is useful to simplify the problem and progressively add the multiple conditions of variability.  
 514 In this section, we analyse shore-normal, short-crested wave simulations with shallow or deep  
 515 breaking (3D\_SC\_D0 or 2D\_SC\_D0). Shore-normal conditions prevents the formation of a  
 516 longshore current and associated horizontal shear instability. In addition, we look at long-  
 517 crested wave solutions to isolate the effect of 3D instabilities, i.e., the monochromatic solution  
 518 (3D\_MONO\_D0; presented in the previous section) and a similar case with JONSWAP  
 519 frequency spectrum (3D\_LC\_D0). This latter comparison will help evaluate the effect of  
 520 frequency spreading on eddy variability before addressing the effect of directional spreading.

521 Figure 16 compares vertical vorticity for shore-normal, short-crested wave cases. As for

522 oblique waves, deep-breaking leads to a rich vortical field with large filaments extending  
523 far offshore, similarly to Boussinesq models. This is confirmed here with a comparison  
524 between FUNWAVE-TVD and pseudo-2D CROCO applied to the same configuration. A  
525 difference between Boussinesq and pseudo-2D solutions is the effect of 3D dynamics over the  
526 innershelf in the latter case, where surface-intensified offshore eddies and filaments present a  
527 more fragmented aspect due to forward energy cascade (Uchiyama et al., 2017; McWilliams  
528 et al., 2018). However, the full 3D nonhydrostatic model with shallow breaking (Fig. 16,  
529 right panel) shows patterns radically different from both Boussinesq and pseudo-2D solutions  
530 with regular shorter-scale rib structures that present a more limited cross-shore extension.

531 Figure 17 presents EKE cross-sections for all shore-normal wave experiments. A striking  
532 element of these figures is the presence of large surface and bottom EKE in the shallow  
533 breaking cases. This pattern is not a result of shear production and is absent from the  
534 monochromatic case (see previous section and Fig. 15). Therefore, it can only result from  
535 wave groups associated with frequency spreading. Through wave height modulation, wave  
536 groups produce variability in the breaking-induced surface onshore flow and associated un-  
537 dertow. The variability amounts to about half of integrated mean EKE. However, it is much  
538 reduced in the deep-breaking case, consistent with depth-averaged model studies (de Schip-  
539 per et al., 2014).

540 We now turn to the effect of directional spreading. In Figure 17, short-crested waves  
541 (produced by directional spreading) extend EKE production over a wider surf zone than long-  
542 crested waves, where EKE is confined to the breaker zone. However, the seaward extension  
543 is much larger in the pseudo-2D model, confirming the impression made from vorticity  
544 inspection. Further confirmation is given by vertical EKE integration (and normalization  
545 by mean depth; Fig. 18). It highlights 3 regions of eddy energy: the inner and outer  
546 surfzone and innershelf. The top panel presents unfiltered data. In this case, 3D instability  
547 and wave group forcing dominates eddy production in the outer surfzone. The most striking  
548 observation is that the deep-breaking solution has a much larger cross-shore expansion,  
549 stretching shoreward with a maximum in the inner surfzone and also 100 m seaward over  
550 the innershelf.



551 Short-crested waves do not seem to affect 3D instability, while, on the contrary, shallow-  
552 breaking largely affects eddy production associated with the Peregrine process. This is  
553 particularly true for seaward extension. This is even clearer using a low-pass filter on velocity  
554 fluctuations, removing a large part of variability from 3D instability and wave group forcing  
555 (bottom panel of Fig. 18). What remains is closer to the usual definition of surfzone eddies  
556 as Very Low Frequency features. They are much more energetic in the deep breaking case  
557 (up to 3 times more than shallow breaking), showing a clearer EKE maximum in the inner  
558 surfzone and a large patch over the innershelf. This result is consistent with the findings from  
559 previous Boussinesq model studies that filaments forced by short-crested waves originate in  
560 the inner surfzone, then spread offshore, forming eddies that grow in scale (Johnson and  
561 Pattiaratchi, 2006).

#### 562 *4.6. 2D and 3D surfzone turbulent cascade*

563 If there is energy produced by short-crested waves in the inner surfzone of the shallow  
564 breaking case, the question is why does it not produced large filaments in the deep breaking  
565 case. We found an answer in computing the spectrum energy flux. In 2D turbulence, the  
566 flux of energy is negative and small fluctuations can grow into larger coherent structures.  
567 This process is usually involved to explain the growth of filaments and eddies from variable  
568 wave forcing (e.g., Johnson and Pattiaratchi 2006; Feddersen 2014).

569 To check its validity in a 3D model, we performed a wavenumber spectral flux analysis  
570 for pseudo-2D and 3D simulations 2D\_SC\_D0 and 3D\_SC\_D0 (Fig. 19). The spectral flux  
571 is computed as in Marchesiello et al. (2011) by spectral integration of  $v$  advection term.  
572 Consistently with 2D turbulence there is a strong inverse cascade of kinetic energy (negative  
573 flux) in the pseudo-2D model starting from the scale of injection corresponding to short-  
574 crested wave forcing (wavelength of 30-40 m here), and there is no direct cascade towards  
575 smaller scales. In the 3D case, the turbulent regime is very dissimilar. The negative flux of  
576 energy produced by variable wave forcing is present but considerably reduced. In addition,  
577 there is a second injection at smaller scales that corresponds to the most unstable mode of  
578 3D instability (wavelength of 7-10 m). This small-scale energy travels both backward and

579 forward across the spectrum and thus widens the range of variability associated with 3D  
580 instability. In the 3D long-crested wave case 3D\_LC\_D0, the same spectral flux is produced  
581 at small scales but there is no large-scale inverse cascade due to missing injection by short-  
582 crested waves.

583 This analysis shows that the growth of filaments and eddies associated with the Pere-  
584 grine process heavily relies on a 2D inverse cascade that is not robust when extending to  
585 3D dynamics. In this case, the vorticity fluctuation generated by variable waves cannot  
586 transform into coherent structures as described for the 2D paradigm created by Boussinesq  
587 models (Johnson and Pattiaratchi, 2006). The shallow water approximation simply does not  
588 hold for nearshore wave-averaged currents.

#### 589 *4.7. Oblique waves and horizontal shear instability*

590 The precedent experiments with shore-normal waves showed that shallow breaking tends  
591 to hinder the generation of large 2D eddies by short-crested waves, while sustaining forced  
592 and intrinsic 3D surfzone eddy dynamics. We now address the case of oblique waves by  
593 increasing obliquity to  $D = 20^\circ$  in order to generate longshore currents with larger horizontal  
594 shear. From linear stability analysis of a 2D problem (Bowen and Holman, 1989), the  
595 wavelength, frequency and growth rate of the most unstable shear waves are  $\lambda_h = 2.5L$  and  
596  $f_h = 0.07\frac{V}{L}$ ,  $\sigma_h = 0.15\frac{V}{L}$  where  $V$  is the longshore current magnitude and  $L$  is the longshore  
597 current half-width (outer shear). For a narrow, shoreline-intensified jet typical of Grand  
598 Popo at mid-tide (Almar et al., 2014, 2015b), shear can be strong ( $\sim 0.05 \text{ s}^{-1}$ ), implying a  
599 minimum shear wave period of 5 min, wavelength of 80 m, and growth time  $\sigma_h^{-1} = 3 \text{ min}$ .

600 Forcing long-crested waves ( $\sigma_\theta = 0$ ) with imposed deep breaking (2D\_LC\_D20), CROCO  
601 recovers results that are typical of wave-averaged shallow-water models (or 3D models with  
602 deep breaking as in Marchesiello et al. 2016, or Kumar and Feddersen 2017). Figure 20 (left  
603 panel) shows an active horizontal shear instability producing shear waves with wavelength  
604 consistent with linear theory. The shear waves propagate with the longshore current as  
605 they become nonlinearly unstable, generating filaments and eddies that propagates offshore.  
606 When both horizontal shear instability and short-crested wave vorticity generation are active

607 (with deep breaking), the result is even more energetic (Fig. 20, center panel). However,  
608 with shallow breaking, the horizontal shear instability appears much weaker and is replaced  
609 again by rib structures associated with vertical shear instability. Both processes appear  
610 reduced by vertical shear.

611 Inspection of the cross-shore profile of mean longshore currents (Fig. 6) may help to  
612 understand how shallow breaking undermine horizontal shear instability. With deep break-  
613 ing, cross-shore advection is inactive and the longshore current remains trapped over the  
614 terrace slope, and its outer shear is strong. With shallow breaking, however, the longshore  
615 current is advected by the cross-shore recirculation, stretching its profile across the terrace  
616 in a way that minimizes the outer shear. Then, the instability growth rate becomes too weak  
617 to overcome friction (from turbulence or bottom drag). This may explain why Newberger  
618 and Allen (2007) did not find horizontal shear instability in their 3D wave-averaged model  
619 solutions as opposed to many previous 2D modeling studies (Allen et al., 1996; Slinn et al.,  
620 1998; Uchiyama et al., 2009).

621 This process is verified in Figure 21, showing cross-sections of time-mean and longshore-  
622 mean eddy and mean flow features for the four cases with oblique waves. Horizontal shear  
623 instability is best assessed with the eddy-mean flow interaction term  $-\overline{u'v'}\frac{\partial \bar{v}}{\partial x}$ . In all cases,  
624 shear production is clearly correlated with outer and inner slopes of the mean longshore  
625 current, with stronger production in the outer shear. Deep-breaking cases show strong  
626 shear production and large EKE patches centered over the terrace outer slope, where the  
627 current shear is strongest. In the case of horizontal shear instability alone (2D\_LC\_D20), the  
628 magnitude is lower than that of 2D\_SC\_D20, despite similar shear intensity. This indicates an  
629 amplification of shear instability by short crested waves as they drive transient intensification  
630 of longshore currents.

631 When comparing with shore-normal wave simulations of deep breaking cases, offshore  
632 EKE seems nearly a linear combination of effects from short-crested waves and horizontal  
633 shear instability. Offshore EKE extends further than predicted from shear production due to  
634 mean and eddy advection, but short-crested waves clearly provide the most efficient process  
635 for innershelf eddy activity.

636 The shallow-breaking cases (3D\_LC\_D20 and 3D\_SC\_D20) also features shear production,  
637 but within a narrower zone and in shallower water, better controlled by friction. As a result,  
638 EKE has a reduced amplitude. Short-crested waves (3D\_SC\_D20) appear to amplify the  
639 inner surfzone energy (compared with 3D\_LC\_D20), but in both cases offshore energy is  
640 weak. Over the innershelf, the EKE magnitude can be reduced by a factor 4-5.

## 641 5. Discussion and conclusion

642 Flash rips and surfzone eddies are traditionally conceived within a depth-averaged frame-  
643 work that involves intrinsic horizontal shear instabilities or/and direct short-crested wave  
644 vorticity generation. They are revisited in this study using a 3D nonhydrostatic wave-  
645 resolving model applied to a real case with longshore-uniform topography at Grand Popo  
646 Beach, Benin. We first presented a quick overview of a new free-surface, compressible ap-  
647 proach adapted to wave-resolved nearshore dynamics. Its ability to simulate surface gravity  
648 wave propagation and nearshore breaking is validated against laboratory experiment. Then,  
649 the model is applied to Grand Popo Beach nearshore circulation generated by waves with  
650 frequency and directional spreading. We assume based on comparison with Boussinesq solu-  
651 tions that the essential difference between 2D and 3D models reduces to the vertical profile  
652 of breaking acceleration, i.e., deep or shallow breaking. This allows a direct comparison of  
653 2D and 3D frameworks within the same model equations and model setup.

654 The generation of transient rips by the 3D model is shown to differ considerably from  
655 that produced by depth-averaged models, owing to the vertical structure of currents pro-  
656 duced by shallow breaking. Processes of both horizontal shear instability and short-crested  
657 wave breaking are restricted in a 3D model by the cross-shore vertical recirculation that  
658 prevent a strong inverse cascade. Variable wave forcing (in space and time) tends to in-  
659 crease flow variability in the surfzone (especially at the surface and bottom), but it does  
660 not translate into large-scale rips streaming far offshore. Usual 2D mechanisms are replaced  
661 by a Kelvin-Helmholtz-type instability, generating rib structures with spanwise and stream-  
662 wise (alongshore and cross-shore) vorticity of intermediate scale between turbulence and  
663 large horizontal eddies — periods of 30 s to a few minutes encroaching on the infragravity

664 wave range and wavelength around 5-10 m. Streamwise filaments extend beyond the sur-  
665 fzone but with lower intensity than usual depth-averaged model rips (offshore mean EKE  
666 is reduced by 50 percent). Energy spectra and visual inspections of tracer and sediment  
667 concentration shows a much better fit of the 3D model patterns to observational data in  
668 Grand Popo Beach. Our results thus question the qualitative and quantitative relevance of  
669 depth-averaged models for nearshore dynamics.

670 These results are representative of mid-tide conditions of a low tide terrace with moderate  
671 wave heights. Interestingly, the rib structures that are described here are comparable to the  
672 *mini rips* described for similar conditions by Short et al. (1993): *Under typical mid-tide*  
673 *conditions, with waves breaking across the bar, a low 'friendly' surf zone is produced. Waves*  
674 *are less than 1 m and most water appears to head toward the shore. In fact it is return*  
675 *seaward also, both by reflection of the beach face and via the mini rips, even if no rip*  
676 *channel are present. The rips, however, are usually weak, ephemeral and shallow.*

677 In order to assess the ubiquity of mini rips in the nearshore zone, future 3D studies  
678 should address different nearshore conditions. We assume that the result would be partic-  
679 ularly sensitive to the penetration depth of wave breaking. As breaking-induced flow and  
680 turbulence are mostly produced above trough level, the breaking vertical length-scale would  
681 vary as the root-mean-square wave height  $H_{rms}$  (Uchiyama et al., 2010). In our model, it  
682 is about half of  $H_{rms}$ . Therefore, in case of higher waves, higher penetration would reduce  
683 vertical shear and increase the contribution of horizontal shear instability and short-crested  
684 waves in surfzone eddy generation — as seen in overpublicized photos of large roll-up vortices  
685 developing during high wave events. The penetration depth in our simulation is a function  
686 of subgrid scale turbulence. Increasing the Smagorinsky coefficient from 0.1 to 0.5 (which  
687 is an unrealistic limit, e.g., Canuto and Cheng 1997; Meyers and Sagaut 2006) reduces the  
688 vertical shear and largely damps vertical shear instability — the frictional time  $h^2/\nu_t$  is then  
689 close to the growth time of about 1 minute. In this case, cross-shore advection is reduced and  
690 the wave-averaged longshore flow remains in the breaker zone. Horizontal shear instability  
691 is thus stronger, but the variability associated with short-crested waves, while increasing in  
692 the inner surfzone, remains low on the innershelf. Therefore, even with high turbulence,

693 conventional 2D surf-shelf exchange processes are restrained.

694 Sensitivity to bottom roughness length  $z_0$  is another interesting aspect of our tests. We  
695 increased  $z_0$  from 0.01 to 1 mm. In this case, the drag coefficient goes from about 0.002 to  
696 0.008. Simulations with deep breaking were very sensitive to these values and the largest  
697 roughness would completely shutdown horizontal shear instability due to shorter frictional  
698 time (decreased from 5 to 2 min, i.e., shorter than growth time of about 5 min), and damp  
699 short-crested wave vortical generation. On the contrary, full 3D solutions with shallow  
700 breaking are weakly sensitive to bottom roughness, because of surface intensified currents  
701 and shorter growth time of 3D instability. These tests inspire further confidence in our  
702 results, while they point to an overemphasized importance given to bottom drag in studies  
703 using depth-averaged models (e.g., Allen et al. 1996).

704 Finally, an important question is what exactly in the 3D model counteracts the generation  
705 of surf eddies by short-crested waves. Vertical vorticity generation by the Peregrine process  
706 can be written as:

$$\frac{\partial \omega_z}{\partial t} = - \frac{\partial F_{br}}{\partial y_c} \quad (22)$$

707 where  $F_{br}$  is the breaking force, extending to the bottom in a depth-averaged model, and  $y_c$   
708 is the along-crest direction. Using a breaking parametrization, Clark et al. (2012) propose  
709 a scaling relation for vorticity generation of a single wave as  $\frac{H_s^3}{h^{2.5}}$ , at a maximum in the  
710 outer surfzone. However, flash rip generation originates in the inner surfzone in depth-  
711 averaged models (Johnson and Pattiaratchi, 2006) and in our deep breaking simulations. The  
712 reason is that adding a transient source of vorticity is not enough to generate a horizontal  
713 recirculation (with offshore filament). It needs a coastal boundary and an inverse energy  
714 cascade that transform vorticity fluctuations into larger-scale coherent structures, as shown  
715 by our spectral flux analysis (Sec. 4.6 and Fig. 19). In a 3D turbulent regime, this cascade  
716 is much reduced (due to vortex tilting by the shear flow; McWilliams et al. 2018) and the  
717 variability generated in the inner surfzone does not translate into large rips jetting offshore.  
718 The inhibition of inverse cascade persist with higher viscosity ( $C_s = 0.5$ ), which however  
719 damps 3D instabilities. Therefore, tridimensionality is responsible for both counteracting

720 the generation of large horizontal eddies, and favoring that of intermediate-scale 3D mini  
721 rips.

722 In conclusion, our results suggest that nearshore dynamics and transport processes may  
723 be dominated by nonhydrostatic dynamics, not only for surface gravity waves as is known  
724 since the 19<sup>th</sup> century, but also for vortical motions. This conclusion should hold for mod-  
725 erate waves in other applications but further studies should explore the range of waves and  
726 topographic conditions encountered in the global coastal ocean.

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733 [org](http://www.croco-ocean.org). Both observational and modeling data are available upon request.

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Table 1: Model setup of CROCO's Grand Popo Beach configuration

Model parameters	Values
Grid type	Horizontal: rectangular, regular mesh; vertical: terrain following grid with free surface
Domain size ( $L_x, L_y$ )	240 x 542 m
Horizontal resolution (dx/dy)	1 m
Vertical grid (Nz)	10 levels (dz=10 cm over the terrace)
Time step	dt=0.025 s, dt <sub>f</sub> =0.001 s, c <sub>sound</sub> =200 m/s (pseudo-acoustic)
Bathymetry (h)	longshore-uniform low tide terrace derived from March 2014 survey
Tides	mid-tide: 1-m depth over the terrace
Wave forcing (u,v,w at offshore boundary)	linear wave solutions reconstructed from JONSWAP spectrum with $H_s = 1.15$ m and $T_p = 11$ s
Air-sea forcing (u,v,T,S fluxes)	0
Sediment model (D50, Ws, $E_0$ , $\tau_{cr}$ )	$D50 = 100 \mu\text{m}$ ; $Ws=5$ mm/s; $E_0 = 10^{-5}$ kg/m <sup>2</sup> /s; $\tau_{cr} = 0.01$ N/m <sup>2</sup>
Breaking/turbulence	WENO5-Z shock-capturing advection scheme Smagorinsky SGS model ( $C_S = 0.1$ )
Bottom roughness ( $z_0$ )	0.01-1 mm

Table 2: List of CROCO simulations for Grand Popo Beach.

Simulation	Breaking	Wave type	Direction	Test
3D_SC_D10	shallow	short-crested	10°	Data vs. 3D instab. vs. Peregrine process
2D_SC_D10	deep	short-crested	10°	
3D_SC_D0	shallow	short-crested	0°	3D instab. vs. Peregrine process
2D_SC_D0	deep	short-crested	0°	
3D_LC_D0	shallow	long-crested	0°	
3D_MONO_D0	shallow	monochromatic	0°	
3D_SC_D20	shallow	short-crested	20°	3D instab. vs. 2DH instab. vs. Peregrine process
3D_LC_D20	shallow	long-crested	20°	
2D_SC_D20	deep	short-crested	20°	
2D_LC_D20	deep	long-crested	20°	
FUNWAVE-TVD	deep	short-crested	0°	Test of pseudo-2D CROCO

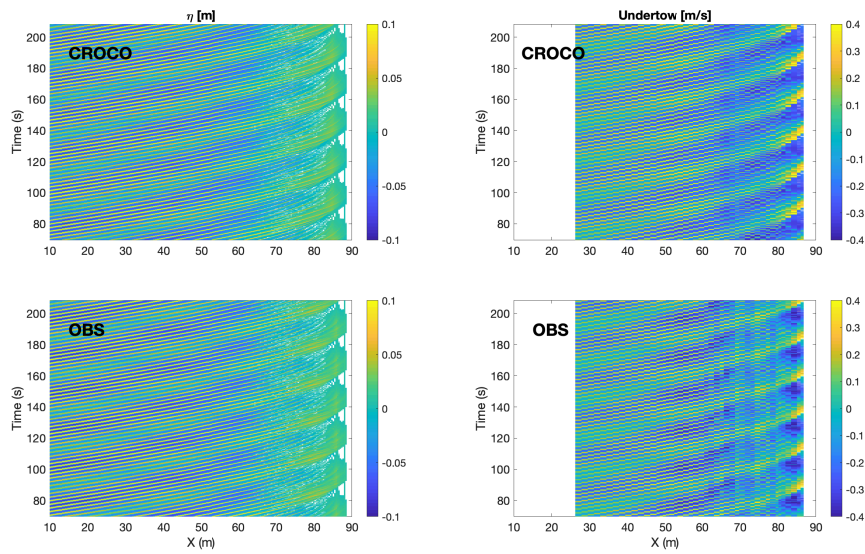


Figure 1: Hovmuller plot  $(x, \text{time})$  of data and model sea level  $\eta$  and undertow  $u_b$  for the GLOBEX B3 flume experiment. When data is missing in the measurements, it is also removed from the model output.

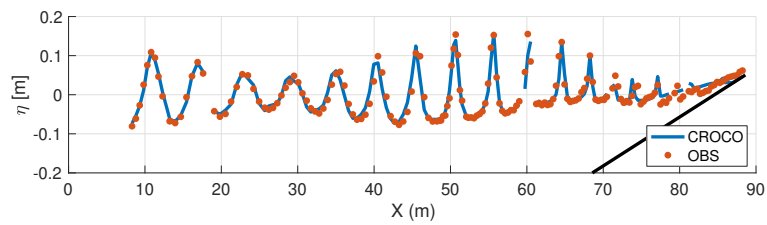


Figure 2: Snapshot of wave field across the GLOBEX B3 flume experiment during runup conditions for model (blue line) and data (red dots).

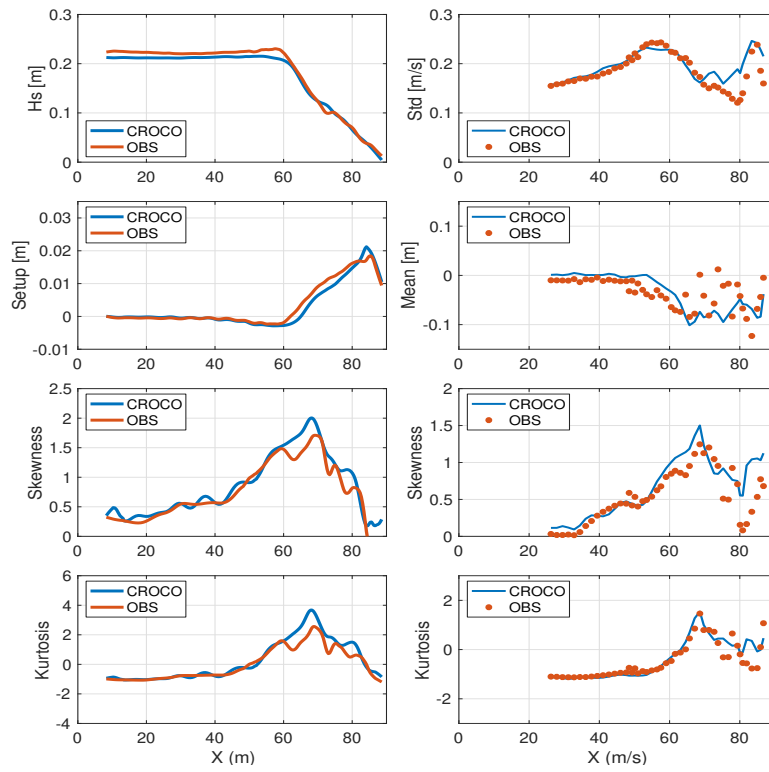


Figure 3: Wave statistics from GLOBEX B3 experiment for sea level  $\eta$  and undertow  $u_b$  in model (blue line) and data (red line or dots). From top to bottom: standard deviation (or  $H_s$  for  $\eta$ ), mean, skewness and kurtosis.



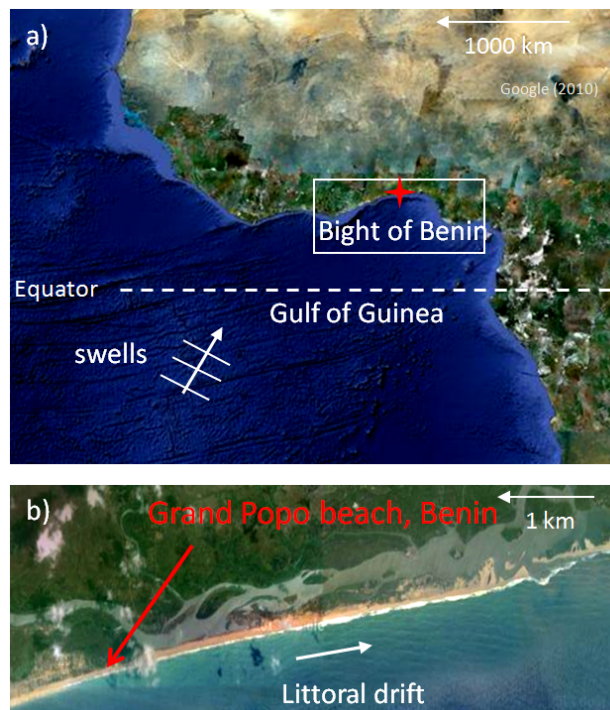


Figure 4: Grand Popo Beach, Benin, is a longshore uniform beach located in the Gulf of Guinea. It is representative of an open, wave-dominated and microtidal environment exposed to S-SW long period swells generated at high latitudes in the South Atlantic.

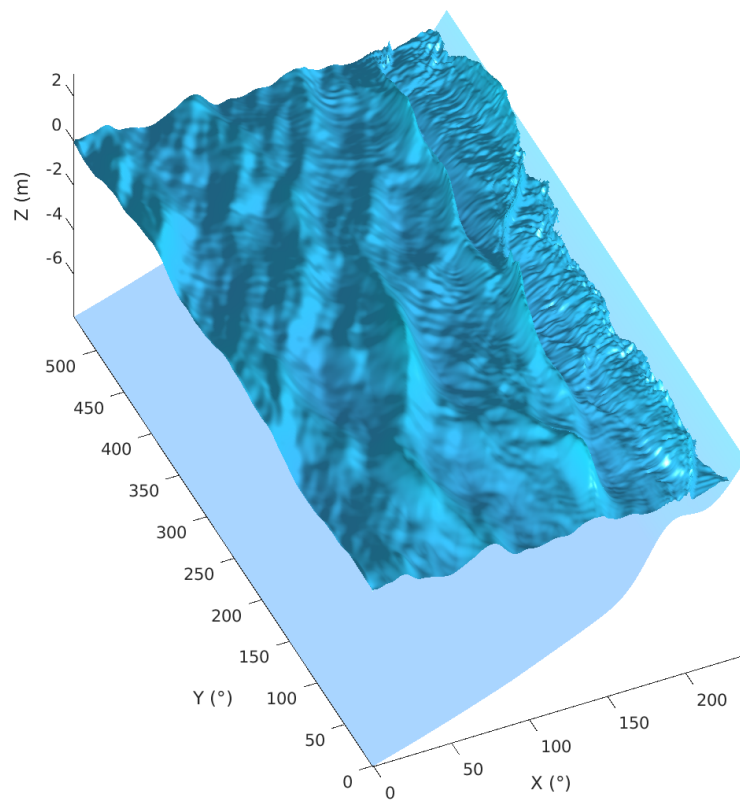


Figure 5: CROCO sea level snapshot, showing short-crested waves generated at the offshore boundary and propagating shoreward at an angle of  $10^\circ$ , with refraction and breaking through the surf and swash zones.

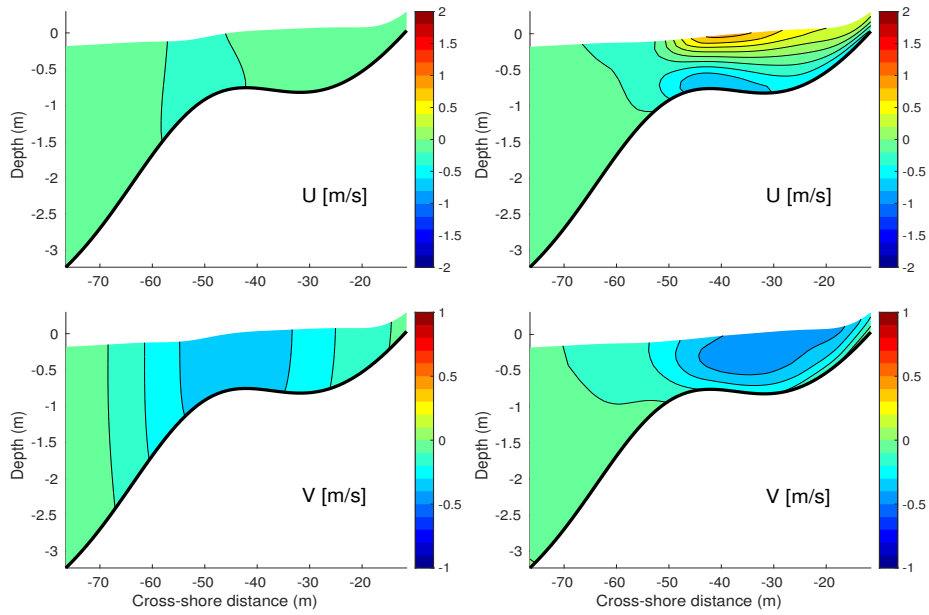


Figure 6: Cross-section of time-mean and longshore-mean, cross-shore (top) and longshore (bottom) currents in the case of shallow (right) and deep (left) breaking.

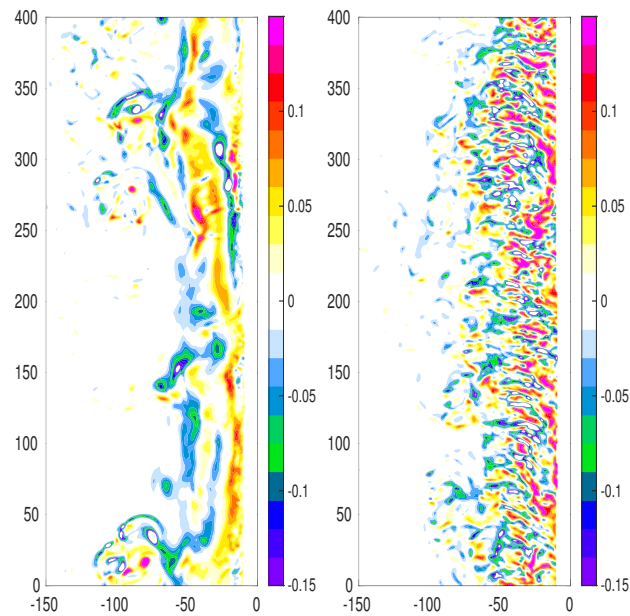


Figure 7: Vertical vorticity snapshot in the case of shallow (right) and deep (left) breaking.

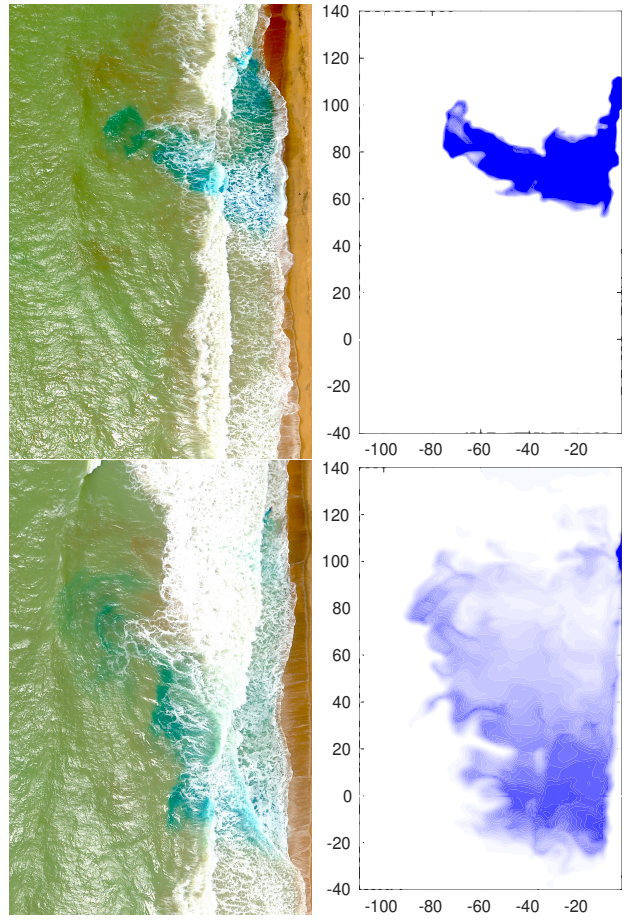


Figure 8: Drone photos (left) and CROCO simulations (right) of dye release at 154 s interval during the Grand Popo survey of March 13 2014 at afternoon mid-tide.

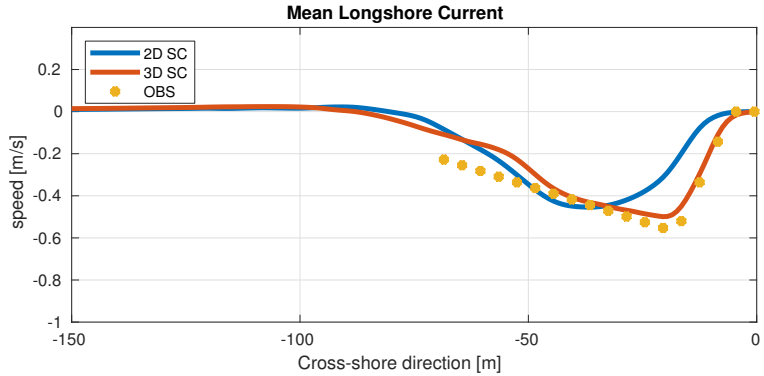


Figure 9: Cross-shore profile of time-mean and longshore-mean surface longshore flow for the full 3D simulation with wave direction  $D = 10^\circ$ . An estimation of Lagrangian velocities from drone photos of Figure 8 is added for comparison.

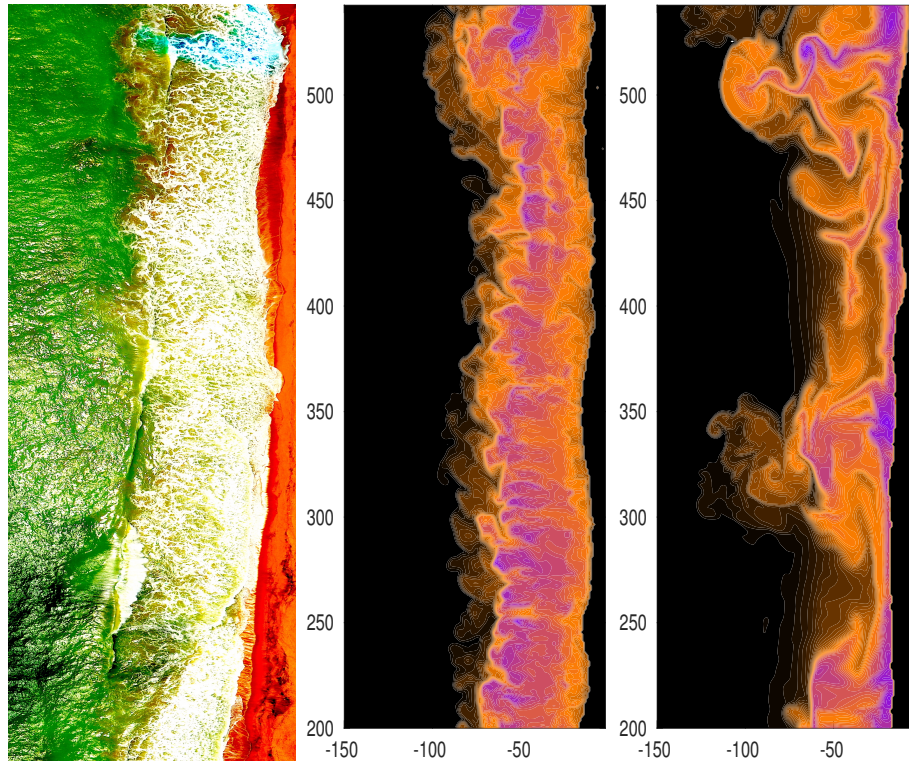


Figure 10: Aerial photo (left) and CROCO simulations of surfzone suspended sediments for shallow-breaking (center) and deep-breaking (right) cases. The contrasts in the photo is enhanced to better expose suspended sediments (brown color). The model suspended sediments correspond to snapshots at 15 min of simulation.

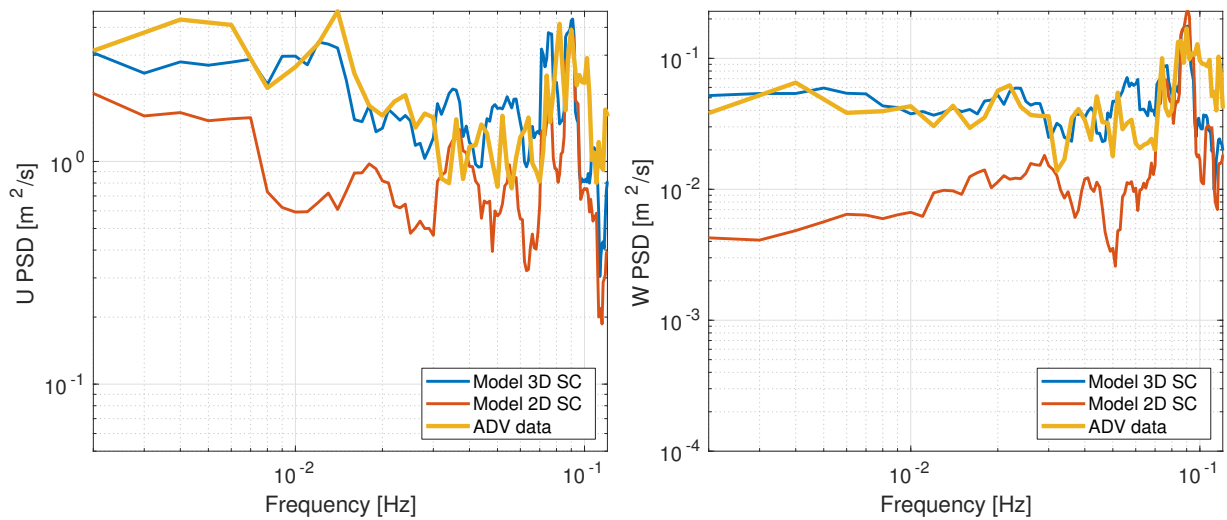


Figure 11: Power Spectral Density of horizontal (left) and vertical (right) velocity fluctuations compared with ADV measurements in the middle of the terrace, in March 13 2014 at afternoon mid-tide.

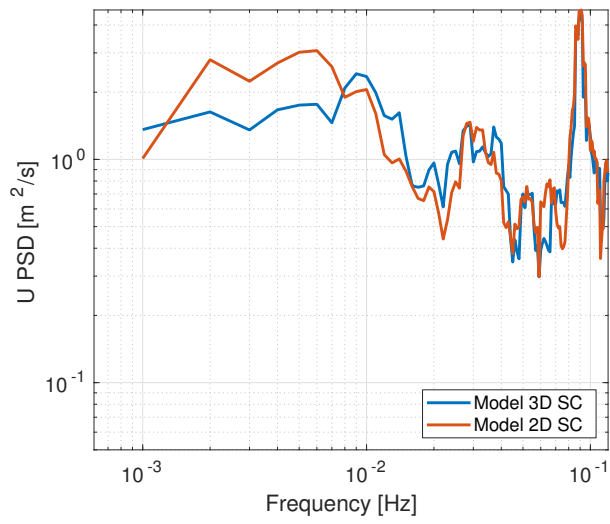


Figure 12: Power Spectral Density of offshore horizontal velocity fluctuations in March 13 2014 at afternoon mid-tide.

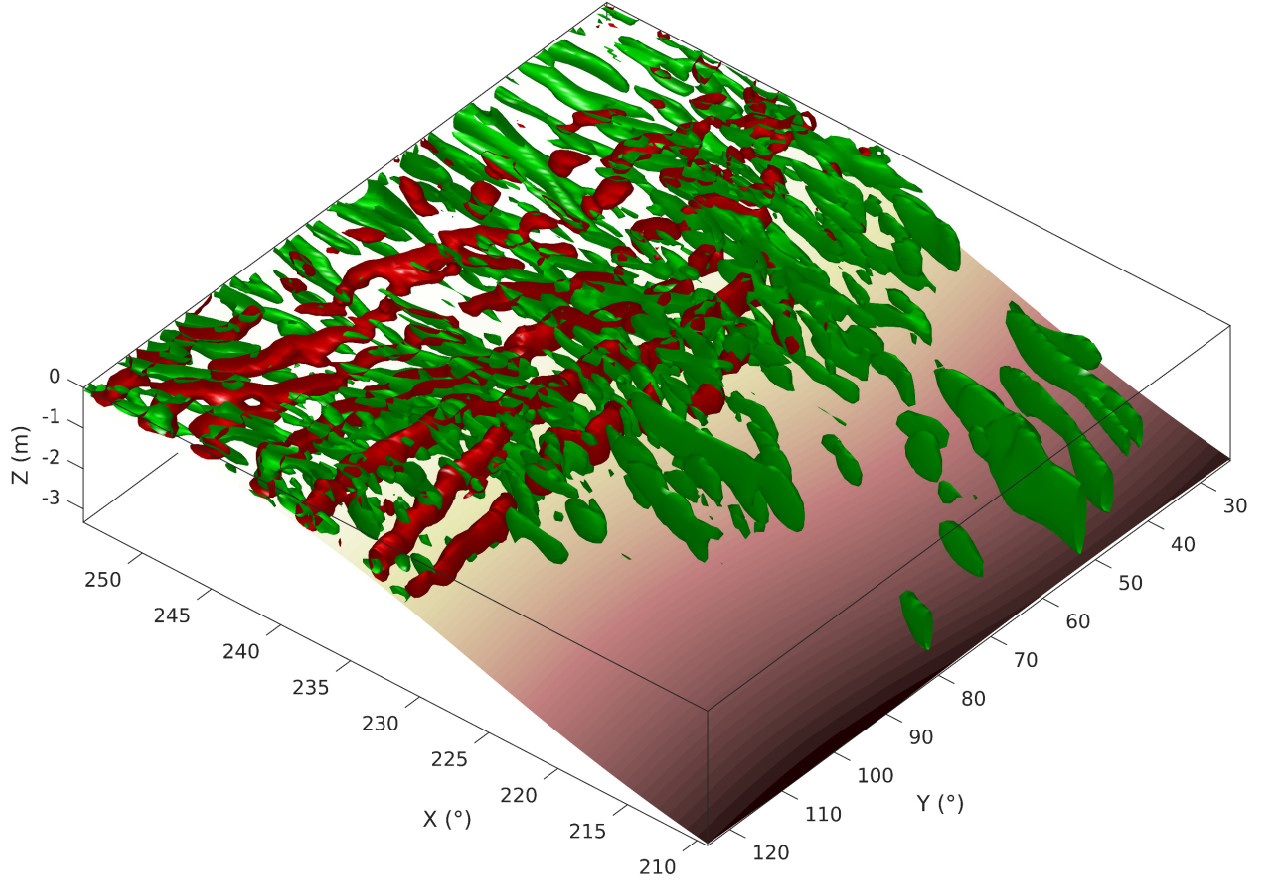


Figure 13:  $Q$  field defined by  $Q = -\frac{1}{2} \frac{\partial u_i}{\partial x_j} \frac{\partial u_j}{\partial x_i}$ , showing coherent structures similar to rolls and ribs in a transitional mixing layer. Cross-shore and alongshore  $Q$  terms are split: spanwise rolls (aligned across shear direction) are identified by  $Q_y = -\frac{\partial u}{\partial z} \frac{\partial w}{\partial x} - \frac{1}{2} \frac{\partial u^2}{\partial x}$  in red; and streamwise ribs (along shear direction) are identified by  $Q_x = -\frac{\partial v}{\partial z} \frac{\partial w}{\partial y} - \frac{1}{2} \frac{\partial v^2}{\partial y}$  in green. The fields are normalized and only positive isosurface values (0.02) are plotted.

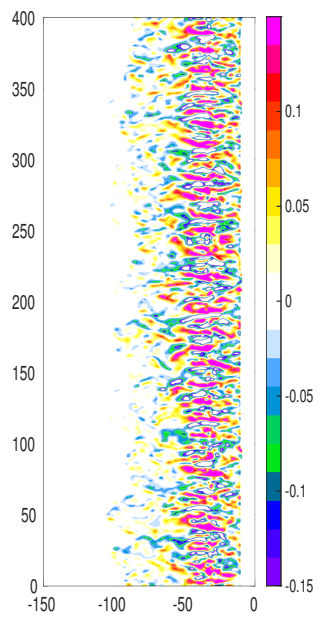


Figure 14: Vertical vorticity snapshot for the case with monochromatic shore-normal wave forcing (3D\_MONO\_D0)



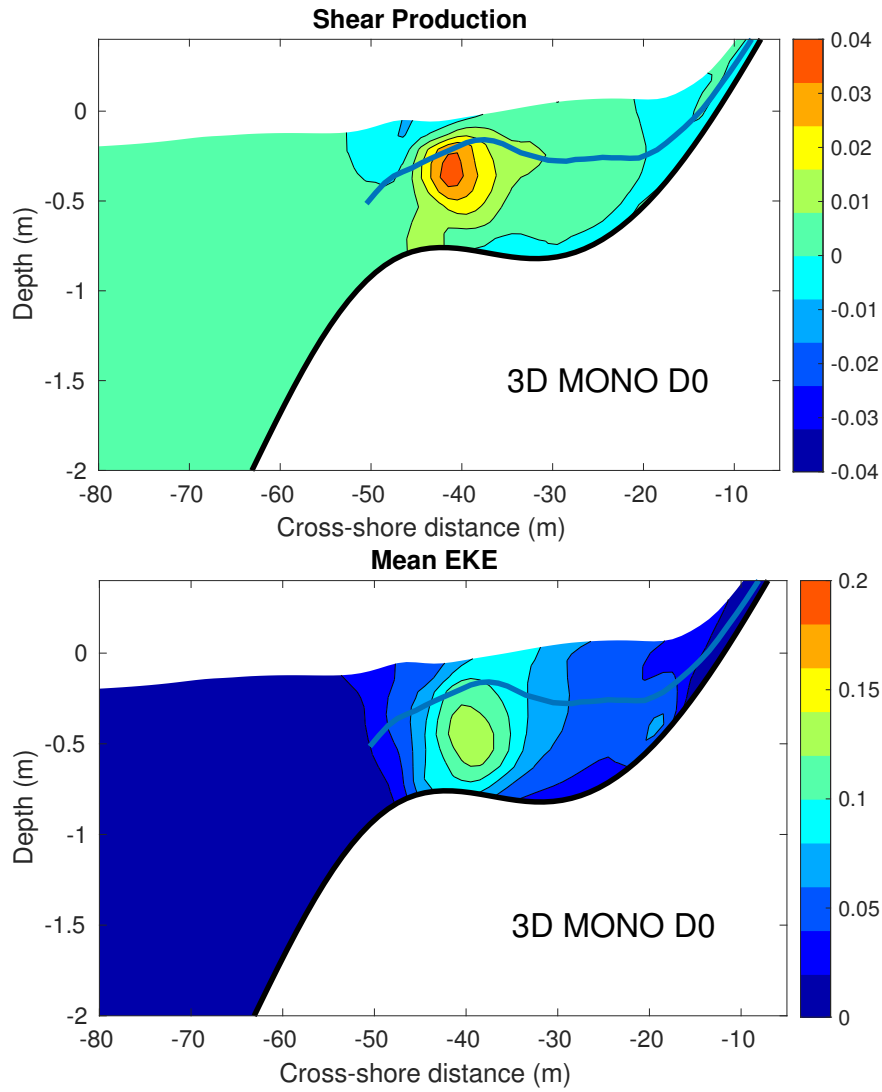


Figure 15: Cross-section of EKE [ $m^2/s^3$ ] (bottom) and EKE production by the mean shear flow (top) [ $m^2/s^3$ ] for the case with 3D instabilities only, forced with monochromatic long-crested waves (3DMONOD0). The position of shear flow inflection point is drawn in a blue line

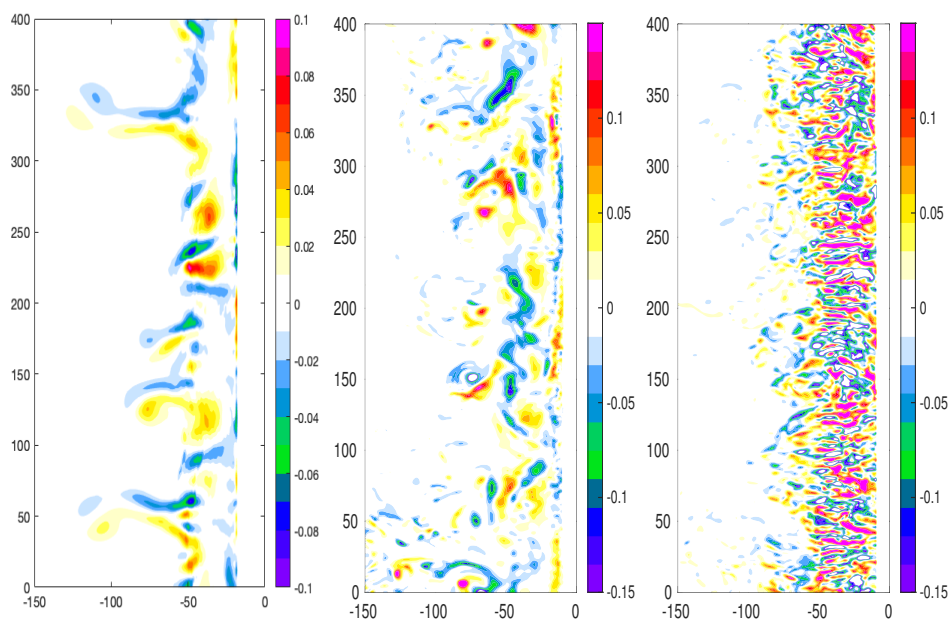


Figure 16: Vertical vorticity snapshot for 3 cases with shore-normal wave forcing: FUNWAVE-TVD (2D Boussinesq) with short-crested waves (left); CROCO with short-crested waves and deep breaking (center); short-crested waves and shallow breaking (right).

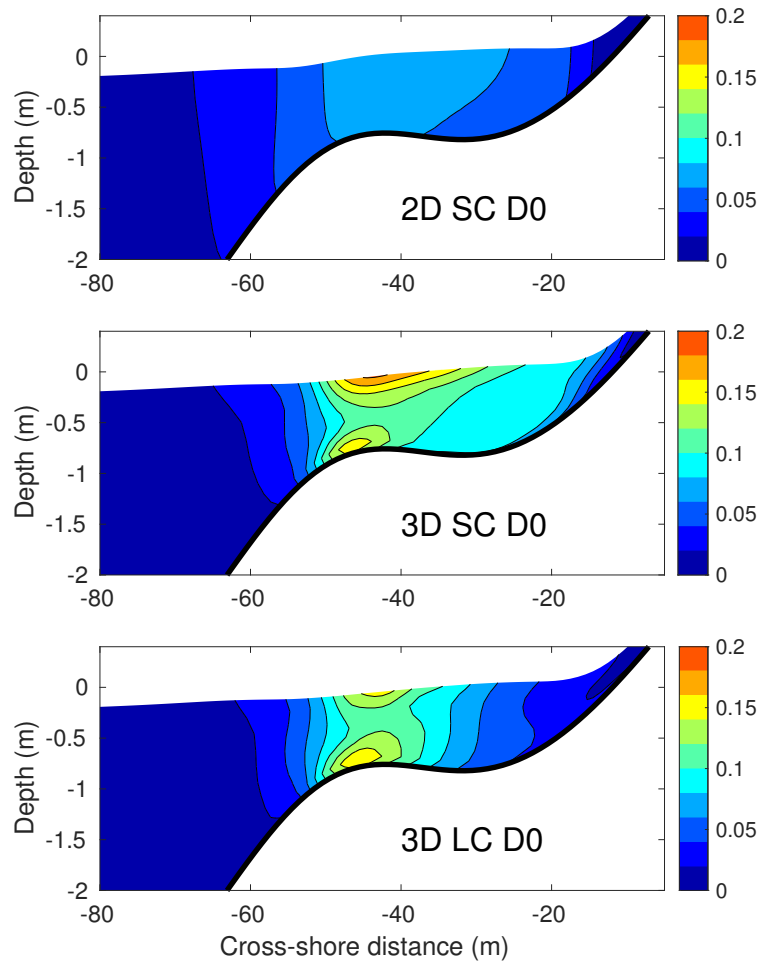


Figure 17: Cross-section of time-mean and longshore-mean EKE for the 3 cases of Figure 16

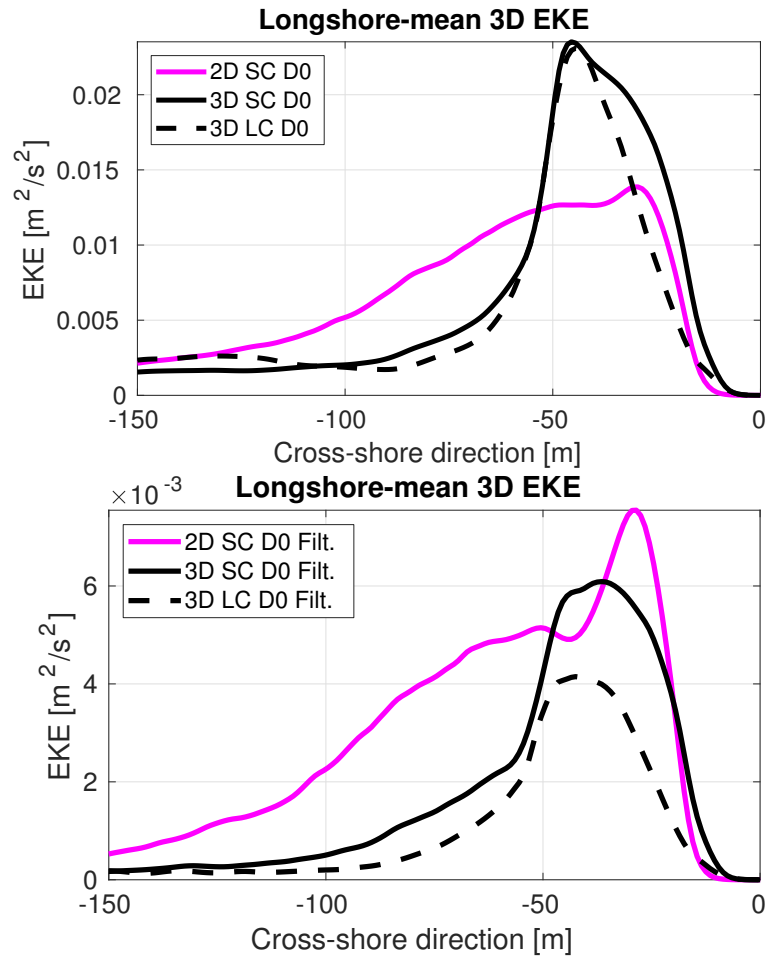


Figure 18: Cross-shore profile of depth-integrated (normalized), time and longshore-mean EKE for the 3 cases in Figure 16. Top: EKE of wave-averaged flow; bottom: EKE of low-pass filtered flow to remove 3D instability modes.

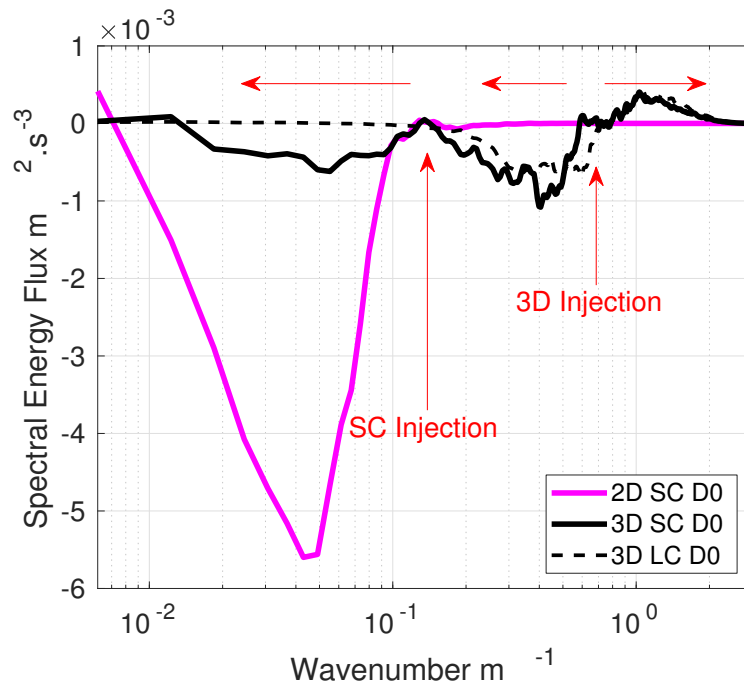


Figure 19: 3D and 2D model wavenumber spectral flux in the surfzone. Vertical red arrows point to the wavenumbers of energy injection from short-crested waves ( $\sim 40$  m wavelength) and from 3D shear instability ( $\sim 10$  m). The spectral flux is computed by spectral integration of  $v$  advection term (Marchesiello et al., 2011). Horizontal red arrows indicate positive/negative fluxes, i.e., direct/inverse energy cascade toward smaller/larger scales.

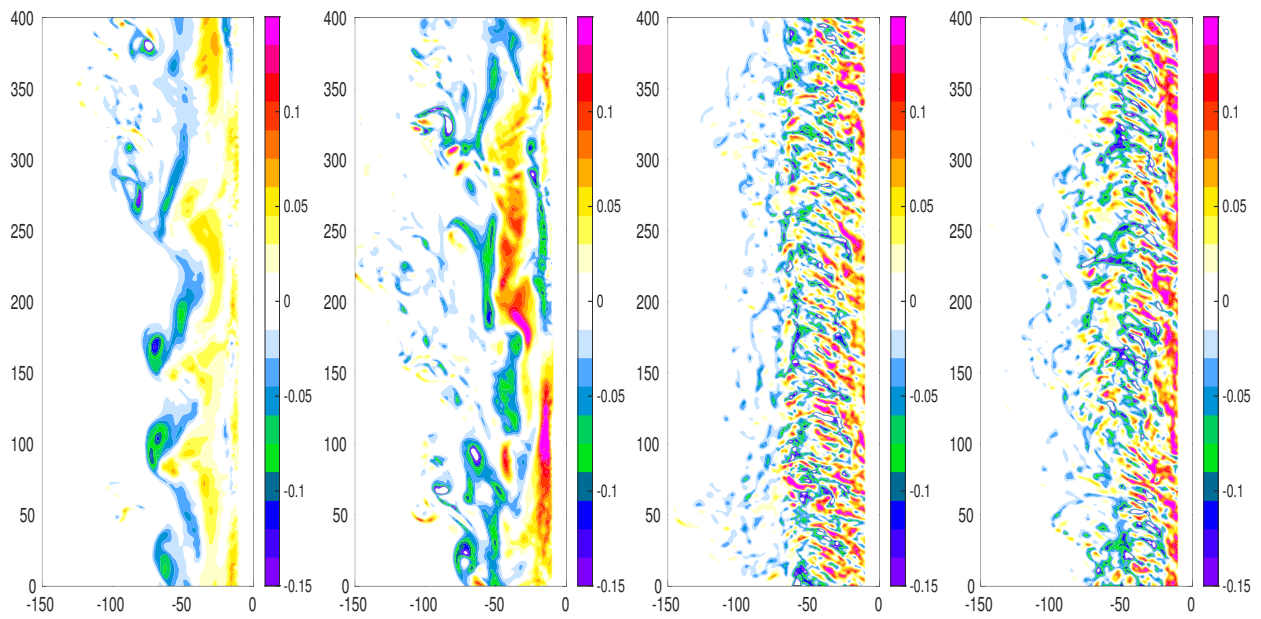


Figure 20: Snapshot of vorticity fields for 4 cases with oblique waves: long-crested waves with deep breaking (2D\_LC\_D20: first left); short-crested waves with deep breaking (2D\_SC\_D20: second left); long-crested waves with shallow breaking (3D\_LC\_D20: first right) and short-crested waves with shallow breaking (3D\_SC\_D20: last right).

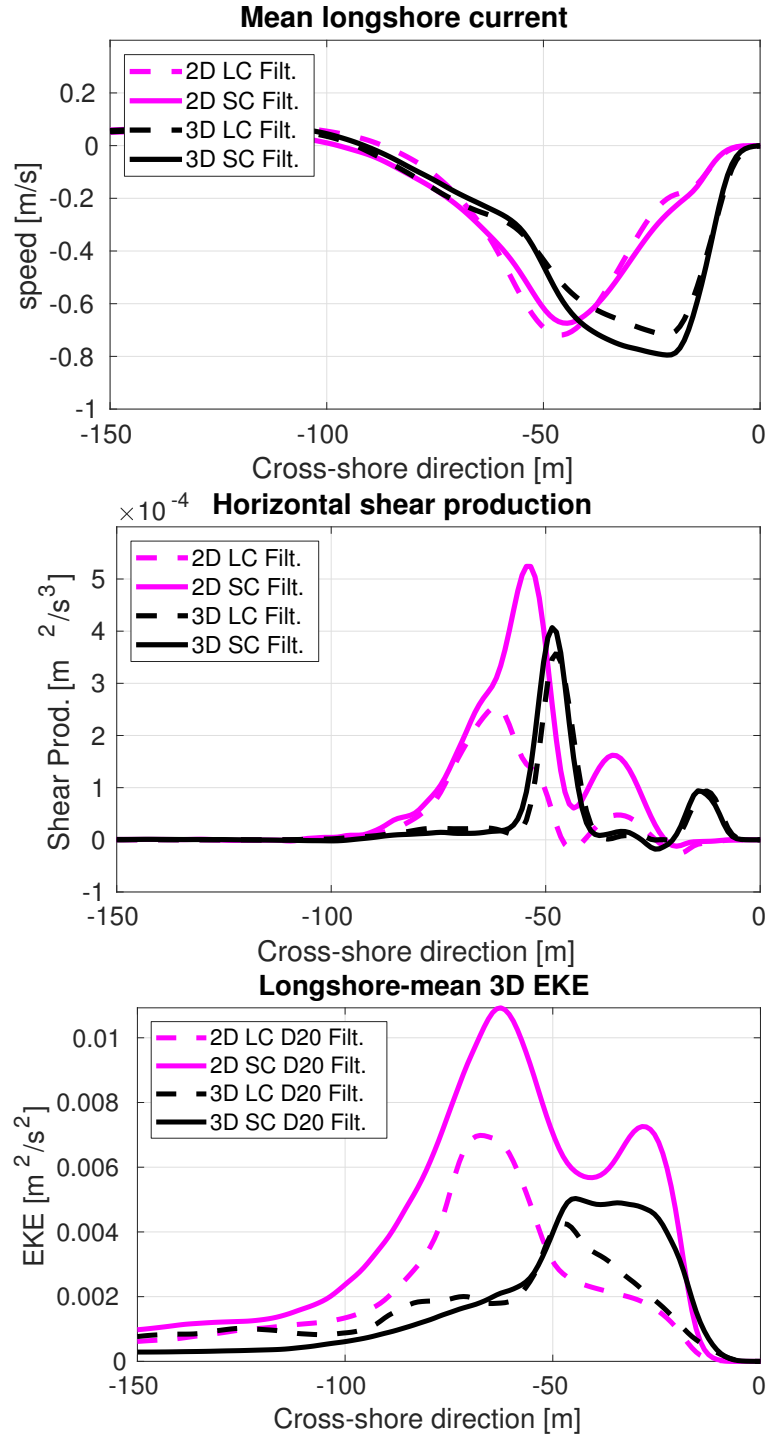


Figure 21: Cross-shore profile of time-mean and longshore-mean flow and eddy statistics for the 4 cases in Figure 16; top) surface longshore flow; center): horizontal shear production  $-\overline{u'v'}\frac{\partial \bar{v}}{\partial x}$ ; bottom) depth-integrated (normalized) EKE (computed from low-pass filtered velocities showing low-frequency modes).