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Automatic Self-Calibration of Suspended Under-Actuated Cable-Driven Parallel Robot using Incremental Measurements

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Abstract. This paper focuses on the problem of the initial-pose estimation by means of proprioceptive sensors (self-calibration) of suspended under-actuated Cable-Driven Parallel Robots (*CDPRs*). For this class of manipulators, the initial-pose estimation cannot be carried out by means of forward kinematics only, but mechanical equilibrium conditions must be considered as well. In addition, forward kinematics solution is based on cable-length measurements, but if the robot is equipped with incremental sensors cables' initial values are unknown. In this paper, the self-calibration problem is formulated as a non-linear least square optimization problem (*NLLS*), based on the direct geometrico-static problem, where only incremental measurements on cable lengths and on swivel pulley angles are required. In addition, a data acquisition algorithm and an initial value selection procedure for the *NLLS* are proposed, aiming at automatizing the self-calibration procedure. Simulations and experimental results on a 3-cable 6-degree-of-freedom robot are provided so as to prove the effectiveness of the proposed methodology.

Keywords: Cable-driven parallel robots, Underconstrained robots, Underactuated robots, Homing, Self-calibration

1 Introduction

Cable-driven parallel robots (*CDPRs*) are a class of parallel manipulators which employs flexible cables instead of rigid links in order to control their end-effector (*e-e*) pose. A *CDPR* is completely-constrained when the pose of its *e-e* can be fully determined if actuators are locked and, thus, all cable lengths are known. On the contrary, a *CDPR* is under-constrained if the *e-e* preserves some degrees of freedom (*DoFs*) when the cable lengths are assigned. This may originate from the *e-e* being constrained by a number of cables smaller than its *DoFs* or from some cables being slack [4]. This paper focuses on suspended *CDPRs*, in which all cables are located above the *e-e*, so that their tension state only depends on the action of gravity and inertia forces. These robots are inherently under-constrained when they are under-actuated, that is, the number of actuators is less than the number of variables needed

to fully describe the manipulator. A growing number of studies are being conducted on under-actuated *CDPRs* [1, 2, 4, 6, 7, 9, 17].

A major issue in the practical use of under-actuated *CDPRs* is the estimation of the *e-e* initial-pose. When the machine is switched on in a generic start-up condition, the *e-e* pose is generally unknown, but its knowledge is fundamental for any subsequent operation. In order to directly measure the *e-e* pose, external measurement devices such as laser trackers [13] or high-resolution cameras [5] can be employed. On the other hand, an indirect estimation of the pose can be performed by measuring some of the robot's internal joint variables, followed by the solution of the direct kinematic problem [10, 14]. When this approach is used for pose estimation in start-up conditions, the solution to this problem is sometimes referred to as *self-calibration* [3] or *internal-calibration* [8] of the *e-e* initial-pose.

In [3], a self-calibration procedure for initial-pose estimation of a 2-*DoF* 4-cable over-constrained robot is proposed, which is based on cable tension and length increment measurements. The proposed method relies on the over-constrained nature of the robot. In [12] a two-stage calibration procedure for generic over-constrained *CDPRs* is introduced, aiming at both optimizing robot static parameters and determining the initial-pose of the *e-e*. Ref. [8] shows how to perform initial-pose estimation by means of a manual self-calibration procedure for over-constrained robots, only relying on cable length increment measurement.

This paper extends the method introduced in [8] by proposing an automatic procedure to estimate the initial-pose of a generic suspended under-actuated *CDPR*, e.g. a 6-*DoF* *CDPR* actuated by $n < 6$ cables, that only relies on incremental measurements of cable length and orientation. An automatic data acquisition procedure is exploited in order to reliably and autonomously collect the information required for calibration purposes. The initial-pose estimation is formulated as a non-linear least square optimization problem (*NLLS*), whose initial guess is generated automatically according to the data acquisition algorithm. In Section 2, the geometrico-static model of an under-actuated *CDPR* is developed. In Sections 3 and 4, the *NLLS* optimization problem is formulated and the data acquisition algorithm employed for its solution is discussed. Finally, simulation and experiments are presented.

2 Geometrico-Static Modelling

2.1 Kinematics

A generic 6-*DoF* under-actuated *CDPR* consists in a mobile platform connected to the base by $n < 6$ cables, which are actuated by motorized winches (Fig. 1). $Oxyz$ is an inertial frame, whereas $Px'y'z'$ is a mobile frame attached to the *e-e*. The platform pose is described by the position vector \mathbf{p}_P of P , and the rotation matrix $\mathbf{R}(\phi, \theta, \chi)$ is parametrized by Tait-Bryant angles $\boldsymbol{\epsilon} = [\phi, \theta, \chi]^T$ according to the xyz convention. The platform generalized coordinates are thus $\mathbf{p} = [\mathbf{p}_P, \boldsymbol{\epsilon}]^T \in \mathbb{R}^6$.

Cables are modelled as massless and inextensible, and are guided by swivel pulleys [15] to their attachment points A_i , $i = 1, \dots, n$ on the platform (Fig. 2a). G is the

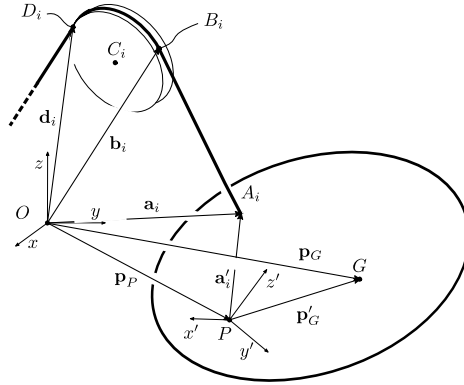


Fig. 1: Geometry of the cable-driven robot

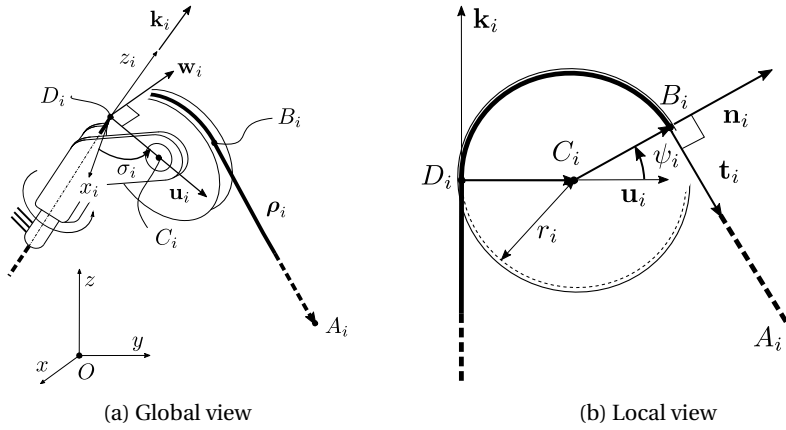


Fig. 2: Geometry of the swivel pulley

platform center of mass. If the coordinates of G and A_i in the mobile frame are described by vectors ${}^P\mathbf{p}'_G$ and ${}^P\mathbf{a}'_i$, their coordinates in the inertial frame are:

$$\mathbf{p}_G = \mathbf{p}_P + \mathbf{p}'_G = \mathbf{p}_P + \mathbf{R}^P \mathbf{p}'_G, \quad \mathbf{a}_i = \mathbf{p}_P + \mathbf{a}'_i = \mathbf{p}_P + \mathbf{R}^P \mathbf{a}'_i \quad (1)$$

The i -th swivel pulley has center C_i , radius r_i , and is mounted on a hinged support, whose swivel axis z_i is tangent to the pulley (Fig. 2a). Vector \mathbf{d}_i defines the fixed position of point D_i where the i -th cable enters the pulley's groove and which is on the z_i -axis. Unit vectors $\mathbf{i}_i, \mathbf{j}_i, \mathbf{k}_i$, associated with an additional fixed reference frame $D_i x_i y_i z_i$ attached in D_i , describe the orientation of each swivel pulley in $Oxyz$. The i -th cable exit point from the pulley groove is denoted by B_i and the vector $\boldsymbol{\rho}_i = A_i - B_i$ is tangent to the pulley.

In static conditions, if friction in the pulley hinges is negligible, vectors \mathbf{z}_i and $\boldsymbol{\rho}_i$ define the pulley plane, forming the swivel angle σ_i with the coordinate plane $x_i z_i$.

If \mathbf{u}_i and \mathbf{w}_i are unit vectors orthogonal to \mathbf{k}_i and to each other:

$$\mathbf{w}_i = -\sin \sigma_i \hat{\mathbf{i}}_i + \cos \sigma_i \hat{\mathbf{j}}_i, \quad \mathbf{u}_i = \cos \sigma_i \hat{\mathbf{i}}_i + \sin \sigma_i \hat{\mathbf{j}}_i \quad (2)$$

the aforementioned static constraint can be analytically expressed as:

$$\mathbf{w}_i \cdot (\mathbf{a}_i - \mathbf{d}_i) = 0 \quad (3)$$

which can be solved for $\sigma_i(\mathbf{p})$, if the pose is assigned.

We define $\psi_i \in (-\pi, \pi)$ as the angle between \mathbf{u}_i and $B_i - C_i$ (Fig. 2b). It is convenient to define two more unit vectors, orthogonal to \mathbf{w}_i and to each other:

$$\mathbf{n}_i = \cos \psi_i \mathbf{u}_i + \sin \psi_i \mathbf{k}_i, \quad \mathbf{t}_i = \sin \psi_i \mathbf{u}_i - \cos \psi_i \mathbf{k}_i \quad (4)$$

so that the i -th cable vector can be expressed as:

$$\boldsymbol{\rho}_i = \mathbf{a}_i - \mathbf{d}_i - r_i(\mathbf{u}_i + \mathbf{n}_i) = \|\boldsymbol{\rho}_i\| \mathbf{t}_i \quad (5)$$

where

$$\|\boldsymbol{\rho}_i\| = l_i - r_i(\pi - \psi_i) \quad (6)$$

is the rectilinear cable length, and l_i is the i -th total cable length, comprising the rectilinear part and the wrapped part $\widehat{B_i D_i}$. The tangency constraint between $\boldsymbol{\rho}_i$ and the pulley can be expressed as:

$$\mathbf{n}_i \cdot \boldsymbol{\rho}_i = 0 \quad (7)$$

which can be solved for $\psi_i(\mathbf{p})$, if the pose (and thus the swivel angle) are known.

Once $\psi_i(\mathbf{p})$ and $\sigma_i(\mathbf{p})$ are determined, $l_i(\mathbf{p})$ can be found from the geometrical constraint that the i -th cable imposes on the platform:

$$\boldsymbol{\rho}_i^T \boldsymbol{\rho}_i - \|\boldsymbol{\rho}_i\|^2 = 0 \quad (8)$$

where $\boldsymbol{\rho}_i$ is evaluated as in Eq. (5) and $\|\boldsymbol{\rho}_i\|$ as in Eq. (6).

2.2 Statics

For the purpose of this work, we will consider that the e - e is acted upon by a constant force only, e.g. gravity, which is parallel to the z axis and applied at point G . Thus, if the e - e mass is m , the gravitational acceleration is g , and $\tilde{\mathbf{p}}'_G$ is the skew-symmetric representation of the vector product, namely $\mathbf{p}'_G \times = \tilde{\mathbf{p}}'_G$, the external wrench applied to the reference point P is $\mathbf{W} = -mg[\mathbf{k}; \tilde{\mathbf{p}}'_G \mathbf{k}]$.

If all cables are taut, the static equilibrium equations of the e - e is:

$$\mathbf{J}^T \mathbf{T} - \mathbf{W} = \mathbf{0} \quad (9)$$

where $\mathbf{T} = [T_1, \dots, T_n]^T$, T_i is the cable tension, and $\mathbf{J} \in \mathbb{R}^{n \times 6}$ is the Jacobian matrix of the constraints in Eq. (8), whose i -th row is $\mathbf{J}_i = [\mathbf{t}_i^T \quad -\mathbf{t}_i^T \tilde{\mathbf{a}}'_i]$. It is convenient to

partition \mathbf{J} in a $n \times n$ matrix \mathbf{J}_a and a $n \times (6 - n)$ matrix \mathbf{J}_u , namely $\mathbf{J} = [\mathbf{J}_a \ \mathbf{J}_u]$, and vector \mathbf{W} as $\mathbf{W} = [\mathbf{W}_a; \mathbf{W}_u]$, so that Eq. (9) can be rewritten as:

$$\mathbf{J}_a^T \mathbf{T} - \mathbf{W}_a = \mathbf{0} \quad (10)$$

$$\mathbf{J}_u^T \mathbf{T} - \mathbf{W}_u = \mathbf{0} \quad (11)$$

The first part can be solved for \mathbf{T} , thus yielding:

$$\mathbf{T} = \mathbf{J}_a^{-T} \mathbf{W}_a \quad (12)$$

and the result can be substituted in the second part, thus obtaining the static equilibrium constraint of the platform:

$$\mathbf{J}_u^T \mathbf{J}_a^{-T} \mathbf{W}_a - \mathbf{W}_u = \mathbf{0} \quad (13)$$

2.3 Forward Geometrico-Static Problem

The aim of the forward geometrico-static problem is to find the *e-e* pose, once the value of a suitable set of the robot's internal joint variables is known. In the case that only cable length measurements are available, it is possible to formulate such a problem by considering the n constraints in Eq. (8) and the $6 - n$ equations in Eq. (13) [1]. The resulting system of nonlinear equations is completely determined and, thus, can be numerically solved by using nonlinear solvers. Alternatively, if redundant measurements are available, one can (possibly) neglect the static constraint equations and replace them with additional kinematic constraint equations that are explicitly dependent on the measured variables [10]. This approach leads to a system of equations that, depending on the number and the type of redundant measurements, can be completely determined or overdetermined (the system is never underdetermined, because static equilibrium constraints can always be accounted for).

In this paper, we assume that both cable lengths and swivel pulley angles can be measured. For the sake of generality, we formulate the forward geometrico-static problem by considering both $2n$ kinematic constraints, derived from Eqs. (3) and (8), and the $6 - n$ static equilibrium constraints of Eq. (13), thus leading to an overdetermined system of $6 + n$ equations in 6 unknowns (namely, the generalized pose coordinates in \mathbf{p}). By letting:

$$\mathbf{F}_1(\mathbf{p}) = \begin{bmatrix} \sigma_1(\mathbf{p}) - \sigma_1^* \\ \vdots \\ \sigma_n(\mathbf{p}) - \sigma_n^* \end{bmatrix}, \quad \mathbf{F}_2(\mathbf{p}) = \begin{bmatrix} l_1(\mathbf{p}) - l_1^* \\ \vdots \\ l_n(\mathbf{p}) - l_n^* \end{bmatrix}, \quad \mathbf{F}_3(\mathbf{p}) = \mathbf{J}_u^T \mathbf{J}_a^{-T} \mathbf{W}_a - \mathbf{W}_u \quad (14)$$

where $\sigma_i(\mathbf{p})$ and $l_i(\mathbf{p})$ can be easily calculated from Eqs. (3) and (8), and σ_i^* and l_i^* are the corresponding measured values, the forward geometrico-static problem can be formulated as:

$$\mathbf{F}(\mathbf{p}) = \begin{bmatrix} \mathbf{F}_1(\mathbf{p}) \\ \mathbf{F}_2(\mathbf{p}) \\ \mathbf{F}_3(\mathbf{p}) \end{bmatrix} = \mathbf{0} \quad (15)$$

This formulation leads to a fairly simple analytical formulation of the first-order differentiation of Eq. (15), as described in Section 3.

3 Initial-Pose Estimation Problem

In this section, the initial-pose estimation problem will be formulated by extending the work presented in [8]. If the under-actuated *CDPR* is equipped with incremental measurement devices on motors and swivel axes, i.e. incremental encoders, cable lengths and swivel angles at a generic pose \mathbf{p}_i can be measured relatively to the initial values σ_i^0 and l_i^0 at pose \mathbf{p}_0 , namely:

$$\sigma_i^* = \sigma_i^0 + \Delta\sigma_i^* \quad (16)$$

$$l_i^* = l_i^0 + \Delta l_i^* \quad (17)$$

While $\Delta\sigma_i^*$ and Δl_i^* are measures provided by the encoders, σ_i^0 and l_i^0 are generally unknown and are the objective of the self-calibration procedure. The direct geometrico-static problem in Eq. (15) can thus be expressed as:

$$\mathbf{F}(\boldsymbol{\sigma}^0, \mathbf{l}^0, \mathbf{p}) = \mathbf{0} \quad (18)$$

where $\boldsymbol{\sigma}^0 = [\sigma_1^0, \dots, \sigma_n^0]^T$ and $\mathbf{l}^0 = [l_1^0, \dots, l_n^0]^T$. This problem has $6 + n$ equations and $6 + 2n$ unknowns ($\boldsymbol{\sigma}^0, \mathbf{l}^0, \mathbf{p}$), and it has generally an infinite number of solutions.

However, by assuming that λ different measurement sets are available, that is:

$$\begin{aligned} \sigma_{i,k}^* &= \sigma_i^0 + \Delta\sigma_{i,k}^* \\ l_{i,k}^* &= l_i^0 + \Delta l_{i,k}^* \end{aligned} \quad k = 1, \dots, \lambda \quad (19)$$

the following system of equations is obtained:

$$\mathbf{G}(\mathbf{X}) = \mathbf{G}(\boldsymbol{\sigma}^0, \mathbf{l}^0, \mathbf{p}_1, \dots, \mathbf{p}_\lambda) = [\mathbf{F}(\boldsymbol{\sigma}^0, \mathbf{l}^0, \mathbf{p}_1); \dots; \mathbf{F}(\boldsymbol{\sigma}^0, \mathbf{l}^0, \mathbf{p}_\lambda)] = \mathbf{0} \quad (20)$$

where $\mathbf{X} = [\boldsymbol{\sigma}^0; \mathbf{l}^0; \mathbf{p}_1; \dots; \mathbf{p}_\lambda] \in \mathbb{R}^{6\lambda+2n}$.

The system (20) has a total of $\lambda(6 + n)$ equations and $6\lambda + 2n$ unknowns. Thus, if $\lambda > 2$, the initial-pose estimation problem is overdetermined and can be formulated as a non-linear least-square optimization:

$$\mathbf{X}_{opt} = \underset{\mathbf{X}}{\operatorname{arg\,min}} \|\mathbf{G}(\mathbf{X})\|^2 \quad (21)$$

This problem can be solved by employing numerical techniques, such as the Levenberg-Marquardt algorithm. The efficient solution of Eq. (21) relies on a reasonable initial guess \mathbf{X}_{guess} (see Section 4), and an analytical formulation of the Jacobian matrix in Eq.(20). While the former is fundamental for both the solution accuracy and the algorithm rapidity, the latter is critical only in terms of computational time.

The Jacobian $\partial\mathbf{G}/\partial\mathbf{X}$ can be expressed analytically as:

$$\frac{\partial \mathbf{G}}{\partial \mathbf{X}} = \begin{bmatrix} -\mathbf{I}_{n \times n} & \mathbf{0}_{n \times n} & \partial \boldsymbol{\sigma}(\mathbf{p}_1)/\partial \mathbf{p} & \mathbf{0}_{n \times 6} & \cdots & \mathbf{0}_{n \times 6} \\ \mathbf{0}_{n \times n} & -\mathbf{I}_{n \times n} & \partial \mathbf{l}(\mathbf{p}_1)/\partial \mathbf{p} & \mathbf{0}_{n \times 6} & \cdots & \mathbf{0}_{n \times 6} \\ \mathbf{0}_{(6-n) \times n} & \mathbf{0}_{(6-n) \times n} & \partial \mathbf{F}_3(\mathbf{p}_1)/\partial \mathbf{p} & \mathbf{0}_{(6-n) \times 6} & \cdots & \mathbf{0}_{(6-n) \times 6} \\ -\mathbf{I}_{n \times n} & \mathbf{0}_{n \times n} & \mathbf{0}_{n \times 6} & \partial \boldsymbol{\sigma}(\mathbf{p}_2)/\partial \mathbf{p} & \cdots & \mathbf{0}_{n \times 6} \\ \mathbf{0}_{n \times n} & -\mathbf{I}_{n \times n} & \mathbf{0}_{n \times 6} & \partial \mathbf{l}(\mathbf{p}_2)/\partial \mathbf{p} & \cdots & \mathbf{0}_{n \times 6} \\ \mathbf{0}_{(6-n) \times n} & \mathbf{0}_{(6-n) \times n} & \mathbf{0}_{(6-n) \times 6} & \partial \mathbf{F}_3(\mathbf{p}_2)/\partial \mathbf{p} & \cdots & \mathbf{0}_{(6-n) \times 6} \\ \vdots & \vdots & \vdots & \vdots & \ddots & \vdots \\ -\mathbf{I}_{n \times n} & \mathbf{0}_{n \times n} & \mathbf{0}_{n \times 6} & \mathbf{0}_{n \times 6} & \cdots & \partial \boldsymbol{\sigma}(\mathbf{p}_\lambda)/\partial \mathbf{p} \\ \mathbf{0}_{n \times n} & -\mathbf{I}_{n \times n} & \mathbf{0}_{n \times 6} & \mathbf{0}_{n \times 6} & \cdots & \partial \mathbf{l}(\mathbf{p}_\lambda)/\partial \mathbf{p} \\ \mathbf{0}_{(6-n) \times n} & \mathbf{0}_{(6-n) \times n} & \mathbf{0}_{(6-n) \times 6} & \mathbf{0}_{(6-n) \times 6} & \cdots & \partial \mathbf{F}_3(\mathbf{p}_\lambda)/\partial \mathbf{p} \end{bmatrix} \quad (22)$$

where $\mathbf{I}_{n \times n}$ and $\mathbf{0}_{n \times n}$ are the $n \times n$ identity and zero matrices, $\boldsymbol{\sigma}(\mathbf{p}_k) = [\sigma_1(\mathbf{p}_k); \cdots; \sigma_n(\mathbf{p}_k)]$ and $\mathbf{l}(\mathbf{p}_k) = [l_1(\mathbf{p}_k); \cdots; l_n(\mathbf{p}_k)]$. Manipulating Eqs. (3), (7) and (8) yields:

$$\frac{\partial \sigma_i}{\partial \mathbf{p}} = \left[\frac{\mathbf{w}_i^T}{\mathbf{u}_i^T(\mathbf{a}_i - \mathbf{d}_i)} \quad -\frac{\mathbf{w}_i^T \tilde{\mathbf{a}}_i^T \mathbf{H}}{\mathbf{u}_i^T(\mathbf{a}_i - \mathbf{d}_i)} \right], \quad \frac{\partial l_i}{\partial \mathbf{p}} = [\mathbf{t}_i^T \quad -\mathbf{t}_i^T \tilde{\mathbf{a}}_i^T \mathbf{H}] \quad (23)$$

where, respectively denoting $\cos x$ and $\sin x$ by c_x and s_x :

$$\mathbf{H} = \begin{bmatrix} 1 & 0 & s_\theta \\ 0 & c_\phi & -s_\phi c_\theta \\ 0 & s_\phi & c_\phi c_\theta \end{bmatrix} \quad (24)$$

Finally, by considering that:

$$\frac{\partial \mathbf{J}_i^T}{\partial \mathbf{p}} = \left[\frac{\partial \mathbf{t}_i}{\partial \mathbf{p}} \quad \frac{\partial \mathbf{a}_i'}{\partial \mathbf{p}} \right], \quad \frac{\partial \mathbf{W}}{\partial \mathbf{p}} = -mg \begin{bmatrix} \mathbf{0}_{3 \times 1} \\ \tilde{\mathbf{k}} \tilde{\mathbf{r}}^T \mathbf{H} \end{bmatrix} \quad (25)$$

and:

$$\frac{\partial \mathbf{t}_i}{\partial \mathbf{p}} = \mathbf{w}_i \sin \psi_i \frac{\partial \sigma_i}{\partial \mathbf{p}} + \mathbf{n}_i \frac{\partial \psi_i}{\partial \mathbf{p}}, \quad \frac{\partial \mathbf{a}_i'}{\partial \mathbf{p}} = [\mathbf{0}_{3 \times 3} \quad -\tilde{\mathbf{a}}_i^T \mathbf{H}] \quad (26)$$

$$\frac{\partial \psi_i}{\partial \mathbf{p}} = \left[\frac{\mathbf{n}_i^T}{\|\boldsymbol{\rho}_i\|} \quad -\frac{\mathbf{n}_i^T \tilde{\mathbf{a}}_i^T \mathbf{H}}{\|\boldsymbol{\rho}_i\|} \right] \quad (27)$$

$\partial \mathbf{F}_3/\partial \mathbf{p}$ can be evaluated according to the partition defined in Section 2.2 as:

$$\frac{\partial \mathbf{F}_3}{\partial \mathbf{p}} = \left(\frac{\partial \mathbf{J}_u^T}{\partial \mathbf{p}} - \mathbf{J}_u^T \mathbf{J}_a^{-T} \frac{\partial \mathbf{J}_a^T}{\partial \mathbf{p}} \right) \mathbf{J}_a^{-T} \mathbf{W}_a + \mathbf{J}_u^T \mathbf{J}_a^{-T} \frac{\partial \mathbf{W}_a}{\partial \mathbf{p}} - \frac{\partial \mathbf{W}_u}{\partial \mathbf{p}} \quad (28)$$

4 Data Acquisition Algorithm

It is beyond the scope of this work to determine an optimal data acquisition algorithm. However, a practical one, which enables autonomous and safe operation of the *CDPR* during calibration, is provided hereafter. For this aim, cable tensions or alternatively motor torques are assumed to be measurable or at least estimated, and actively controlled by a suitable feedback system.

In the instant the robot is switched on, its pose is generally unknown. It is possibly unsafe to start the self-calibration process in this configuration. Then, it is useful to pre-determine a safe start configuration, in which every cable is taut and sufficiently long, so that it can be coiled and uncoiled, and the e - e may attain different poses. By assigning a start cable tension vector \mathbf{T}_0 , the static problem (9) can be solved for \mathbf{p} as a non-linear system of six equations in six unknowns. Because of the non-linearity of the problem, a finite set of real solutions can be determined: this calculation may be done off-line and just once, i.e. during robot parameter calibration. Only stable solutions [4] among the possibly many available should be considered. Additionally, \mathbf{T}_0 may be selected so that only one stable solution exist.

In the following, we will consider a start cable tension vector leading to a unique stable solution of problem (9). Accordingly, a (computed) start pose $\mathbf{p}_{0,comp}$ is unambiguously determined, as well as start cable lengths \mathbf{l}_{comp}^0 and swivel angles σ_{comp}^0 . The real start pose \mathbf{p}_0 attained by the *CDPR* can be fairly different from the ideal one $\mathbf{p}_{0,comp}$, and its determination is the aim of the self-calibration procedure. A maximum cable tension vector \mathbf{T}_m should be set as well. The data acquisition algorithm objective is to ensure that every *DoF* of the e - e is varied during measurements, so that problem (21) is always well conditioned. The procedure workflow can be summarized as follows.

1. *Start phase*: command the *CDPR* so that cable tensions (or motor torques) quasi-statically reach the assigned value \mathbf{T}_0 . When \mathbf{T}_0 is reached and static conditions are attained³, the j -th actuator is assigned an incremental cable tension (or motor torque) set-point, starting from $j = 1$. The change in a single actuator set-point ensures that the pose of the end-effector is different at any iteration, thus being effective, as well as practical and easy to implement;
2. *Tensioning phase*: quasi-statically move the *CDPR* by assigning $\lambda/(2n)$ positive increments of magnitude $\Delta T = 2n(T_{j,m} - T_{j,0})/\lambda$ to the tension set-point of the j -th actuator, namely $T_{j,k} = T_{j,k-1} + \Delta T$, where $T_{j,0}$ is the j -th component of \mathbf{T}_0 . After each assignment k , the *CDPR* e - e could possibly oscillate during the transition. When static conditions are attained, record measurements $\Delta\sigma_{i,k}^*$ and $\Delta l_{i,k}^*$ for $i = 1, \dots, n$;
3. *Detensioning phase*: assign $\lambda/(2n)$ negative increments of magnitude ΔT to the tension set-point of the j -th actuator, namely $T_{j,k} = T_{j,k-1} - \Delta T$. When static conditions are attained, record measurements $\Delta\sigma_{i,k}^*$ and $\Delta l_{i,k}^*$ for $i = 1, \dots, n$. During the detensioning phase, the robot follows exactly the same cable tension (motor torques) set-points as in the tensioning phase: on a real machine, due to repeatability errors, this could lead to different cable lengths and swivel angles, which are possibly useful in the calibration procedure in order to minimize the repeatability error of the robot. λ/n measurement sets are thus obtained by varying a single actuator set-point;

³ Notice that cable tensions are only used to lead the platform to poses where the robot is stable and kinematic measures can be accurately performed. They have no role in the optimization problem solution, since they do not appear as variables in Eq. (21). They may be affected by appreciable errors without compromising the procedure, whereas platform stability plays a key role in the data acquisition process.

Table 1: Actuation unit properties

i	\mathbf{d}_i [m]	r_i [m]	${}^P\mathbf{a}'_i$ [m]	\mathbf{x}_i	\mathbf{y}_i	\mathbf{z}_i
1	$[-2.030 \ -0.170 \ 0.806]^T$	0.025	$[0.020 \ -0.287 \ 0.250]^T$	\mathbf{e}_y	$-\mathbf{e}_z$	$-\mathbf{e}_x$
2	$[0.066 \ 0.920 \ 0.757]^T$	0.025	$[0.251 \ 0.153 \ 0.250]^T$	$-\mathbf{e}_x$	$-\mathbf{e}_z$	$-\mathbf{e}_y$
3	$[-2.043 \ 2.241 \ 0.738]^T$	0.025	$[0.211 \ 0.153 \ 0.250]^T$	$-\mathbf{e}_y$	\mathbf{e}_z	$-\mathbf{e}_x$

4. *Increment phase:* $j = j + 1$; if $j \leq n$ then go to point 2, otherwise the algorithm is finished because λ measurement sets have been recorded.

The initial guess for the solution of problem (21) is computed as:

$$\mathbf{X}_{guess} = [\boldsymbol{\sigma}_{comp}^0; \mathbf{l}_{comp}^0; \mathbf{p}_{1,comp}; \cdots; \mathbf{p}_{\lambda,comp}] \quad (29)$$

where $\mathbf{p}_{k,comp}$, $k = 1, \dots, \lambda$, can be evaluated by solving the static problem (9) with assigned tension \mathbf{T}_k . Finally, by employing \mathbf{X}_{guess} , $\Delta\boldsymbol{\sigma}_k^* = [\Delta\sigma_{1,k}^* \cdots \Delta\sigma_{n,k}^*]^T$ and $\Delta\mathbf{l}_k^* = [\Delta l_{1,k}^* \cdots \Delta l_{n,k}^*]^T$ for $k = 1, \dots, \lambda$, it is possible to determine \mathbf{X}_{opt} as a solution of (21). Ideally, $\boldsymbol{\sigma}_{opt}^0$ and \mathbf{l}_{opt}^0 should converge to $\boldsymbol{\sigma}^0$ and \mathbf{l}^0 , respectively.

5 Simulations and Experimental Results

A simulation example, developed in MATLAB®, aims at testing the efficiency of the optimization routine as a function of λ and the different formulations of the Jacobian. Experimentation on a prototype shows the application of the method in a real-world scenario. The geometrical properties of a 3-cable 6-*DoF* under-actuated CDPR used for both simulation and experimentation are summarized in Table 1, where $\mathbf{e}_x = [1 \ 0 \ 0]^T$, $\mathbf{e}_y = [0 \ 1 \ 0]^T$ and $\mathbf{e}_z = [0 \ 0 \ 1]^T$ are elements of the canonical basis of $SO(3)$. The platform mass is $m = 8$ Kg, and ${}^P\mathbf{p}'_G = [0 \ 0 \ 0.182]^T$ m.

5.1 Simulation results

If the start tension vector $\mathbf{T}_0 = [40 \ 40 \ 40]^T$ N is assigned, the only stable solution of the static problem (9) is $\mathbf{p}_0 = [-1.363 \ 0.963 \ -0.460 \ -0.056 \ -0.069 \ -0.557]^T$ m, $\mathbf{l}^0 = [1.470 \ 1.509 \ 1.543]^T$ m, and $\boldsymbol{\sigma}^0 = [0.738 \ 0.607 \ -0.799]^T$ rad. Since the simulation is based on a perfect data acquisition process, the above (theoretical) values of \mathbf{p}_0 , \mathbf{l}^0 and $\boldsymbol{\sigma}^0$ are the expected output of the optimization algorithm.

According to the procedure proposed in Section 4, several simulations were performed with different values of λ , i.e. $\lambda = 12 \div 372$. The initial guess \mathbf{X}_{guess} for the optimization solver was generated by considering a perturbed start tension $\mathbf{T}_{0,pert} = [46.9 \ 23.9 \ 32.6]^T$ N. In this case, the only stable solution of the static problem (9) yields $\mathbf{p}_{0,comp} = [-1.648 \ 0.740 \ -0.732 \ -0.246 \ 0.179 \ -0.523]^T$ m,

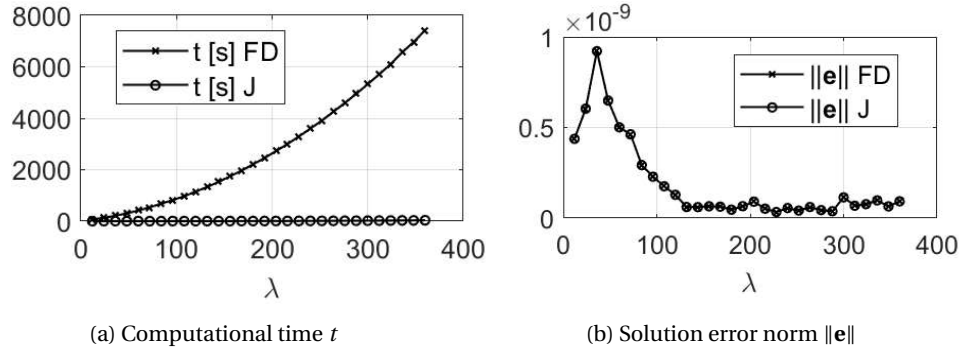


Fig. 3: Simulation results comparing FD and J formulations

$\mathbf{l}_{comp}^0 = [1.468 \ 1.914 \ 1.802]^T$ m, and $\boldsymbol{\sigma}_{comp}^0 = [0.926 \ 0.684 \ -0.849]^T$ rad. Furthermore, $\mathbf{T}_m = [80.0 \ 80.0 \ 80.0]^T$ N was set. Complete numerical data regarding \mathbf{X}_{guess} , for $k = 1, \dots, \lambda$, are omitted due to space limitations.

In the case of ideal measurements, a solution \mathbf{X}_{opt} to the problem (21) is always found that is not only a minimum, but a real numerical zero. Solutions were computed in Matlab by using the *lsqnonlin* solver. Figure 3 shows the computational time and the norm of the error $\mathbf{e} = \mathbf{p}_0 - \mathbf{p}_{0,opt}$ for a variable number λ of measurement sets, in the case a finite-difference estimation (FD) or an analytical formulation (J) of the Jacobian. It is clear that the analytical formulation is crucial for the algorithm time-performance, whereas there is no noticeable difference in the numerical precision achieved by the two numerical formulations. Simulations also show that there are no advantages in acquiring an increasing number of data points for the initial-pose estimation. The norm of error \mathbf{e} is consistent with the numerical tolerance.

5.2 Experimental results

The proposed data acquisition strategy and calibration method was tested on a prototype. Swivel angles were measured by 16-bit incremental encoders, mounted directly on the swivel axes of pulleys, whereas cable lengths were estimated by using 20-bit incremental encoders on each motor axis and a kinematic model of the winch. Swivel pulleys were manufactured by *FDM* technology, thus limited, but not negligible, errors in their geometry and elasticity exist. Cables were coiled on IPAnema winches [16]. Clearance and elasticity in the winch components, as well as cable elasticity itself, are possible sources of error in the estimation of cable lengths.

In order to measure the real pose of the platform during experiments, 8 VICON Motion Capture Systems cameras were employed to track the position of 4 markers mounted on the robot platform. The accuracy of the measure is ± 0.2 mm for each dimension of the marker (x, y, z) , according to manufacturer specifications. In the end, the position of the reference point and the platform orientation were reconstructed from the recorded position of each marker.

Table 2: Experiments results

i	\mathbf{p}_0 [mm, °]	$\mathbf{p}_{0,opt}$ [mm, °]	$\ \mathbf{e}_p\ $ [mm]	$\ \mathbf{e}_e\ $ [°]
1	$\begin{bmatrix} -1314 & 900 & -355 & -5.0 & -4.8 & -32.0 \end{bmatrix}^T$	$\begin{bmatrix} -1324 & 906 & -361 & -4.5 & -4.9 & -32.1 \end{bmatrix}^T$	13.4	0.5
2	$\begin{bmatrix} -1345 & 922 & -322 & -4.0 & -3.6 & -31.9 \end{bmatrix}^T$	$\begin{bmatrix} -1347 & 913 & -325 & -4.2 & -4.0 & -32.0 \end{bmatrix}^T$	9.9	0.4
3	$\begin{bmatrix} -1348 & 917 & 310 & -4.1 & -3.4 & -32.1 \end{bmatrix}^T$	$\begin{bmatrix} -1357 & 895 & -310 & -5.0 & -3.6 & -32.0 \end{bmatrix}^T$	23.4	0.9
4	$\begin{bmatrix} -1349 & 917 & -310 & -4.1 & -3.4 & -32.0 \end{bmatrix}^T$	$\begin{bmatrix} -1359 & 914 & -307 & -4.2 & -3.5 & -31.9 \end{bmatrix}^T$	11.5	0.2
5	$\begin{bmatrix} -1344 & 913 & -314 & -4.2 & -3.6 & -32.0 \end{bmatrix}^T$	$\begin{bmatrix} -1348 & 918 & -315 & -4.0 & -3.9 & -31.9 \end{bmatrix}^T$	5.7	0.4

Because of the lack of force sensors in the robot set-up, motor torques were employed instead of cable tensions for the implementation of the algorithm presented in Section 4. The start tension vector and maximum cable tensions were set to $\mathbf{T}_0 = [40.0 \ 40.0 \ 40.0]^T$ N and $\mathbf{T}_m = [80.0 \ 80.0 \ 80.0]^T$ N, respectively, and converted in motor torques according to static equilibrium of the cable transmissions. In the end, $\lambda = 60$ was chosen as a trade-off between accuracy of the initial-pose estimation and data-acquisition speed.

The results of five experiments are reported in Table 2, where \mathbf{p}_0 is the real starting pose, as measured by the motion tracking system, $\mathbf{p}_{0,opt}$ is the estimated starting pose resulting from the solution of the problem (21), $\|\mathbf{e}_p\| = \|\mathbf{p}_0 - \mathbf{p}_{0,opt}\|$ is the reference position error norm and $\|\mathbf{e}_e\| = \|\mathbf{e}_0 - \mathbf{e}_{0,opt}\|$ is the norm of the error of the orientation parameters. Positions are expressed in millimeters and angles in degrees. The execution of the calibration procedure required, on average, 4 min for the data acquisition procedure, and 2.5 s for the initial-pose estimation by using the analytical formulation of the Jacobian (16 min by using a finite-difference estimation).

During experiments, it was observed that the orientation of the swivel pulley axes plays a crucial role for the conditioning of problem (21). Pulley orientations were set in order to achieve the best possible results with the robot architecture at hand, but are not optimal. Nonetheless, the results are satisfactory by considering the modelling simplification and the hardware at hand.

6 Conclusions

This paper presented an automatic self-calibration method for suspended under-actuated *CDPRs*, extending the method proposed in [8]. An analytical formulation of the problem was developed and an autonomous procedure to calibrate the initial-pose of the *CDPR* by means of incremental measurements of cable lengths and swivel angles was shown. Experimental results on a prototype show that the application of the proposed method is promising, but it needs refining in order to achieve a higher accuracy. In particular, the optimal orientation of the swivel pulleys and the effect of uncertainties in the measurements will be investigated in the future.

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