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# Experimental comparison of velocity estimators for a control moment gyroscope inverted pendulum

Dmitry Sokolov  
Université de Lorraine, CNRS, Inria, LORIA  
F-54000 Nancy, France  
dmitry.sokolov@univ-lorraine.fr

Alexander Gusev  
Kuban State University  
Krasnodar, Russia  
gusev@ftf.kubsu.ru

Stanislav Aranovskiy  
Equipe Automatique, CentaleSupélec — IETR  
Cesson-Sévigné, France  
stanislav.aranovskiy@centralesupelec.fr

Igor Ryadchikov  
Kuban State University  
Krasnodar, Russia  
ryadchikov@kubsu.ru

**Abstract**—We consider the problem of velocity estimation for a control moment gyroscope inverted pendulum. To this end, we consider model-free differentiator, a model-based linear observer and a model-based nonlinear differentiator. The proposed designs are implemented in hardware and the closed-loop system performance in the stabilization task is compared. Moreover, we show that the considered system cannot be partially linearized via a change of coordinates, and thus is not suitable for a recently reported class of nonlinear observers.

**Index Terms**—velocity estimation, differentiator, inverted pendulum, control moment gyroscope

## I. Introduction

The research problem of this paper is motivated by the walking robot we are currently developing in the Laboratory of Robotics and Mechatronics of the Kuban State University (refer to Figure 1, left). This non-anthropomorphic robot has an auxiliary dynamic stabilization system which consists of two scissored pairs of control moment gyroscopes (CMG). The scissored pairs are orthogonal and thus the problem of vertical stabilization of the robot can be considered for each axis separately. Therefore, stabilization of the robot for one axis can be approximated with a simplified one-dimensional prototype. In this paper we consider such a prototype, which is a control moment gyroscope inverted pendulum (Figure 1, middle). Note that the robot has a modular design: the biped is equipped with four identical CMG cubes.

Control moment gyroscope is a widely used technological device that uses the reaction of a spinning wheel to external torques. Due to the advantages of a large ratio of produced torque to control torque and relatively low power consumption, CMGs have a wide range of applications, including vessel stabilisation [1], motorcycle and robot balancing [2], balancing aid for humans and

bipedal exoskeletons [3], [4], attitude steering system for the satellites [5] and underwater vehicles [6].

The key element for the stabilization of an inverted pendulum is velocity estimation. Note that our robot uses multiple accelerometers to estimate its tilt angles [7], and we rely on soft sensors for velocity estimation.

Velocity estimation for a mechanical system is a well-known problem, see, for example, the recent work by Aranovskiy et al. [8] and the references therein. In practice, a common solution is to consider this problem for each degree of freedom separately rather than to estimate all velocities with a single observer. From the signal processing point of view, this approach can be considered as numerical differentiation, where velocity estimation is seen as online differentiation of a measured position signal, e.g., a first-order difference used in [9]. While differentiator-based velocity observers can be designed model-free, a better performance is typically obtained when observers use (at least partially) available model knowledge: sliding-mode exact differentiators first proposed by Levant in [10], high-gain differentiators as described by Vasiljevic and Khalil in [11], and differentiators proposed by Perruquetti et al. [12] that ensure finite-time convergence and robustness with respect to measurement noises and uncertainties. In this paper, we aim at practical comparison of some of the discussed observers.

The contribution of this paper is two-fold: first, we give a rigorous proof that, despite its simplicity, the mechanical system under consideration does not belong to the class of recently reported systems [8] which allow a construction of model-based nonlinear observers. Next, we propose a comparison of three velocity observers, namely a model-free differentiator, a model-based linear observer and a model-based nonlinear differentiator. All three observers are tested on the hardware we have built for this purpose, and the experimental results are provided.

The rest of the paper is organized as follows. In section II we present a model of the considered system. Next, in

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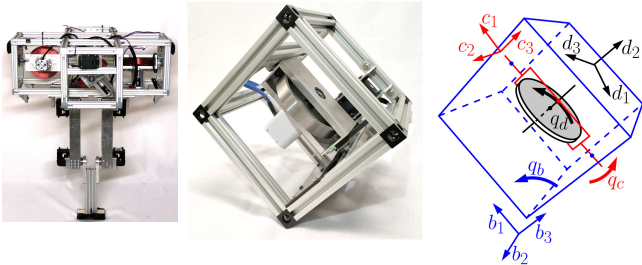


Fig. 1: Left: We are developing a biped that uses four control moment gyroscopes (highlighted in red) as an auxiliary stabilization system. Middle and right: 1D pendulum hardware and corresponding notations. This configuration corresponds to  $q_b = -\pi/4$  and  $q_c = \pi/2$ .

section III we present the state-feedback controller capable to stabilize the system if all states (including velocities) are measured. Then, in section IV we discuss three velocity observers. Hardware experiments and observers comparison are provided in section V. Finally, possible further research directions are discussed in the concluding section VI.

## II. Model Description

The considered inverted pendulum is shown in Figure 1. In this paper we follow the notations from the manual of the model 750 control moment gyroscope commercialized by Educational Control Products company [13]. The notations and the corresponding hardware parameters are summarized in the Table I. The pendulum consists of three bodies: the main body  $B$ , the gimbal  $C$ , and the wheel  $D$ . We associate a frame with each of the bodies:  $\{O, \vec{b}_1, \vec{b}_2, \vec{b}_3\}$ ,  $\{O, \vec{c}_1, \vec{c}_2, \vec{c}_3\}$ , and  $\{O, \vec{d}_1, \vec{d}_2, \vec{d}_3\}$ , respectively. We assume that all the bodies are symmetric, and the centers of mass of all the bodies coincide at the point  $O$ . Due to the symmetry, the inertia matrices are diagonal. We denote the principal moments of inertia (w.r.t. the center of mass) of the bodies  $B$ ,  $C$  and  $D$  as  $\text{diag}(I_b, J_b, K_b)$ ,  $\text{diag}(I_c, J_c, K_c)$  and  $\text{diag}(I_d, J_d, K_d)$ , respectively.

The angle of the body  $B$  with respect to the vertical is denoted as  $q_b$ , the angle of the body  $C$  with respect to the body  $B$  is denoted as  $q_c$ , and the angle of the body  $D$  with respect to the body  $C$  is denoted as  $q_d$ . The configuration shown in Figure 1 corresponds to the angles  $q_b = -\pi/4$  and  $q_c = \pi/2$ . Note that the equilibrium position of an actual robot depends on the configuration of the legs and may be subject to external disturbances; therefore, for our cube we model the equilibrium point as  $q_b = -\pi/4 - e$ , where  $e$  is the unknown (small) bias.

The corresponding time derivatives are denoted as  $\omega_b(t) := \dot{q}_b(t)$ ,  $\omega_c(t) := \dot{q}_c(t)$ ,  $\omega_d(t) := \dot{q}_d(t)$ . If we apply torques  $\tau_c$  and  $\tau_d$  to the bodies  $C$  and  $D$ , respectively,

TABLE I: Hardware parameters

Description	Symbol	Value
Total mass, kg	$m$	2.62
Center of mass to pivot distance, m	$l$	0.13
Moments of inertia, $\text{kg}\cdot\text{m}^2$ :		
of the body $B$	$[I_b, J_b, K_b]$	$[10 \ 13 \ 13] \cdot 10^{-3}$
of the body $C$	$[I_c, J_c, K_c]$	$[10 \ 2.6 \ 9.9] \cdot 10^{-4}$
of the body $D$	$[I_d, J_d, K_d]$	$[5.6 \ 11 \ 5.6] \cdot 10^{-4}$
Disk $D$ velocity, rad/s	$\omega_d$	314
Equilibrium position bias, rad	$e$	unknown

we can find the Euler–Lagrange equations:

$$\begin{aligned}
 0 &= (J_1 + J_2 \cos^2 q_c) \dot{\omega}_b - J_2 \sin(2q_c) \omega_c \omega_b \\
 &\quad + J_d \dot{\omega}_d \cos q_c - J_d \sin(q_c) \omega_c \omega_d \\
 &\quad - mlg \sin\left(q_b + \frac{\pi}{4} + e\right), \\
 \tau_c &= (I_c + I_d) \dot{\omega}_c + J_d \omega_b \omega_d \sin q_c + \frac{1}{2} J_2 \sin(2q_c) \omega_b^2, \\
 \tau_d &= J_d \dot{\omega}_d + J_d \cos(q_c) \dot{\omega}_b - J_d \sin(q_c) \omega_c \omega_b,
 \end{aligned} \tag{1}$$

where  $J_1 = I_d + J_b + K_c + ml^2$ ,  $J_2 = J_c - I_d + J_d - K_c$ . In this expression we use the rotational symmetry  $K_d = I_d$  of the disk  $D$ . For control moment gyroscope systems, the nominal operation mode assumes  $|\omega_d| \gg \max(|\omega_b|, |\omega_c|)$ , and regulation of the velocity  $\omega_d$  is performed by the means of a local motor controller. Assuming that this controller provides fast and accurate velocity regulation ensuring  $\dot{\omega}_d \approx 0$ , we will further assume that  $\omega_d$  is constant and equals to the nominal velocity, see Table I.

Moreover, in our hardware the gimbal  $C$  is controlled by the means of a servo drive that ensures velocity tracking. In this case, the velocity  $\omega_c$  can be considered as an input signal. Under these assumptions the above system can be rewritten as

$$\begin{aligned}
 \dot{q}_b &= \omega_b, \\
 \dot{\omega}_b &= \frac{\omega_c (J_d \omega_d \sin q_c + J_2 \omega_b \sin(2q_c))}{J_1 + J_2 \cos^2 q_c} \\
 &\quad + \frac{mlg \sin\left(q_b + \frac{\pi}{4} + e\right)}{J_1 + J_2 \cos^2 q_c},
 \end{aligned} \tag{2}$$

## III. Linearization-based stabilization

For the system (2), the desired equilibrium is defined as

$$\Omega_0 := \left\{ q_b = -\frac{\pi}{4} - e, \omega_b = 0, q_c = \frac{\pi}{2} \right\}.$$

In what follows we say that a control law (locally) stabilizes the system (2) if under this control law the point  $\Omega_0$  is (locally) attractive.

To proceed, it is convenient to define a new state variable as a deviation of the actual position from the desired equilibrium,  $x := [q_b \ \omega_b \ q_c]^\top - \Omega_0$ . Then the system (2) can be rewritten as

$$\dot{x} = f(x, u) = \begin{bmatrix} x_2 \\ f_2(x, u) \\ u \end{bmatrix}, \tag{3}$$

where  $u = \omega_c$  and

$$f_2(x, u) = \frac{u(J_d \omega_d \cos x_3 - J_2 x_2 \sin(2x_3)) + mgl \sin x_1}{J_1 + J_2 \sin^2 x_3}.$$

The state variable  $x_3$  can be computed through the measurements of the signal  $q_c$ ; however, since the offset  $e$  is not known, the signal  $x_1$  can not be computed. Thus, we define the vector of measurements as

$$y = \begin{bmatrix} q_b + \frac{\pi}{4} \\ q_c - \frac{\pi}{2} \end{bmatrix} = \begin{bmatrix} x_1 - e \\ x_3 \end{bmatrix}. \quad (4)$$

Then the control goal is to find a control law that stabilizes (3) at the origin using the measurements  $y$ .

A common practice to stabilize a (sufficiently well-behaved) nonlinear system is to linearize the system around the desired equilibrium. For the system (3) such equilibrium is given by  $x = 0$ ,  $u = 0$ . Let us define

$$A := \frac{\partial f}{\partial x}(0, 0) = \begin{bmatrix} 0 & 1 & 0 \\ \frac{mgl}{J_1} & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}, \quad (5)$$

$$B := \frac{\partial f}{\partial u}(0, 0) = \begin{bmatrix} 0 \\ \frac{J_d \omega_d}{J_1} \\ 1 \end{bmatrix}$$

Then the linearization of (3) around the origin is given by  $\dot{x} = Ax + Bu$ .

It is tempting to use the state-feedback static control

$$u := -K [y_1 \quad x_2 \quad y_2] = -Kx - k_1 e, \quad (6)$$

where  $K := [k_1 \quad k_2 \quad k_3]$  is the gain vector. The problem, however, is that the equilibrium point would be  $(A - BK)^{-1} Bk_1 e = \begin{bmatrix} 0 & 0 & -\frac{k_1}{k_3} \end{bmatrix}^\top e$ .

Therefore, the stabilization goal  $|x| \rightarrow 0$  is not achieved under the control law (6). In order to overcome the nonzero steady-state body  $C$  angle problem, we add an integral action. To this end, we introduce an auxiliary variable  $x_e$  defined as  $\dot{x}_e := 0 - x_3$ , where zero stays as the reference for  $x_3$ . Then the extended state-space model is

$$\begin{bmatrix} \dot{x} \\ \dot{x}_e \end{bmatrix} = \underbrace{\begin{bmatrix} A & | & 0_{3 \times 1} \\ \hline 0 & 0 & -1 & | & 0 \end{bmatrix}}_{A_e} \begin{bmatrix} x \\ x_e \end{bmatrix} + \underbrace{\begin{bmatrix} B \\ 0 \end{bmatrix}}_{B_e} u.$$

The pair  $A_e$ ,  $B_e$  is controllable and we can design the extended control law

$$u := -K_e [y_1 \quad x_2 \quad y_2 \quad x_e]^\top = -K_e [x^\top \quad x_e]^\top - k_{e,1} e, \quad (7)$$

where  $K_e \in \mathbb{R}^{1 \times 4}$ . Then the closed-loop dynamics is

$$\begin{bmatrix} \dot{x} \\ \dot{x}_e \end{bmatrix} = (A_e - B_e K_e) \begin{bmatrix} x \\ x_e \end{bmatrix} - B_e k_{e,1} e,$$

and the equilibrium is

$$(A_e - B_e K_e)^{-1} B_e k_{e,1} e = \begin{bmatrix} 0 & 0 & 0 & -\frac{k_{e,1}}{k_{e,4}} \end{bmatrix}^\top e.$$

Thus, the state  $x$  converges to zero, while the integral action  $x_e$  ensures the equilibrium offset compensation.

However, to implement the control law (7), it is required to estimate the velocity  $\omega_b$ . In the next section we discuss possible velocity observers for the considered system.

#### IV. Observers design

A model-based nonlinear observer has been recently proposed in [8] for a class of mechanical systems that are partially linearizable via coordinate changes (PLvCC). The observer can be applied to the mechanical system (1) if it admits a change of coordinates allowing to rewrite the system in such a form that the dynamics is linear in momenta. Then a globally converging exponential momenta observer can be constructed that yields velocity estimation. Unfortunately, despite its simplicity, the considered system does not belong to this class; this claim is rigorously proven in the Appendix. In this section, we present three designs that are suitable for the considered system, namely a linear model-free differentiator, a linear Luenberger's observer, and a nonlinear model-based differentiator.

##### A. Finite differences

The simplest way to get the velocity estimation is to use finite differences, however, it is well known that differentiation can be noisy at high frequencies. To this end, a common engineering practice for the velocity estimation is to use a low pass filter together with the differentiator. This can be used to reduce the consequences of noise in the signal but care is needed to ensure that the phase lag does not distort the results. For a 2nd order filter with a time constant  $\tau$ , the continuous-time transfer function of the model-free differentiator can be written as  $G(s) = \frac{s}{(\tau s + 1)^2}$ , yielding the following state-space realization

$$\begin{aligned} \dot{z}_1 &= z_2, \\ \dot{z}_2 &= -\frac{1}{\tau^2} z_1 - \frac{2}{\tau} z_2 + \frac{1}{\tau^2} y_1, \\ \hat{x}_2^{ld} &= z_2, \end{aligned} \quad (8)$$

where  $\hat{x}_2^{ld}$  is the estimate of  $x_2$  provided by the differentiator.

##### B. A full-order linear state observer

A full-state model-based linear observer is constructed as a Luenberger's observer for the linearization of the model dynamics at the desired equilibrium:

$$\dot{\hat{x}} = A\hat{x} + Bu + L(y - C\hat{x}), \quad \hat{x}_2^{lo} = \hat{x}_2, \quad (9)$$

where  $\hat{x}_2^{lo}$  is the estimate of  $x_2$  provided by the linear observer, the vector of measurements  $y$  is defined in (4), matrices  $A$  and  $B$  are defined in (5), and

$$C = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix}.$$

Define the estimation error as  $\tilde{x} := x - \hat{x}$ . Then in the absence of the bias, i.e., when  $e = 0$ , the error dynamics becomes  $\dot{\tilde{x}} = (A - LC)\tilde{x}$ . The gain matrix  $L$  is chosen such that the matrix  $A - LC$  is Hurwitz. For example, it can be done by pole placement, or as a solution of an optimal estimation problem, e.g., Kalman filter. Then, the asymptotic convergence of  $\tilde{x}$  to zero is ensured.

For the case  $e \neq 0$  we have  $y = Cx + \begin{bmatrix} 1 \\ 0 \end{bmatrix} e = Cx + C_e e$  and  $\dot{\tilde{x}} = (A - LC)\tilde{x} - LC_e e$ . Thus, the steady state value of the velocity estimation will differ from zero due to the bias  $e$ . However, it does not compromise the closed-loop stabilization. Indeed, with the observer, the control action (7) becomes  $u = -K_e [\hat{x}^\top \ x_e]^\top = -K_e [x^\top \ x_e]^\top + K_e [\tilde{x}^\top \ 0]^\top$ .

Define  $\bar{x} := [x^\top \ x_e]^\top$ . The closed-loop dynamics obeys

$$\begin{bmatrix} \dot{\tilde{x}} \\ \dot{\bar{x}} \end{bmatrix} = \begin{bmatrix} A_e - B_e K_e & B_e K_e \begin{bmatrix} I_{3 \times 3} \\ 0_{1 \times 3} \end{bmatrix} \\ 0_{3 \times 4} & A - LC \end{bmatrix} \begin{bmatrix} \tilde{x} \\ \bar{x} \end{bmatrix} + \begin{bmatrix} 0_{4 \times 1} \\ LC_e \end{bmatrix} e.$$

Then is straightforward to verify that the equilibrium of the closed-loop system satisfies  $x = 0$ , i.e., the integral action compensates the offset being used in the loop with the state observer even if the observer has a steady-state estimation error.

### C. Homogeneous finite-time differentiator

Following Perruquetti et al. [14], the model-based homogeneous differentiator for the states  $x_1, x_2$  of the system (3) is constructed as

$$\begin{aligned} \dot{\hat{x}}_1 &= \hat{x}_2 - k_1 [e_b]^\alpha, \\ \dot{\hat{x}}_2 &= \frac{u(J_d \omega_d \cos y_2 - J_2 \hat{x}_2 \sin(2y_2)) + mgl \sin y_1}{J_1 + J_2 \sin^2 y_2} - k_2 [e_b]^{2\alpha-1}, \\ \hat{x}_2^{hd} &= \hat{x}_2, \end{aligned} \quad (10)$$

where  $\hat{x}_2^{hd}$  is the estimate of  $x_2$  provided by the homogeneous observer,  $e_b = \hat{x}_1 - y_1$  and  $[e_b]^\alpha = |e_b|^\alpha \text{sign}(e_b)$ . In [14] it is shown that if  $k_1$  and  $k_2$  are such that the polynomial  $s^2 + k_2 s + k_1$  is Hurwitz and  $\alpha \in (\frac{1}{2}, 1]$ , then the estimation error  $\hat{x} - x$  converges to a vicinity of the origin. More precisely, convergence to the vicinity instead of the finite-time convergence to the origin follows from the replacement of  $x_2$  and  $\sin(x_1)$  in  $f_2(x, u)$  in (3) with  $\hat{x}_2$  and  $\sin(y_1) = \sin(x_1 + e)$ , respectively. A more detailed analysis of the size of this vicinity can be performed by the means of Lyapunov function analysis in a similar way as in [15]; however, such a result is rather technical and is not presented here for brevity.

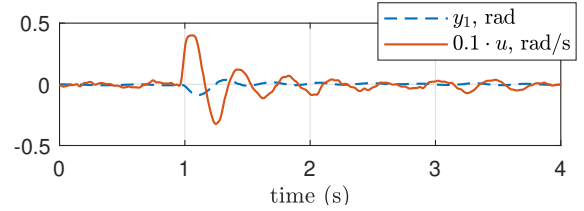
## V. Experiments and comparison

The hardware for the tests<sup>1</sup> (shown in Figure 1, middle) is assembled from off-the-shelf components. The hardware parameters are summarized in the Table I. A STM32F746

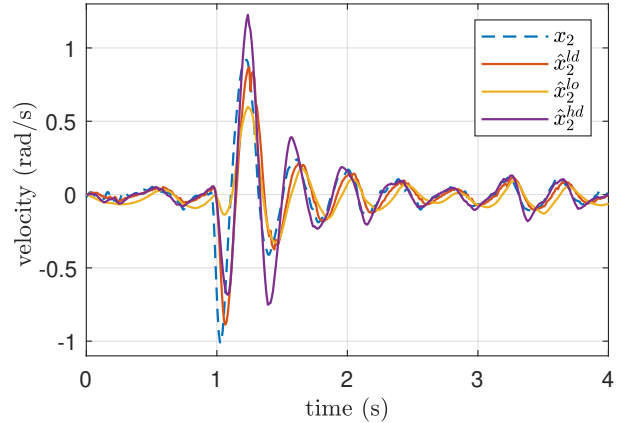
<sup>1</sup>We have filmed all the experiments, the video is available here: <https://youtu.be/0xFanQ0QaEk>.

TABLE II: Controller parameters used in experiments.

Description	Symbol	Value
LQR gains in (7)	$K_e$	[35, 4, -1, 0.3]
Time constant in (8)	$\tau$	0.02
Observer gains in (9)	$L$	[[20,0],[150,0],[0,20]]
Parameters in (10)	$[k_1, k_2, \alpha]$	[20, 150, 0.85]



(a) Angle measurement  $y_1$  and corresponding control  $u$



(b) Velocity estimation tuning

Fig. 2: Observers tuning using ground truth measurements of  $x_2$ .

discovery board was chosen as the main computing unit. We have chosen a small brushless motor to drive the wheel  $D$ , the frame  $C$  is actuated by a Dynamixel MX106-R servo motor. The robot we are currently developing (Figure 1, left) uses multiple accelerometers to estimate its tilt angles as was proposed in [7], and we rely on soft sensors for velocities estimation. In the case of the 1D pendulum, we use two accelerometers to measure  $y_1$ , and we have installed a fiber optic gyroscope to have the ground truth while comparing the soft sensors.

First of all, since the additional hardware is available, we have implemented the control law (7). Figure 2(a) provides the angle measurements  $y_1$  and the corresponding control signal  $u$ . Note that after one second of the experiment an external force was applied for a short period of time. Then we have tuned all three soft sensors to fit the best the measured signal  $x_2$ . Estimated velocities are provided in Figure 2(b). Table II summarizes the control gains as well as the parameters of the soft sensors.

Then we have performed three experiments, replacing the signal  $x_2$  in the control law (7) by each of the soft sensors we have implemented. The results provided in Figures 3, 4 and 5 correspond to the velocity estimators (8),

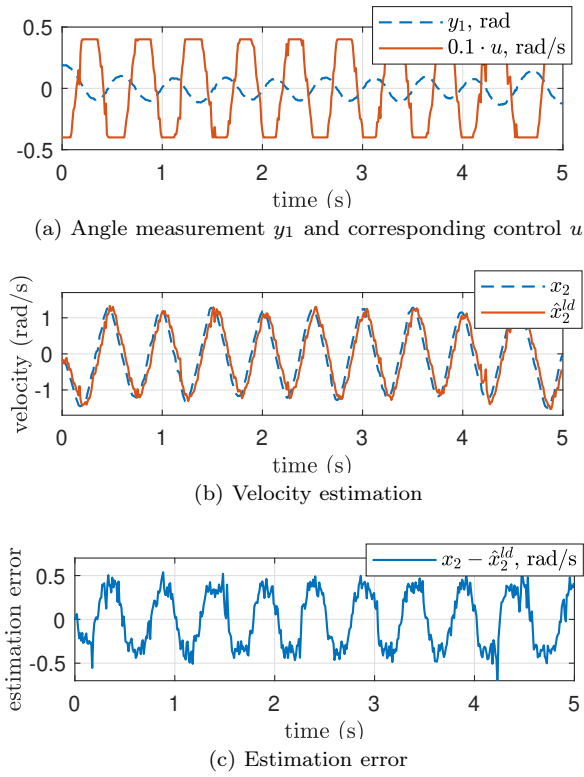


Fig. 3: Closed-loop stabilization using observer (8).

(9) and (10), respectively.

It is easy to see that the non-linear differentiator (10) offers the best behavior. The finite differences introduce an inherent lag into the estimation process, and the system enters into sustained oscillations (Figure 3). A similar behavior can be witnessed (Figure 4) for the observer (9). In this case, the oscillations are due to the fact that the linearization does not reflect well the behavior of the system. In particular, this observer ignores completely the signal  $y_2$ ; and thus it is not robust w.r.t external disturbances. An illustration is available in Figure 2(b), where at time step  $t \approx 1$ s the linear observer fails completely to estimate the signal  $x_2$  under a sudden application of an external force.

## VI. Conclusion

We have considered the velocity estimation problem for the control moment gyroscope inverted pendulum case study. Three different velocity observers, namely the linear model-free differentiator, the linear model-based observer, and the nonlinear model-based differentiator, have been implemented in the hardware and experimentally compared in the pendulum stabilization task. The experimental studies illustrate that the designs that utilize (at least partial) model knowledge outperform the model-free differentiator. Moreover, the nonlinear model-based design provides smaller error than the linear one.

At a further research direction, we intend to apply the designed nonlinear differentiator for the biped system

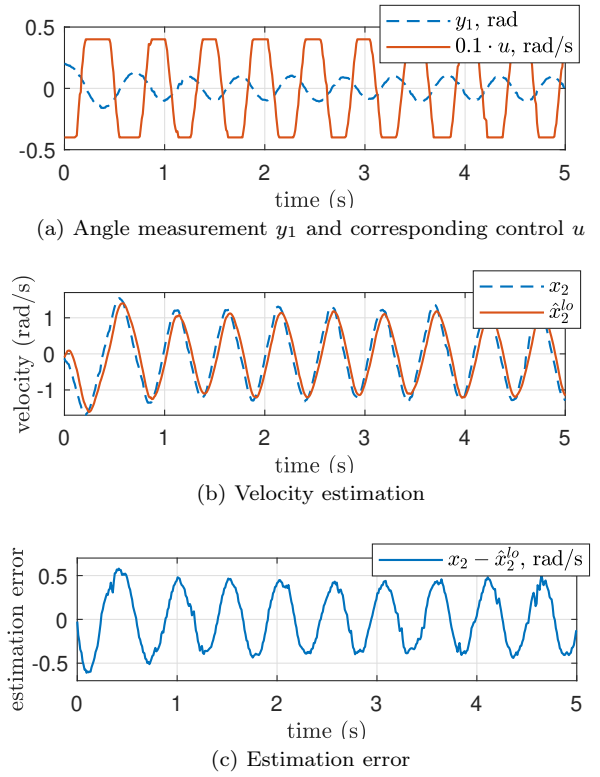


Fig. 4: Closed-loop stabilization using observer (9).

described in Introduction, Fig. 1. At this step, we also intend to incorporate a friction model into the dynamics of the model-based velocity estimator to reduce the modeling errors in the system.

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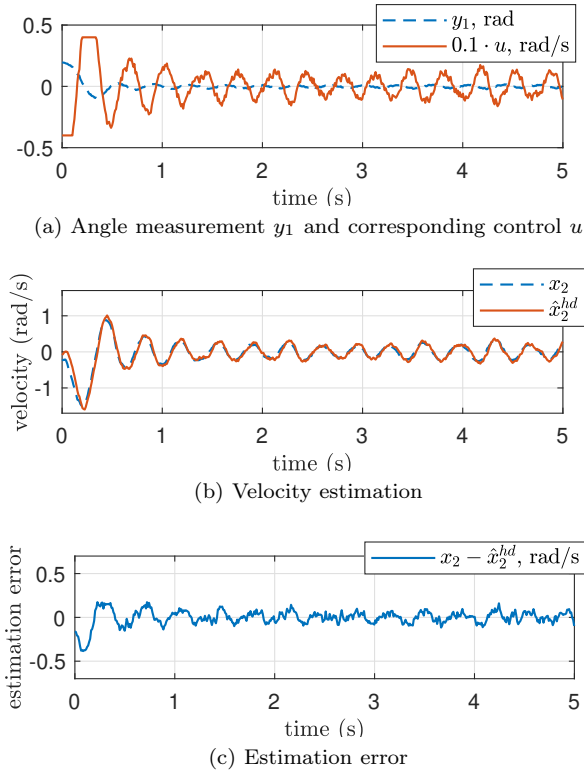


Fig. 5: Closed-loop stabilization using observer (10).

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## Appendix

In [16] it is proven that a mechanical system with inertia matrix  $M$  and  $n$  degrees of freedom is partially linearizable via a change of coordinates (PLvCC) if there exists a full-

rank matrix  $\Psi : \mathbb{R}^n \rightarrow \mathbb{R}^{n \times n}$  such that for all  $i = 1, \dots, n$  the matrices  $\mathcal{B}_{(i)}$  are skew-symmetric, where

$$\mathcal{B}_{(i)} := \sum_{j=1}^n \left\{ [\Psi_i, \Psi_j] \Psi_j^\top (M \Psi \Psi^\top)^{-1} + \frac{1}{2} \Psi_{ji} \Psi \frac{\partial}{\partial q_j} (\Psi^\top M \Psi)^{-1} \Psi^\top \right\}.$$

Here  $\Psi_i$  is the  $i$ -th column of  $\Psi$ ,  $\Psi_{ij}$  is the element of  $\Psi$  with the indices  $i$  and  $j$ , and  $[\Psi_i, \Psi_j] = \frac{\partial \Psi_i}{\partial q} \Psi_j - \frac{\partial \Psi_j}{\partial q} \Psi_i$  is the Lie bracket.

Assuming that regulation of the velocity  $\omega_d$  is performed by the means of a local motor controller and  $\dot{\omega}_d \approx 0$ , the system (1) can be written in the standard mechanical system form as  $M(q)\ddot{q} + C(q, \dot{q})\dot{q} + G(q) = \tau$ , where the inertia matrix is  $M(q) = \begin{bmatrix} m_1(q_2) & 0 \\ 0 & 1 \end{bmatrix}$ , with  $m_1(q_2) := \frac{1}{I_c + I_d} (J_1 + J_2 \cos^2(q_2))$ . Since the PLvCC property depends on the inertia matrix only, we are not writing down other terms.

In our case we define  $\Psi := \begin{bmatrix} a & b \\ c & d \end{bmatrix}$ , where  $a, b, c$ , and  $d$  are the functions of  $q$  to be found. Then we obtain

$$[\Psi_1, \Psi_2] = \begin{bmatrix} a \frac{\partial b}{\partial q_1} - b \frac{\partial a}{\partial q_1} + c \frac{\partial b}{\partial q_2} - d \frac{\partial a}{\partial q_2} \\ a \frac{\partial d}{\partial q_1} - b \frac{\partial c}{\partial q_1} + c \frac{\partial d}{\partial q_2} - d \frac{\partial c}{\partial q_2} \end{bmatrix},$$

$$[\Psi_2, \Psi_1] = -[\Psi_1, \Psi_2], \quad [\Psi_1, \Psi_1] = [\Psi_2, \Psi_2] = 0,$$

To satisfy the PLvCC property, the matrices  $\mathcal{B}_{(1)}$  and  $\mathcal{B}_{(2)}$  must be skew-symmetric. The equation  $\mathcal{B}_{(2)2,2} = -\frac{\partial d}{\partial q_2} = 0$  dictates that  $d$  does not depend on  $q_2$ , i.e., it is a function of  $q_1$  only. Now let us focus on the following subsystem:

$$\begin{cases} \mathcal{B}_{(2)1,1} = \frac{1}{2m_1^2} \left( -2m_1 \frac{\partial b}{\partial q_1} - d \frac{\partial m_1}{\partial q_2} \right) = 0 \\ \mathcal{B}_{(2)1,2} + \mathcal{B}_{(2)2,1} = -\frac{1}{m_1} \left( \frac{\partial d}{\partial q_1} + m_1 \frac{\partial b}{\partial q_2} \right) = 0. \end{cases}$$

Since  $m_1(q_2) > 0$  for all  $q_2$ , we have:

$$\begin{cases} \frac{\partial b(q_1, q_2)}{\partial q_1} = -\frac{d(q_1)}{2m_1(q_2)} \frac{\partial m_1(q_2)}{\partial q_2} \\ \frac{\partial b(q_1, q_2)}{\partial q_2} = -\frac{1}{m_1(q_2)} \frac{\partial d(q_1)}{\partial q_1}. \end{cases}$$

The trivial solution is  $d = 0$  with  $b = b_0$ , but it leads to a singular matrix  $\Psi$ ; let us check if the system has non-trivial solutions. We can differentiate both equations:

$$\begin{cases} \frac{\partial}{\partial q_2} \frac{\partial}{\partial q_1} b(q_1, q_2) = -\frac{d(q_1)}{2} \frac{\partial}{\partial q_2} \left( \frac{1}{m_1(q_2)} \frac{\partial m_1(q_2)}{\partial q_2} \right) \\ \frac{\partial}{\partial q_1} \frac{\partial}{\partial q_2} b(q_1, q_2) = -\frac{1}{m_1(q_2)} \frac{\partial^2 d(q_1)}{\partial q_1^2}. \end{cases}$$

The symmetry of second derivatives leads to:

$$\underbrace{-\frac{d(q_1)}{2}}_{\text{depends on } q_1} \underbrace{\frac{\partial}{\partial q_2} \left( \frac{1}{m_1(q_2)} \frac{\partial m_1(q_2)}{\partial q_2} \right)}_{\text{depends on } q_2} = \underbrace{-\frac{1}{m_1(q_2)}}_{\text{depends on } q_2} \underbrace{\frac{\partial^2 d(q_1)}{\partial q_1^2}}_{\text{depends on } q_1}.$$

Therefore, it leads us to the condition

$$m_1(q_2) \cdot \frac{\partial}{\partial q_2} \left( \frac{1}{m_1(q_2)} \frac{\partial m_1(q_2)}{\partial q_2} \right) = \text{constant}.$$

Since  $m_1(q_2)$  is a known function, it is easy to verify that this condition does not hold, and therefore the above system does not admit any (non-trivial) solution. Thus we conclude that this mechanical system is not PLvCC.