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Rami Albasha, Christian Fournier, Christophe Pradal, Michaël Chelle, Jorge Alejandro Prieto, et al.. HydroShoot: a functional-structural plant model for simulating hydraulic structure, gas and energy exchange dynamics of complex plant canopies under water deficit - application to grapevine (*Vitisvinifera* L.). *in silico Plants*, 2019, 1 (1), 10.1093/insilicoplants/diz007 . hal-02253260

**HAL Id: hal-02253260**

**<https://inria.hal.science/hal-02253260v1>**

Submitted on 1 Aug 2019

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# HydroShoot: a functional-structural plant model for simulating hydraulic structure, gas and energy exchange dynamics of complex plant canopies under water deficit - application to grapevine (*Vitis vinifera* L.)

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# Abstract

This paper presents HydroShoot, a leaf-based functional-structural plant model (FSPM) that simulates gas-exchange rates of complex plant canopies under water deficit conditions. HydroShoot is built assuming that simulating both the hydraulic structure of the shoot together with the energy budget of individual leaves is the asset for successfully scaling-up leaf to canopy gas-exchange rates. HydroShoot includes three interacting modules: *hydraulic* which calculates the distribution of xylem water potential across shoot hydraulic segments, *energy* which calculates the complete energy budget of individual leaves, and *exchange* which calculates net carbon assimilation and transpiration rates of individual leaves. HydroShoot was evaluated on virtual and real grapevines having strongly contrasted canopies, under well-watered and water deficit conditions. It captured accurately the impact of canopy architecture and soil water status on plant-scale gas-exchange rates and leaf-scale temperature and water potential. Both shoot hydraulic structure and leaf energy budget simulations were, as postulated, required to adequately scaling-up leaf to canopy gas-exchange rates. Notwithstanding, simulating shoot hydraulic structure was found more necessary to adequately performing this scaling task than simulating leaf energy budget. That is, the intra-canopy variability of leaf water potential was a better predictor of the reduction of whole plant gas-exchange rates under water deficit than the intra-canopy variability of leaf temperature. We conclude that simulating the shoot hydraulic structure is a prerequisite if FSPM's are to be used to assess gas-exchange rates of complex plant canopies as those of grapevines. Finally, HydroShoot is available through the OpenAlea platform (<https://github.com/openalea/hydroshoot>) as a set of reusable modules.

## Keywords:

Functional-structural plant model (FSPM), grapevine (*Vitis vinifera* L.), water deficit, hydraulic structure, energy budget, gas-exchange

# Introduction

Climate change is seriously challenging viticulture sustainability in its current areas of production (Hannah *et al.*, 2013; van Leeuwen *et al.*, 2013; Duchêne *et al.*, 2014). One efficient short-term solution for hampering the projected adverse effects of water and heat stress on viticulture, is to reconsider training systems so that they allow maximizing the ratio of carbon assimilation ( $A_{n,plant}$ ) to water loss by transpiration ( $E_{plant}$ ) whilst maintaining optimal leaf temperature conditions (Medrano *et al.*, 2012; Duchêne *et al.*, 2014; Palliotti *et al.*, 2014). However, training systems present a wealth of possibilities (Reynolds and Vanden Heuvel, 2009) that cannot be compared experimentally. Therefore, the design of canopy structures that are adapted to adverse environmental conditions is most efficiently performed with the aid of models able to accurately predict the influence of canopy architecture on its gas exchange rates and leaves temperature under combined water and heat stress. That is what functional-structural plant models (FSPMs) offer (Vos *et al.*, 2010).

FSPMs received nevertheless little attention in grapevine scientific literature to assess the impact of shoot architecture on plant gas-exchange rates (Medrano *et al.*, 2015 a). This is probably due to the inherent complexity in scaling up eco-physiological processes from the leaf to the canopy level, as strong variability in gas exchange rates (CO<sub>2</sub> versus water vapor) exists inside the canopy driven by variations in micrometeorological conditions and leaf functional traits (Niinemets *et al.*, 2014; Medrano *et al.*, 2015 b). This scaling-up task is even more complex under water deficit conditions, as stomatal aperture is likely to reduce under water deficit in a non-uniform pattern across the canopy (e.g. Gonzalez-Dugo *et al.*, 2012; Ngao *et al.*, 2017) further distorting intra-canopy gas-exchange and leaf temperature variability (Reynolds and Vanden Heuvel, 2009). Bauerle *et al.* (2007) indicated that disregarding this variability may lead to strongly overestimate the predicted whole canopy daily transpiration flux, up to 25% greater than observed values as they found on a study on Red Maple (*Acer rubrum* L.)

Hence, adequately predicting the intra-canopy variability of both leaf stomatal conductance and temperature stands out as the key challenge to using FSPMs to predict plant gas-exchange rates under water deficit conditions. Yet, the remaining question is how this variability can be accurately described and what are their main determinants.

Describing the intra-canopy variability of both leaf stomatal conductance and temperature requires from the one hand to explicitly describe their drivers as a function of leaf position inside the canopy, and from the other hand to adequately account for their mutual interactions (how stomatal aperture affects leaf energy budget and *vice versa*) (Chelle, 2005). The main drivers for both processes are commonly determined as incident shortwave irradiance, air temperature, air humidity and leaf “water status” which determines stomatal closure (Damour *et al.*, 2010). Among these drivers, leaf water status (which controls stomatal aperture and consequently both leaf transpiration and temperature) still makes no consensus in the scientific literature when it comes to determining what it refers to. A basal approach considers that leaf water status is equal to the soil water status (e.g. Misson *et al.*, 2004; van Wijk *et al.*, 2000), considering that the “remote” action of available water in



and photosynthesis rates by scaling-up these processes from the leaf-level. This model uses as lever for this scaling process the simulation of the interactions between hydraulic structure of the shoot, the energy balance, and gas-exchange rates of individual leaves. The second objective is to evaluate the performance of the model using both virtual and real canopies with data collected on photosynthesis and transpiration rates (plant scale), and stomatal conductance and temperature (leaf scale). Finally, the third objective is to examine how detailed hydraulic structure and energy budget simulations determine the predicted gas-exchange rates at the plant scale under water deficit conditions.

## Materials and methods

### Model structure and basic assumptions

HydroShoot is a static FSPM (with regards to plant structure) that takes plant shoot architecture, weather, and soil water conditions as inputs, and returns transpiration and net photosynthesis rates both of individual leaves and the whole plant at hourly time steps as outputs. It is conceived as a set of three modules which simulate water potential (*hydraulic* module), energy budget (*energy* module), and  $C_3$ -type gas-exchange rates (*exchange* module). These three modules run jointly, having leaf xylem water potential and temperature at the leaf level as pivots (cf. [implementation and numerical solution](#) section). The formalisms used in each module are developed in the following sections.

#### *Hydraulic* module

The *hydraulic* module computes water potentials of plant segments (output of the module) as a function of water flow in the plant and water potential of the soil (input to the module). The whole plant is compartmentalized in elementary conducting elements corresponding to petioles, internodes of the current-year stems, and elements of previous-year trunk and branches (internodes or pruning complexes). Leaves are treated in this system as nodes letting water flow but having no gradient in their water potential ( $\Psi_{leaf}$ ).

**Figure 1:** (a) Illustration of the parameters required to calculate the hydraulic structure:  $F$ , rate of water flow [ $kg\ s^{-1}$ ],  $K$ , hydraulic conductivity per unit length of the conducting element [ $kg\ s^{-1}\ m\ MPa^{-1}$ ],  $L$ , length of the conducting element [ $m$ ] and  $H_u$  and  $H_l$  are respectively water potentials at upper (downstream) and lower (upstream) extremities of the conducting element [ $MPa$ ]; and (b) the schematic representation of the electrical analog.

Water transfer across the hydraulic segments is simulated by analogy to Ohm's law in electrical circuits (Figure 1). Each segment is characterized by its length ( $L, m$ ) and hydraulic conductivity ( $K, kg s^{-1} m MPa^{-1}$ ), and is crossed by a water flux ( $F, kg s^{-1}$ ) which, together with conductivity modifies water head at its upper (downstream,  $H_u$ ) and lower (upstream,  $H_l$ ) extremities [MPa]:

$$F_i = -K_i \frac{H_{u,i} - H_{l,i}}{L_i} = -K_i \frac{\Psi_{u,i} - \Psi_{l,i} + \rho g(z_{u,i} - z_{l,i})}{L_i} \quad (\text{Eq. 1})$$

where  $i$  denotes the segment identifier,  $\Psi_{u,i}$  and  $\Psi_{l,i}$  are respectively xylem water potential at the upper and lower extremities,  $z_{u,i}$  and  $z_{l,i}$  are elevations of upper and lower extremities [m], respectively,  $\rho$  is water density [ $kg m^{-3}$ ] and  $g$  is the gravitational acceleration [ $m s^{-2}$ ].

Xylem conductivity varies with water potential as a result of xylem cavitation under water deficit (Tyree and Sperry, 1989). This relationship is described using a sigmoidal function:

$$K_i = K_{max,i} \frac{1}{1 + \left( \frac{\Psi_i}{\Psi_{icrit,stem}} \right)^{c_{x1}}} \quad (\text{Eq. 2})$$

where  $K_{max,i}$  is the maximum segment conductivity [ $kg s^{-1} m MPa^{-1}$ ],  $\Psi_i$  is the arithmetic mean of water potential values of the segment  $i$  ( $\frac{\Psi_{u,i} + \Psi_{l,i}}{2}$ ),  $\Psi_{icrit,stem}$  [MPa] and  $c_{x1}$  [-] are shape parameters.  $K_{max,i}$  is estimated empirically as proposed by Tyree and Zimmermann (2002):

$$K_{max,i} = c_{x2} D_i^{c_{x3}} \quad (\text{Eq. 3})$$

where  $D_i$  is segment average diameter [m] and  $c_{x2}$  and  $c_{x3}$  are dimensionless shape parameters, mostly given within the ranges of [2.5, 2.8] and [2.0, 5.0], respectively (Tyree and Zimmermann, 2002).

Equations 1 to 3 apply to all conducting segments (not leaves blades). Water potential of the upper extremity of the petiole is assumed equal to that of the lumped leaf water potential  $\Psi_{leaf}$ .

### Exchange module

The *exchange* module computes the rates of net carbon assimilation and transpiration per unit surface area (respectively  $A_n$  and  $E$ ) for each individual leaf as a function of micrometeorological

conditions and leaf water status. The calculations use the analytical solution proposed by **Yin *et al.* (2009)** for coupling the  $C_3$  photosynthesis model of **Farquhar *et al.* (1980)** to the stomatal conductance model of **Ball *et al.* (1987)**. This coupling allows stomatal conductance (to both  $CO_2$  and water vapor) to respond to environmental stimuli (temperature and irradiance) via photosynthesis [see Supporting Information S2]. It is based on Fick's first law of diffusion, whereby  $A_n$ , the stomatal conductance to  $CO_2$  ( $g_{s,CO_2}$ ), and the mesophyll conductance ( $g_m$ ) are used. However, as Farquhar's model has been thoroughly detailed in literature, its description is given in Appendix I. The focus of this section is given instead to the stomatal conductance formulae which are a key element in this work.

$g_{s,CO_2}$  is calculated according to **Yin *et al.* (2009)** as:

$$g_{s,CO_2} = g_{s0,CO_2} + m_0 \frac{A_n + R_d}{(C_c - \Gamma)} f_w \quad (\text{Eq. 4})$$

where  $g_{s0,CO_2}$  is the residual stomatal conductance to  $CO_2$  [ $mol_{CO_2} m^{-2} s^{-1}$ ],  $R_d$  is mitochondrial respiration in the light [ $\mu mol_{CO_2} m^{-2} s^{-1}$ ],  $\Gamma$  is  $CO_2$  compensation point in the absence of mitochondrial respiration [ $\mu mol_{CO_2} mol_{CO_2}^{-1}$ ],  $m_0$  is a dimensionless shape parameter, and  $f_w$  is a dimensionless function representing the response of  $g_{s,CO_2}$  to air water vapor deficit (VPD,  $kPa$ ).  $f_w$  is deduced from the stomatal conductance model of **Leuning (1995)** as:

$$f_w = \frac{1}{\left(1 + \frac{VPD}{D_0}\right)} \quad (\text{Eq. 5a})$$

where  $D_0$  is a scaling parameter [ $kPa$ ].

Eq. 5a does not account for stomatal sensitivity to soil water deficit ("remote" approach) or local leaf water potential ("local" approach). **Tuzet *et al.* (2003)** and **Leuning *et al.* (2004)** suggested to express  $f_w$  as a function of the local  $\Psi_{leaf}$ . This function is implemented in HydroShoot following **Nikolov (1995)**:

$$f_w = \frac{1}{\left(1 + \left(\frac{\Psi_{leaf}}{\Psi_{crit,leaf}}\right)^n\right)} \quad (\text{Eq. 5b})$$



where  $\Psi_{crit,leaf}$  is a critical leaf water potential threshold [MPa] at which stomatal conductance is reduced by 50%, and  $n$  is a shape parameter [-]. The same last equation is used to express the dependency of  $g_{s0,CO_2}$  on the remote soil water potential ( $\Psi_{soil}$ ):

$$f_w = \frac{1}{\left(1 + \left(\frac{\Psi_{soil}}{\Psi_{crit,leaf}}\right)^n\right)} \quad (\text{Eq. 5c})$$

The transpiration rate  $E$  [ $mol_{H_2O} m^{-2} s^{-1}$ ] is calculated as:

$$E = \frac{1}{\frac{1}{g_{b,H_2O}} + \frac{1}{1.6 g_{s,CO_2}}} \left(\frac{VPD}{P_a}\right) \quad (\text{Eq. 6})$$

where  $P_a$  is the atmospheric pressure [MPa] and  $g_{b,H_2O}$  is the boundary layer conductance to water vapor [ $mol_{H_2O} m^{-2} s^{-1}$ ], derived from **Nobel (2005)** as:

$$g_{b,H_2O} = \frac{D_{H_2O}(t) P_v}{R T \Delta x} \quad (\text{Eq. 7})$$

with

$$D_{H_2O}(t) = D_{H_2O} \frac{P_a}{P_v} \left(\frac{T}{273}\right)^{1.8} \quad (\text{Eq. 8})$$

where  $D_{H_2O}$  is the diffusion coefficient of H<sub>2</sub>O in the air at 0 °C ( $2.13 \cdot 10^{-5} m^2 s^{-1}$ ),  $P_a$  is the ambient air pressure at 0 °C temperature [MPa],  $P_v$  is water vapor partial pressure [MPa], and  $\Delta x$  is the thickness of the boundary layer [m] which is defined as (**Nobel 2005**):

$$\Delta x = 0.004 \sqrt{\frac{l}{v}} \quad (\text{Eq. 9})$$

where  $l$  is the mean length of the leaf in the downwind direction [m], set to 70% of blade length, and  $v$  is the ambient wind speed [ $m s^{-1}$ ].

Finally, mesophyll conductance to CO<sub>2</sub> is assumed to simply depend on bulk leaf temperature (**Evers et al., 2010**) following an Arrhenius equation trend (as for photosynthetic parameters, cf. Eq. A8) with a basal value at 25 °C set to  $0.1025 [mol_{CO_2} m^{-2} s^{-1}]$ .

## Intra-canopy variability in photosynthetic capacity

Leaf photosynthetic traits (maximum carboxylation rate  $V_{cmax}$ , maximum electron transport rate  $J_{max}$ , triose-phosphate transport rate TPU and  $R_d$ ; cf. [Appendix I](#)) have been shown to strongly vary within the plant canopy so that to increase light-saturated net assimilation rate with increasing solar irradiance availability throughout the canopy (**Niinemets *et al.*, 2014**). HydroShoot accounts for this variability by considering leaf nitrogen content per unit leaf surface area ( $N_a$ ,  $g_N m^{-2}$ ) as the pivotal trait to determine the photosynthetic capacity of leaves (**Prieto *et al.*, 2012**) as follows:

$$P^{25} = S_{N_a} N_a - b_{N_a} \quad (\text{Eq. 10})$$

where  $P^{25}$  is the value at 25 °C for any of the rates  $V_{cmax}$ ,  $J_{max}$ , TPU and  $R_d$  (given as inputs), and  $S_{N_a}$  [ $\mu mol_{CO_2} g_N^{-1} s^{-1}$ ] and  $b_{N_a}$  [ $\mu mol_{CO_2} m^{-2} s^{-1}$ ] are the slope and the intercept of the linear relationship with  $N_a$  specific to each rate.  $N_a$  is calculated as the product of nitrogen content per unit leaf dry mass  $N_m$  [ $g_N g_{drymatter}^{-1}$ ] and leaf dry mass per area LMA [ $g_{drymatter} m^{-2}$ ].  $N_m$  linearly varies with plant age, expressed as the thermal time cumulated from budburst (input of the model), and LMA is determined by leaf exposure to light during the last past days (**Prieto *et al.*, 2012**). This is expressed respectively in the two following equations:

$$N_m = a_N \sum_{i=budburst}^d (\max(0, T_{air,i} - T_b)) + b_N \quad (\text{Eq. 11})$$

$$LMA = a_M \ln(PPFD_{10}) + b_M \quad (\text{Eq. 12})$$

where  $T_{air,i}$  is the mean temperature of the day  $i$  [°C] and  $T_b$  is the base temperature (minimum required for growth) [°C], set to 10°C for grapevine and used for the calculation of thermal time since budburst,  $a_N$  [ $g_N g_{drymatter}^{-1} °C d^{-1}$ ] and  $b_N$  [ $g_N g_{drymatter}^{-1}$ ] are the slope and intercept of the linear relationship between  $N_m$  and accumulated thermal time since budburst,  $PPFD_{10}$  [ $mol_{photon} m^{-2} d^{-1}$ ] is the cumulative photosynthetic photon flux density irradiance intercepted by the leaf (output of the energy module) averaged over the past 10 days,  $a_M$  [ $g_{drymatter} m^{-2}$ ] and  $b_M$  [ $g_{drymatter} m^{-2}$ ] are the slope and intercept of the linear relationship between LMA and the logarithm of  $PPFD_{10}$ .



It is noteworthy that only the forced convective heat transfer is currently considered in HydroShoot since forced convection dominates free convection once wind speed exceeds roughly  $0.1 \text{ m s}^{-1}$  (Nobel 2005). This wind speed threshold is generally exceeded during diurnal hours. However, under low wind conditions heat transfer may be underestimated.

Since the resolution of the last equation is highly time-consuming, we assumed the energy gain from the neighbouring leaves through thermal longwave as a lumped term whereby average leaf temperature  $T_{leaves}$  is considered instead of individual leaves (Dauzat *et al.*, 2001). In this case, the lumped form factor  $\sum_{j \in \Omega} F_{ij}$  is simply taken as  $1 - (k_{sky} + k_{soil})$  (that is the solid angle where neither the sky nor the soil are seen by a single leaf). The former equation becomes:

$$0 = \alpha_{iR_g} \Phi_{iR_g} + \varepsilon_{ileaf} \sigma (k_{isky} \varepsilon_{sky} T_{sky}^4 + k_{isoil} \varepsilon_{soil} T_{soil}^4 + [1 - (k_{sky} + k_{soil})] T_{leaves}^4) - 2 \varepsilon_{ileaf} \sigma T_i^4 - \lambda E_i - 2K_{air} \frac{(T_i - T_{air})}{\Delta x_i} \quad (\text{Eq. 14})$$

## Implementation and numerical resolution

HydroShoot is developed using the *Python* programming language (Python Software Foundation <http://www.python.org>) in the OpenAlea platform (Pradal *et al.*, 2008; Pradal *et al.*, 2015). The code of the model can be freely accessed through its public depository (<https://github.com/openalea/hydroshoot>). It uses the Multiscale Tree Graph (MTG) method (Godin and Caraglio, 1998; Balduzzi *et al.*, 2017) as a central data-structure in order to allow indirect communication between the different models which favours modularity (Fournier *et al.*, 2010; Garin *et al.*, 2014). Each process has been implemented as a reusable component in OpenAlea and can be reused independently in other models and composed in various ways, provided that the other models are written in the *Python* language and provide the adequate inputs.

The resolution of HydroShoot equations is performed by an iterative procedure that is schematized in [Figure 2](#).

**Figure 2:** Schematic representation of the numerical resolution of HydroShoot. Meteorological inputs that are common to all leaves are air temperature ( $T_{air}$ , K), air relative humidity (RH, –), air CO<sub>2</sub> concentration [ $\mu\text{mol mol}^{-1}$ ], wind speed ( $u$ ,  $\text{m s}^{-1}$ ), and atmospheric pressure ( $Pa$ ,  $kPa$ ). Inputs per individual leaves are

the absorbed photosynthetic photon flux density (PPFD,  $\mu\text{mol m}^{-2} \text{s}^{-1}$ ) and  $\text{PPFD}_{10}$  the absorbed PPFD during the last 10 days.  $\Psi_u$  is xylem water potential at the nodes between each pair of stem elements [MPa].  $\Psi_{uinit}$  is initial  $\Psi_u$  [MPa].  $\Psi_{soil}$  is soil water potential.  $T_i$  is leaf temperature [K].  $T_{iinit}$  is initial  $T_i$  [K].  $K_{init}$  [ $\text{kgs}^{-1} \text{m MPa}^{-1}$ ] is initial hydraulic conductivity of each segment,  $\epsilon_x$  is the maximum allowable error of the estimation of xylem water potential [MPa] and  $\epsilon_T$  is the maximum allowable error of the estimation of leaf temperature [K]. Circles inside module boxes indicate internal iteration loops. Symbols between curly brackets represent spatially structured variables.

Iterations have three levels. The first is in the *hydraulic* module and concerns calculating xylem water potential of plant segments in interaction with their hydraulic conductivity (interdependent processes, cf. equations 1 and 2). The second level is between the *exchange* and *hydraulic* modules in order to calculate jointly gas-exchanges rates and leaf water potential values (transpiration affects the hydraulic structure Eq. 1 while the latter affects stomatal aperture Eq. 5b). The third level is between the *energy* module and both *exchange* and *hydraulic* modules, so that at each time new transpiration fluxes are calculated, leaf temperature values are updated, and the new temperature values are used to update gas-exchange rates which in their turn impose new xylem water potential distribution. The details on the numerical resolution are given in [Appendix III](#).

## Coupling with irradiance and soil models

HydroShoot needs irradiance absorption by individual leaves and soil water potential as inputs. It is therefore coupled in this work to Caribu irradiance model (**Chelle and Andrieu, 1998**) and to a simple soil water-budget model in order to calculate respectively irradiance absorption (PPFD) and soil water potential ( $\Psi_{soil}$ ) values on an hourly basis ([Figure 3](#)).

The *soil* module links transpired water rates to the transpirable soil water volume (TSW) in order to predict the hourly variations in  $\Psi_{soil}$ . At the beginning of each calculation step, transpired water volume from the previous step is withdrawn from the TSW. The soil volumetric water content  $\theta_{soil}$  is then determined by dividing TSW by the effective soil porosity.  $\Psi_{soil}$  is then obtained from  $\theta_{soil}$  from the water retention curve (**van Genuchten, 1980**) and used as an input for the *hydraulic* module. This procedure is referred to as the *Root-Shoot loop* in [Figure 3](#).

**Figure 3:** Flowchart of the modelling frame used in this application example. Meteorological inputs that are common to all leaves are air temperature ( $T_{air}$ , K), air relative humidity (RH, —), air CO<sub>2</sub> concentration [ $\mu\text{mol mol}^{-1}$ ], wind speed ( $u$ ,  $\text{m s}^{-1}$ ), and atmospheric pressure ( $P_a$ , kPa). Inputs per individual leaves are

the absorbed photosynthetic photon flux density (PPFD,  $\mu\text{mol m}^{-2} \text{s}^{-1}$ ) and  $\text{PPFD}_{10}$  the absorbed PPFD during the last 10 days.  $\Psi_{u,init}$  is the initial xylem water potential at the nodes between each pair of stem elements [ $\text{MPa}$ ].  $\Psi_{soil}$  is soil water potential.  $T_{i,init}$  is initial temperature of individual leaves [ $\text{K}$ ].  $K_{init}$  [ $\text{kg s}^{-1} \text{m MPa}^{-1}$ ] is initial hydraulic conductivity of each segment. Symbols between curly brackets represent spatially structured variables. *architecture*, *CARIBU* (Chelle and Andrieu, 1998) and *soil* are external modules used to simulate canopy architecture, irradiance interception, and soil water potential, respectively.

## Model evaluation

Model evaluation was performed in three steps. Firstly, the coherence between expected and simulated gas-exchange, temperature, and xylem water potential dynamics for different canopy architectures was assessed. Secondly, the precision was assessed by comparing model outputs to measured plant gas-exchange rates and leaf stomatal conductance, water potential and temperature. Finally, the required complexity level was evaluated, whereby we sought at determining whether simulating the hydraulic structure and energy balance were (both) required in order to obtain accurate predictions of gas-exchange rates at the plant scale. For all the following simulations, parameter values are given in Appendix IV.

## Coherence

HydroShoot was run on 3 virtual grapevine canopies which share the same soil type, soil initial water content, weather conditions, and total leaf area, and differ only in their shoot architecture (Figure 4). The objective was to examine whether the model reflects the differences of shoot architecture on gas and energy exchange rates as may be expected. For instance, whether higher photosynthesis and transpiration rates are obtained for canopies absorbing higher solar irradiance flux densities. Similarly, whether higher transpiration rates trigger steeper drops in leaf water potential.

The 3 canopies were trained on three different training systems: Vertical Shoot Positioning (VSP), Geneva Double Curtain (GDC) and Lyre systems (Figure 4a). All canopies had the same leaf area ( $5.7 \text{ m}^2$ ), internode diameter distribution (Figure 4b), planting density (inter-and intra-row spacing of 3.6 and 1.0 m respectively), soil type (Sand Loam) and initial collar water potential ( $-0.6 \text{ MPa}$ ).

The simulations were run using weather data extracted from the database of the weather station of the National Institute for Agricultural Research (INRA) in Montpellier ( $3^{\circ}53' \text{ E}$ ,  $43^{\circ}37' \text{ N}$ , 44 m alt) on July 29<sup>th</sup>, 2009 (DOY 210). Weather conditions corresponded to a warm day having minimum and maximum air temperature of 19 and 34 °C respectively, relative humidity oscillating

between 32 and 44%, wind speed at 2 m height going from 0 to 2  $ms^{-1}$ , and a clear sky with a maximum PPFD of 1670  $\mu mol m^{-2} s^{-1}$  at solar midday.

**Figure 4:** Mock-ups of three virtual grapevine canopies trained respectively to Vertical Shoot Positioning (VSP), Geneva Double Curtain (GDC) and Lyre systems. (a) Canopies mock-ups, (b) conducting segments (primary and secondary internodes, petioles) diameters distribution, and (c) cumulative leaf area with height.

## Precision

The precision of simulated outputs was evaluated by running HydroShoot on real canopies using collected data from experiments conducted in 2009 and 2012 on grapevine (cv. Syrah, grafted on SO4) at INRA, in Montpellier (same above-mentioned station). Five grapevines trained with two contrasting training systems were considered (cf. [Figure 5](#)): GDC in 2009 and VSP in 2012. Grapevine rows were oriented 140° from North on a shallow sandy loam soil with a low water holding capacity. Inter-row spacing was 3.6 m for GDC and 1.8 m for VSP. Intra-row spacing was 1 m [see Supporting Information S4].

Data on VSP grapevines (2009) were collected during a period of 4 days under well-watered and water deficit conditions. Water deficit was created by cutting off the irrigation system on the first day of the experiment (July 29<sup>th</sup>). Whole plant transpiration  $E_{plant}$  and net assimilation  $A_{n,plant}$  were monitored using open portable gas-exchange chambers (**Perez Peña and Tarara, 2004**). Temperature of individual leaves were monitored using thermocouples inserted into the primary veins of 10 fully developed individual leaves positioned on different heights from the top of the canopy to the inside, so that temperature gradient resulting from different irradiance conditions was captured.

Data on GDC grapevines (2012) were also collected during a 4 days experiment (starting on August 1<sup>st</sup>), but only under water deficit conditions. Only  $E_{plant}$  rate was monitored by measurements of sap flow installed on the two cordons of the GDC plants. Stomatal conductance and leaf water potential measurements were performed for a number of leaves on GDC grapevines during the experiment, but the exact position of leaves was not reported with measurements.

For both VSP and GDC grapevines, shoot architecture was constructed based on digitisation data, using a grapevine-specific shoot architecture module following a Multiscale Tree Graph (MTG) approach (**Godin and Caraglio, 1998; Pradal et al., 2008; Balduzzi et al., 2017**), in which organs topological connections and geometry were associated to shoot architecture ([Figure 5](#)). Plant mock-ups were produced so that the simulated vertical and horizontal profiles of leaf surface area fitted those observed.

**Figure 5:** 3D mockups of grapevines plants trained to Vertical Shoot Positioning system (VSP, a and b) under water deficit (VSP<sub>WD</sub>), well water conditions (VSP<sub>WW</sub>) and Geneva Double Curtain (GDC, c, d and e). The mockups were reconstructed from measured leaf surface profiles using the *architecture* module (input to HydroShoot). Numbers below canopies indicate leaf area per cordon [ $m^2$ ].

## Complexity

In order to explore the contribution of HydroShoot's *hydraulic* and *energy* modules components to the final simulation output, a sensitivity analysis was performed by plugging/unplugging each of these components and observing the resulting difference on simulated outputs. This procedure aims *in fine* at evaluating whether adding complexity to an FSPM would improve its performance in predicting gas-exchange dynamics at the plant-scale. The following simulation combinations are used:

- λ sim0: the reference (complete) version of HydroShoot having the ensemble of its components;
- λ sim1: stomatal conductance varies with VPD (as described by **Leuning, 1995** in [Eq. 5a](#)) regardless of leaf water potential;
- λ sim2: the hydraulic structure is disregarded (water potential of all leaves is forced equal to water potential at the collar) and stomatal conductance varies with collar water potential [Eq. 5c](#);
- λ sim3: energy balance is disregarded, that is all leaves have the same temperature as that of the air;
- λ sim4: the same case of sim1 but using tighter control of VPD on stomatal conductance ( $D_0$  in [Eq. 5a](#) is set to 1 instead of 30 as proposed by **Prieto et al. (2012)**).

## Evaluation criteria

The overall adequacy between observed and simulated variables was assessed based on the estimation of the mean bias error (MBE) and root mean square error (RMSE):

$$MBE = \frac{\sum_{i=1}^{n_{obs}} (y_{sim,i} - y_{obs,i})}{n_{obs}} \quad (\text{Eq. 15})$$

$$RMSE = \sqrt{\frac{\sum_{i=1}^{n_{obs}} (y_{sim,i} - y_{obs,i})^2}{n_{obs}}} \quad (\text{Eq. 16})$$



where  $y_{sim}$  and  $y_{obs}$  are respectively simulated and observed variables values and  $n_{obs}$  is the number of observations.

## Results and discussion

### Outputs coherence

Simulation outputs for virtual canopies are illustrated in [Figure 6](#) (plant-scale outputs) and [Figures 7](#) and [8](#) (leaf-scale outputs).

**Figure 6:** Simulation of absorbed irradiance (a), net carbon assimilation (b), temperature (c) and transpiration (d) at the plant-scale for three contrasted grapevine canopies (VSP, GDC and Lyre);  $T_{air}$  is air temperature. Temperature curves in (c) trace the hourly values of the median of leaves temperatures.

The simulations at the plant scale ([Figure 6](#)) show that GDC canopies had the highest absorbed irradiance rates, followed by Lyre and VSP canopies ([Figure 6a](#)), reflecting the higher exposure to solar irradiance using the GDC system. This trend was reflected on carbon assimilation ([Figure 6b](#)), temperature ([Figure 6c](#)), and transpiration ([Figure 6d](#)), whereby highest values were obtained for GDC then Lyre followed by VSP canopies.

Midday depression in  $A_{n,plant}$  was simulated for the three canopies proportionally to the absorbed irradiance, that is, highest for GDC and lowest for VSP ([Figure 6b](#)). The higher transpiration rates of GDC led to simulate lower leaf water potential values ([Figure 7](#)) around midday, which, combined with higher absorbed irradiance, led also to higher leaf temperatures ([Figure 8](#)). The combined effects of lower leaf water potential and higher temperature in GDC led to simulate a higher effect of midday depression in  $A_{n,plant}$  compared to Lyre and VSP canopies as may be expected.

**Figure 7:** Snapshot at solar midday (14:00hs) of water potential distribution across the shoot (left column) and only for leaves (boxplots, right column) for three contrasted grapevine canopies (VSP, GDC and Lyre).

**Figure 8:** Snapshot at solar midday of individual leaf temperature values (left column) and leaf temperature distribution (boxplots, right column) for three contrasted grapevine canopies (VSP, GDC and Lyre).

This first illustrative example on virtual canopies shows that the effect of canopy architecture on its gas-exchange and temperature behaviour is captured in HydroShoot. The comparison to measurements in the following section will show how the observed dynamics on both plant and leaf scales are accurately reproduced using HydroShoot for two real canopies.

## Comparison to observed data

### Leaf-scale

Simulation results at the leaf-scale are shown in Figures 9, 10 and 11, respectively for water potential, stomatal conductance, and temperature. The dynamics of these variables were adequately reproduced but with some discrepancies regarding the onset timing of the effect of water deficit.

Figures 9 and 10 show that the simulated  $\Psi_{leaf}$  and  $g_{s,H_2O}$  of the three GDC canopies decreased progressively as the soil water deficit increased, consistently with observations, but with an earlier onset of water stress which is probably due to inadequate parametrization either of the response function of  $g_{s,H_2O}$  to  $\Psi_{leaf}$  (cf. Eq. 5b) or of the soil hydrodynamic model (cf. Coupling with irradiance and soil models). Upon the onset of water stress, when water deficit was still mild in the first day (date 01 08 in Figure 10), HydroShoot simulated higher  $g_{s,H_2O}$  for sunlit leaves than for shaded leaves. Later, as water deficit increased, this trend was inverted, whereby sunlit leaves had the lowest  $g_{s,H_2O}$  rates (dates Aug 2<sup>nd</sup> and Aug 3<sup>rd</sup> in Figure 10). This inversion was due to a lower  $\Psi_{leaf}$  for sunlit leaves as a consequence of higher potential transpiration withdrawal per unit leaf surface area (cf. Eq. 1).

Moreover, Figure 10 shows that, by the end of the water deficit period (day Aug 3<sup>rd</sup>), leaf position had merely no more effect on its water vapor conductance  $g_{s,H_2O}$ . At this stage, water potential of all leaves reached low values at which stomata were almost closed. This uniformization of stomatal closure through the canopy is consistent with the observations reported by Escalona *et al.* (2003, 2016). Both studies reported a progressive homogenization of gas-exchange rates of grapevine leaves (cv. Tempranillo, Manto Negro and Grenache) as soil water deficit increased. Ngao *et al.* (2017) reported similar results on apple trees (*Malus pumila* Mill.), showing that intra-canopy variability in  $g_{s,H_2O}$  decreased significantly under the effect of soil water deficit.

**Figure 9:** Snapshots of the simulated hydraulic structure of the three GDC canopies considered in this study, referred to as 'Canopy1', 'Canopy2' and 'Canopy3', respectively, prior to solar noon, during the first three days

following the onset of soil water deficit, respectively 1 Aug, 2 Aug and 3 Aug. Soil predawn water potential of the three days was equal to  $-0.19$ ,  $-0.38$ ,  $-0.61$  MPa respectively. Filled circles represent xylem water potential, their colors (only for leaves) represent the absorbed PPFD value per unit leaf surface area; sunlit leaves are yellow while shaded leaves are red, and grey circles are for the trunk. Due to uncertainties in measurements locations, the observed water potential values of sunlit leaves are indicated by the grey patches which cover minimum and maximum leaf water potential values. Observed data were collected from experiments conducted in 2012.

**Figure 10:** Snapshots of the stomatal conductance of the three GDC canopies considered in this study, referred to as 'Canopy1', 'Canopy2' and 'Canopy3', respectively, prior to solar noon, during the first three days following the onset of soil water deficit, respectively 1 Aug, 2 Aug and 3 Aug. Soil predawn water potential of the three days was equal to  $-0.19$ ,  $-0.38$ ,  $-0.61$  MPa respectively. Filled circles represent stomatal conductance to water ( $g_{s,H_2O}$ ), their colors represent absorbed PPFD value per unit leaf surface area; sunlit leaves are yellow while shaded leaves are red. Due to uncertainties in measurements locations, the observed stomatal conductance values of sunlit leaves are indicated by the dark grey patches which cover minimum and maximum values. Observed data were collected from experiments conducted in 2012.

The effect of soil water deficit on leaf temperature was efficiently captured by HydroShoot (Figures 11 and 12). The diurnal trends of leaf temperature were adequately reproduced (Figure 11) whereby water-deficit leaves (Figure 11b, d) had higher temperature than those well-watered (Figure 11a, c). The comparison between simulated and observed temperatures at the leaf level (Figure 12) shows that the model simulated an increase in leaf-to-air temperature of approximately  $2$  °C, in agreement with observations (Figure 12a). Furthermore, HydroShoot reproduced the observed magnitude between minimum and maximum leaf temperatures across the canopy (Figure 12b) and how this magnitude increased with soil water deficit (Figure 12c).

The overall adequation between simulated and observed leaf temperature was high when comparing median values (Figure 11) having an MBE of  $-0.5$  and  $-0.8$  °C and an RMSE of  $0.8$  and  $1.0$  °C under well-watered and water deficit conditions, respectively. A greater RMSE of  $2.4$  °C was obtained when leaf-to-leaf comparison was performed (Figure 12), yet, MBE remained at  $-0.45$  °C.

It is noteworthy that leaf temperature was systematically underestimated during nocturnal hours (Figure 11, Figure 12). Luquet *et al.* (2003) and Bailey *et al.* (2016) reported similar trends that they explained by the frequent dysfunction of thermocouples during the night. From a modelling perspective however, such discrepancies between simulated and observed temperatures may be explained by three possibilities. From the one hand, HydroShoot assumes flat leaves having uniform temperature across their surface, whereas strong temperature gradients occur across the surface of each individual leaf due to their three-dimensional structure (Saudreau *et al.*, 2017). Thermocouples measure the temperature of only a limited fraction of leaf surface, and it is likely that the measured

temperature differs from the uniform one simulated. From the other hand, HydroShoot considers only forced heat convection driven by wind speed (cf. [Eq. 14](#)), which may lead to underestimate convective heat transfer during nights with low wind speed (0.02 to 0.2  $m s^{-1}$  were recorded). The overall result is an underestimate leaf temperature during nocturnal hours. Finally, the error in simulated temperature may result from the assumption of a constant sky emissivity, while the latter is well known to vary with air humidity and temperature ([Brunt \*et al.\*, 1932](#)).

**Figure 11:** Comparison between simulated and observed individual leaf temperature for VSP canopies under well-watered (a, b) and water deficit (c and d) conditions. Soil predawn water potential of the four days was equal to -0.37, -0.50, -0.40, and -0.32  $MPa$  respectively. (a and b) diurnal variation in leaf temperature: red zones indicate the extension between maximum and minimum simulated values, black curves indicate simulated mean values while blue boxplots indicate observed leaf temperature; (c and d) are 1:1 plots between observed (x-axis) and simulated (y-axis) leaves median temperatures for each hour with error bars representing minimum and maximum temperature values.

**Figure 12:** Comparison between the observed and simulated (a) differences between leaf and air temperatures, (b) leaf temperatures, and (c) magnitude between minimum and maximum leaf temperatures across the canopy of VSP plants. Maximum and minimum leaf temperatures during each hour are represented by circles and triangles, respectively (a and b plots), well-watered and water deficit conditions are represented by blue red colours, respectively.

## Plant-scale

The observed daily patterns of  $A_{n,plant}$  and  $E_{plant}$  were accurately reproduced under both well-watered and water deficit conditions ([Figure 13](#) for VSP and [Figure 14](#) for GDC) .

For VSP canopies ([Figure 13](#)), the reduction in soil-water availability was reflected by the severe reductions in  $A_{n,plant}$  and  $E_{plant}$  rates, consistently with observations but with a slight overestimation of  $E_{plant}$  ([Figure 13](#)) under well-watered conditions. MBE and RMSE totalled respectively  $-0.1 \mu mol s^{-1}$  and  $5.5 \mu mol s^{-1}$  for  $A_{n,plant}$  under well-watered conditions ([Figure 13a](#)), compared to  $1.0 \mu mol s^{-1}$  and  $3.8 \mu mol s^{-1}$ , respectively, under water deficit conditions ([Figure 13b](#)). For  $E_{plant}$ , MBE and RMSE were respectively  $89.5 g h^{-1}$  and  $141.7 g h^{-1}$  under well-watered conditions ([Figure 13c](#)), compared to  $27.7 g h^{-1}$  and  $67.6 g h^{-1}$ , respectively under water deficit conditions ([Figure 13d](#)).

For the three water-deficit GDC canopies (where only  $E_{plant}$  rates were observed), HydroShoot reasonably reproduced the diurnal patterns in  $E_{plant}$  (Figure 14). Yet,  $E_{plant}$  rates were underestimated upon the onset of water stress (day 1 Aug in Figure 14) and were slightly overestimated thereafter. MBE fall between  $-22.3$  and  $29.2 \text{ g h}^{-1}$  and RMSE between  $13.7$  and  $105.4 \text{ g h}^{-1}$  which were similar to values obtained for VSP. It is noteworthy that the impact of the imbalance in leaf area between both cordons of Canopy1 (cf. Figure 5) was reflected in the simulated  $E_{plant}$  (Figure 14, Canopy1) whereby a noticeable differences in the simulated fluxes was obtained between both cordons of the canopy consistently with the observed sap flow rates. This example further demonstrates how the impact of canopy is adequately reflected on its eco-physiological functioning in HydroShoot.

**Figure 13:** Comparison between simulated and observed plant net carbon assimilation ( $A_{n,plant}$ ) and transpiration ( $E_{plant}$ ) rates of VSP canopies. The subplots a, b, c and d trace the temporal trends of  $A_{n,plant}$  and  $E_{plant}$  (grey circles are for observed values and blue lines are for those simulated) conducted under well-watered (a, c) and water deficit (b, d) conditions. Subplots e and f compare simulated to observed rates for both water conditions (blue dots for well-watered and red dots for water deficit). Soil predawn water potential of the four days was equal to  $-0.13$ ,  $-0.15$ ,  $-0.15$ ,  $-0.08$  respectively under well-watered conditions and  $-0.19$ ,  $-0.30$ ,  $-0.37$ , and  $-0.50 \text{ MPa}$  respectively under water-stress. MSE and RMSE indicate respectively mean bias error and root mean squared error (same units of the y-axes).

**Figure 14:** Comparison between the observed (circles) and simulated (curves) transpiration rates  $E_{plant}$  for each cordon of three grapevines plants trained to GDC under water deficit conditions. Soil predawn water potential of the three canopies was equal to  $-0.19$ ,  $-0.38$ ,  $-0.61$ , and  $-0.51 \text{ MPa}$  respectively. Red and blue colors indicate fluxes through east- and west-exposed cordons respectively. MSE and RMSE indicate respectively mean bias error and root mean squared error (same units of the y-axes).

## To which extent is modelling complexity needed?

We show in Figure 15 together with Table 1 that the best fit between simulated and observed gas-exchange rates was obtained using the complete HydroShoot model (i.e. sim0) which yielded, in almost all cases, the least values of MBE and RMSE for both  $A_{n,plant}$  and  $E_{plant}$ . However, the simulated hydraulic structure and spatialized leaf temperature values had unequal contributions to prediction's accuracy.

When stomatal aperture was dissociated from soil water status (i.e. sim1 and sim4), the results indicated a substantial increase in prediction errors, resulting in particular in the highest values for both MBE and RMSE for  $E_{plant}$ . For instance, RMSE increased from 142 to 361  $g h^{-1}$  under well-watered conditions, and from 68 to 315  $g h^{-1}$  under water deficit conditions, when sim0 is compared to sim1. An improvement in prediction quality was obtained when stomatal aperture was linked to the collar water potential  $\Psi_{collar}$  (i.e. sim2), yet, a considerable error still existed compared to the reference case. For instance, MBE of  $A_{n,plant}$  increased from -0.05 to 1.26  $\mu mol s^{-1}$  and from 1.01 to 3.53  $\mu mol s^{-1}$ , respectively under well-watered and water deficit conditions, with sim2 compared to sim0. Similarly, MBE of  $E_{plant}$  increased from 89 to 170  $g h^{-1}$  and from 28 to 35  $g h^{-1}$  respectively under well-watered and water deficit conditions, using sim2 compared to the reference case sim0.

This result confirms the central role played by the hydraulic structure on tightening stomatal conductance in a species well-known for its conservative behaviour towards water deficit (i.e. iso- or near-isohydric, **Jacobsen et al., 2015**). It indicates that linking leaf-scale stomatal aperture to leaf-level water potential (through  $\Psi_{leaf}$ ), by simulating the hydraulic structure, brings a considerable improvement to model performance. That is, predicting the intra-canopy variability in leaf water potential improves prediction accuracy of gas-exchange rates at the whole plant scale. This result agrees with the conclusions reported by **Ngao et al. (2017)** on the role of leaf water potential variability on apple tree gas-exchange rates. The authors firstly reported that a reliable prediction of plant-scale gas-exchange fluxes in apple trees was allowed when stomatal closure was simulated as a function of soil water potential. However, they postulated that further improvements are yet expected when the hydraulic structure of the shoot is simulated.

Regarding the contribution of simulating leaf-scale energy balance to the predicted plant-scale fluxes, its effect was shown weak (Table 1). Indeed, disregarding energy balance calculations (i.e. sim3) merely affected the predicted  $A_{n,plant}$  rates under both water conditions. For the well-watered case, MBE and RMSE changed from of -0.05 to -0.26  $\mu mol s^{-1}$  and from 5.5 to 5.6  $\mu mol s^{-1}$ , respectively, using sim0 compared to sim3. For the water deficit case, MBE changed from of 1.01 to 1.05  $\mu mol s^{-1}$  while RMSE merely changed. Similar results were also obtained for  $E_{plant}$ .

Our results disagree with those reported by **Bauerle et al. (2007)** who estimated that disregarding the intra-canopy variability in leaf temperature would lead to overestimate  $E_{plant}$  by 22 to 25% for Red Maple (*Acer rubrum* L.) In our case study on grapevine, disregarding leaf energy balance calculations increased the simulated  $E_{plant}$  by no more than 9% [see Supporting Information S5]. The differences between our results and those reported by **Bauerle et al. (2007)** may rely on the

way the authors accounted for the impact of microclimate inside the canopy on leaf photosynthetic traits. In their study, **Bauerle et al. (2007)** used leaf temperature as the primer driver for intra-canopy variability in leaf photosynthetic traits. In our study, we linked leaf photosynthetic traits to the 10-days cumulative absorbed PPFD (cf. Eq. 12) while leaf temperature was used only to affect directly  $A_n$ , and indirectly  $g_{s,H_2O}$ . This conceptual difference may explain the lower sensitivity to leaf temperature in our study compared to that performed by **Bauerle et al. (2007)**. **Bailey et al. (2016)** showed furthermore that the importance of accounting for the intra-canopy distribution of leaf temperature in FSPMs is a matter of canopy size. The authors reported that for grapevines, leaf temperature distribution had a negligible impact on the simulated plant-scale emitted thermal longwave irradiance. In contrast, on Freeman maple (*Acer × Freemanii*) which have notably higher leaf area per plant, simulating the spatial distribution of leaf temperature reduced by 50% prediction errors of the emitted thermal longwave irradiance. The low sensitivity of HydroShoot to leaf temperature may thus be linked to the simulated canopy size.

Notwithstanding, it is noteworthy that omitting energy balance calculations in HydroShoot allowed saving up to 75% compared to the case where all processes combination was considered (Table 2). Using the complete combination (sim0) is indeed quite costly in time (between 7 and 12 seconds for each simulation time step, i.e. hour). Removing the energy balance reduced considerably time cost (by up to 75% in the case of VSP) and reduced non-convergence risk (data not show). Removing the hydraulic structure (i.e. stomata are only function of VDP, sim4) increased considerably the time required for convergence (60% for VSP and up to 250% for the water-deficit GDC Canopy 1) and non-convergence risk. The considerable economy in calculation cost is an argument that should be considered when simulating large-scale plant scenes.

**Figure 15:** Impact of different modelling details of HydroShoot on the simulated plant carbon assimilation ( $A_{n,plant}$ ) and transpiration ( $E_{plant}$ ) rates: the reference (complete) HydroShoot version is indicated as sim0, sim1 indicates the version whereby leaf stomatal conductance varies with vapor pressure deficit instead of leaf water potential (i.e. original model of **Leuning, 1995**,  $D_0= 5$  in Eq. 5a), sim2 indicates the results obtained when the shoot hydraulic structure was omitted (i.e. all leaves have the same water potential which is equal to that of the collar), sim3 is for results obtained by omitting energy balance of individual leaves (i.e. leaves temperature equal to air temperature) and sim4 is the same as sim1 but with an increased impact of the vapor pressure deficit on  $g_{s,CO_2}$  ( $D_0= 1$  in Eq. 5a), finally, obs and VPD indicate respectively the observed gas rate and air vapor pressure deficit.

**Table 1:** Precision estimators of simulated carbon assimilation ( $A_{n,plant}$ ) and transpiration ( $E_{plant}$ ) rates of the plant of well-watered and water-deficit VSP grapevines using five versions of HydroShoot: sim0, the reference (complete) HydroShoot version, sim1, the version whereby leaf stomatal conductance varies with vapor pressure deficit instead of leaf water potential (i.e. original model of **Leuning, 1995**,  $D_0= 5$  in **Eq. 5a**), sim2, shoot hydraulic structure omitted (i.e. all leaves have the same water potential which is equal to that of the collar), sim3, energy balance of individual leaves omitted (i.e. leaves temperature equal to air temperature) and sim4, the same as sim1 but with an increased impact of the vapor pressure deficit on  $g_{s,CO_2}$  ( $D_0= 1$  in **Eq. 5a**).

		$A_{n,plant}$		$E_{plant}$	
		MBE	RMSE	MBE	RMSE
		$[\mu mol s^{-1}]$	$[\mu mol s^{-1}]$	$[g h^{-1}]$	$[g h^{-1}]$
WW	sim0	-0.05	5.49	89.47	141.66
	sim1	1.26	7.43	225.00	361.18
	sim2	1.20	5.27	170.15	247.45
	sim3	-0.26	5.58	109.18	154.60
	sim4	0.50	5.40	100.04	156.68
WD	sim0	1.01	3.76	27.65	67.57
	sim1	3.03	6.95	193.89	315.41
	sim2	1.36	3.86	35.41	71.13
	sim3	1.05	3.82	34.12	70.81
	sim4	3.16	6.07	127.40	196.02

**Table 2:** Estimation of computation cost for two canopies and three HydroShoot versions (sim0, the complete HydroShoot version, sim3, energy balance of individual leaves omitted (i.e. leaves temperature equal to air temperature) and sim4, leaf stomatal conductance varies with vapor pressure deficit instead of leaf water potential)

Training system	Water condition	Leaf area $[m^2 plant^{-1}]$	Computation time (per time step)		
			sim0	sim3	sim4
VSP <sub>ww</sub>	well-watered	5.2	11.96	2.98	19.87
GDC (Canopy 1)	water deficit	3.56	7.45	2.29	26.57





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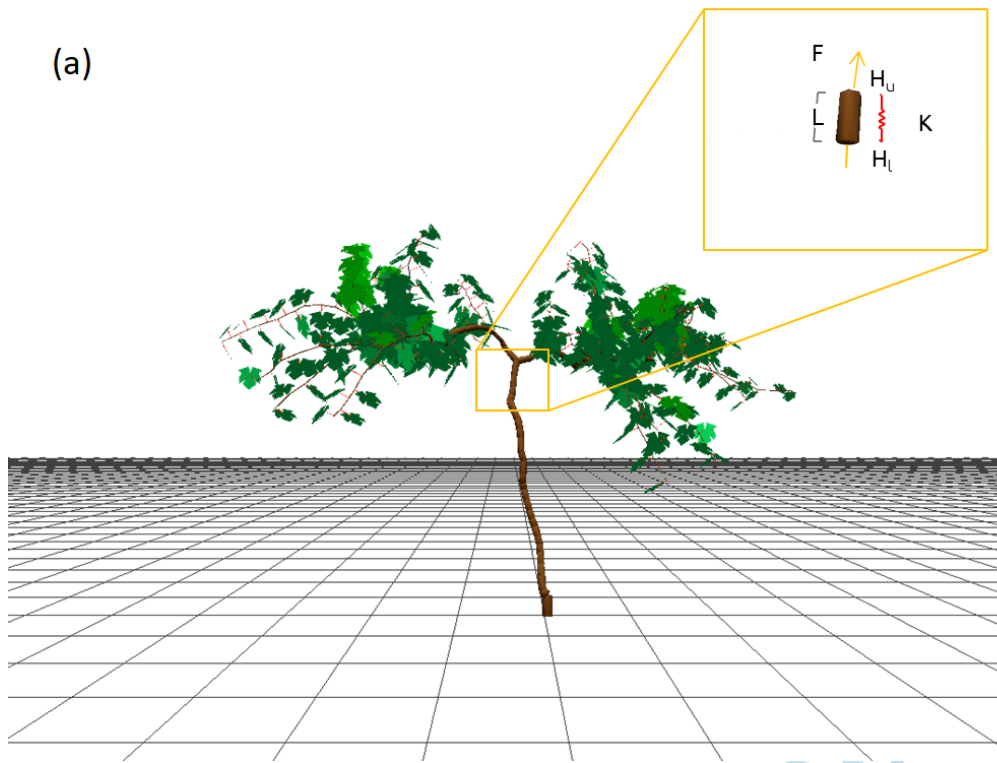
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(b)

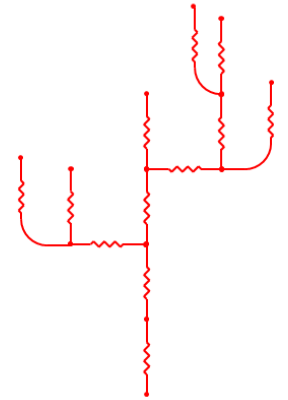


Fig 1

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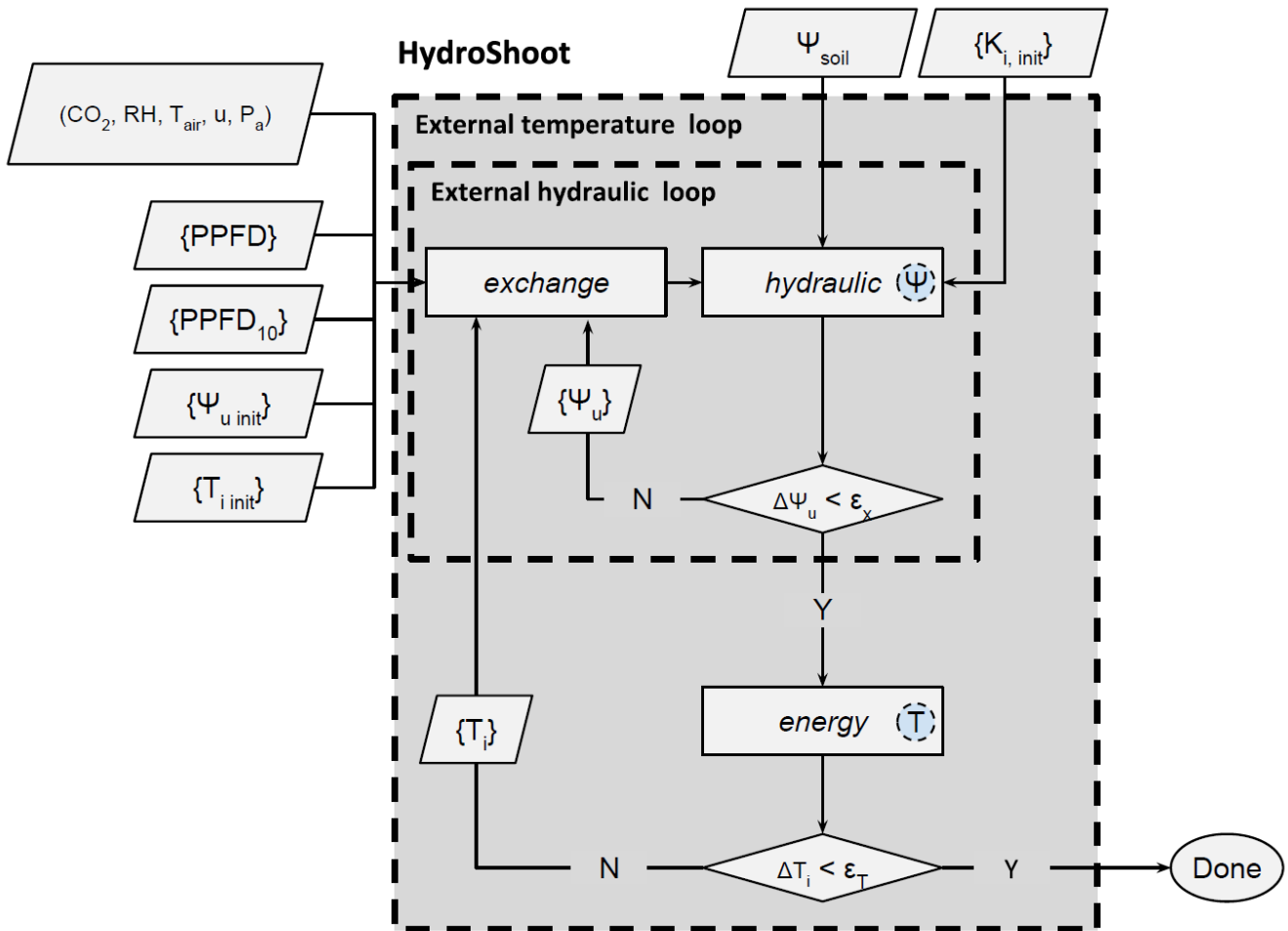


Fig 2

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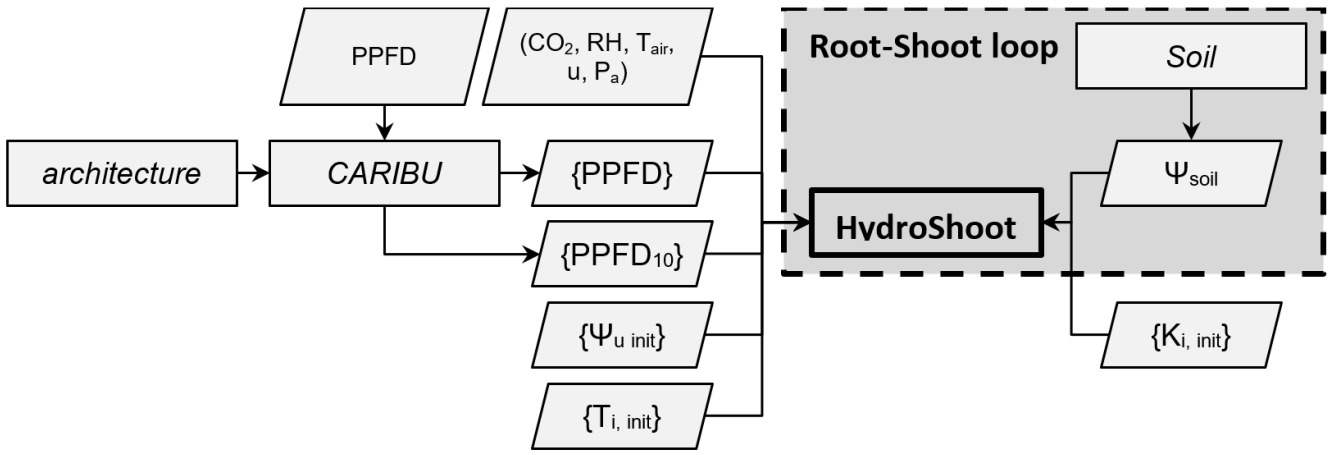


Fig 3

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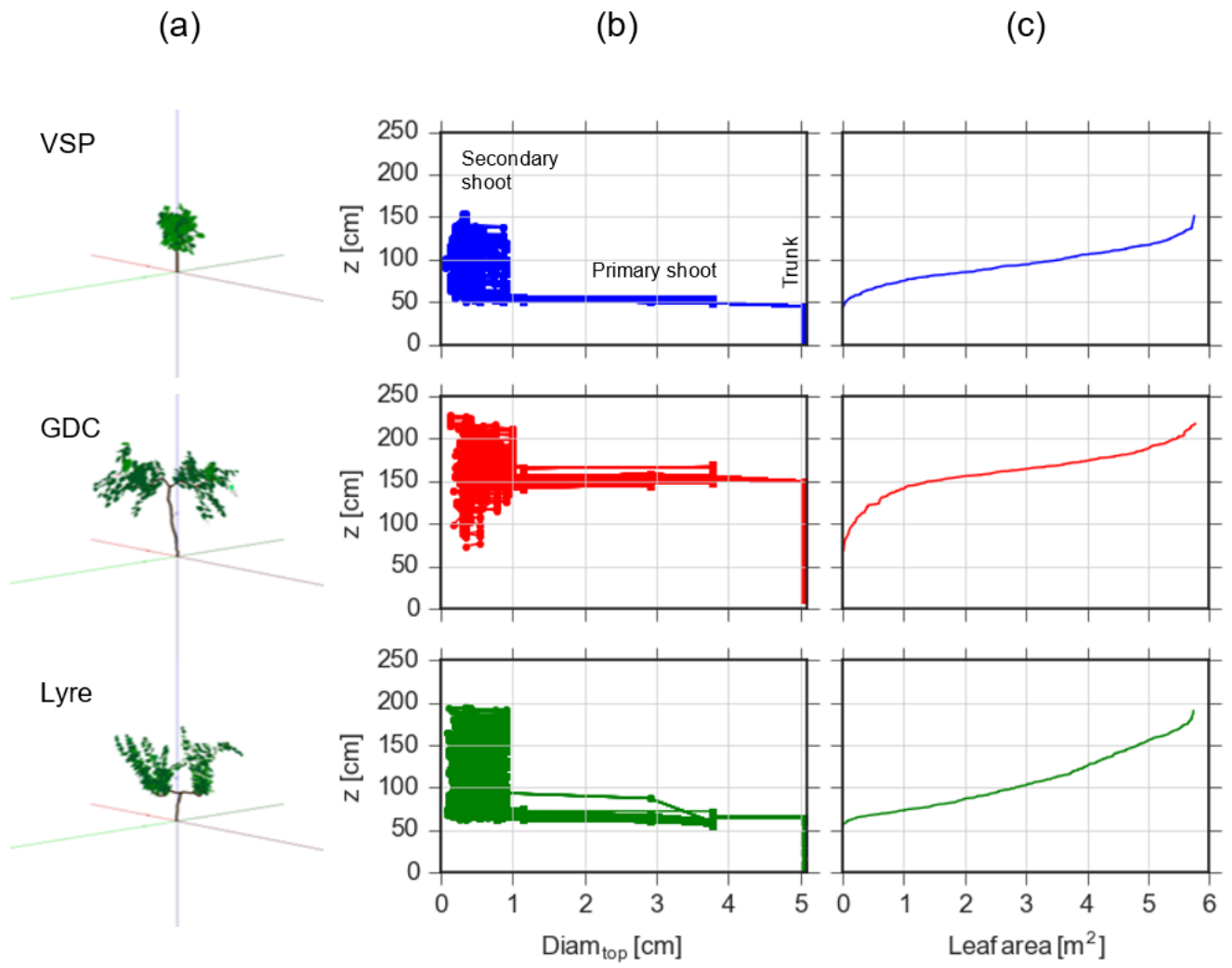


Fig 4

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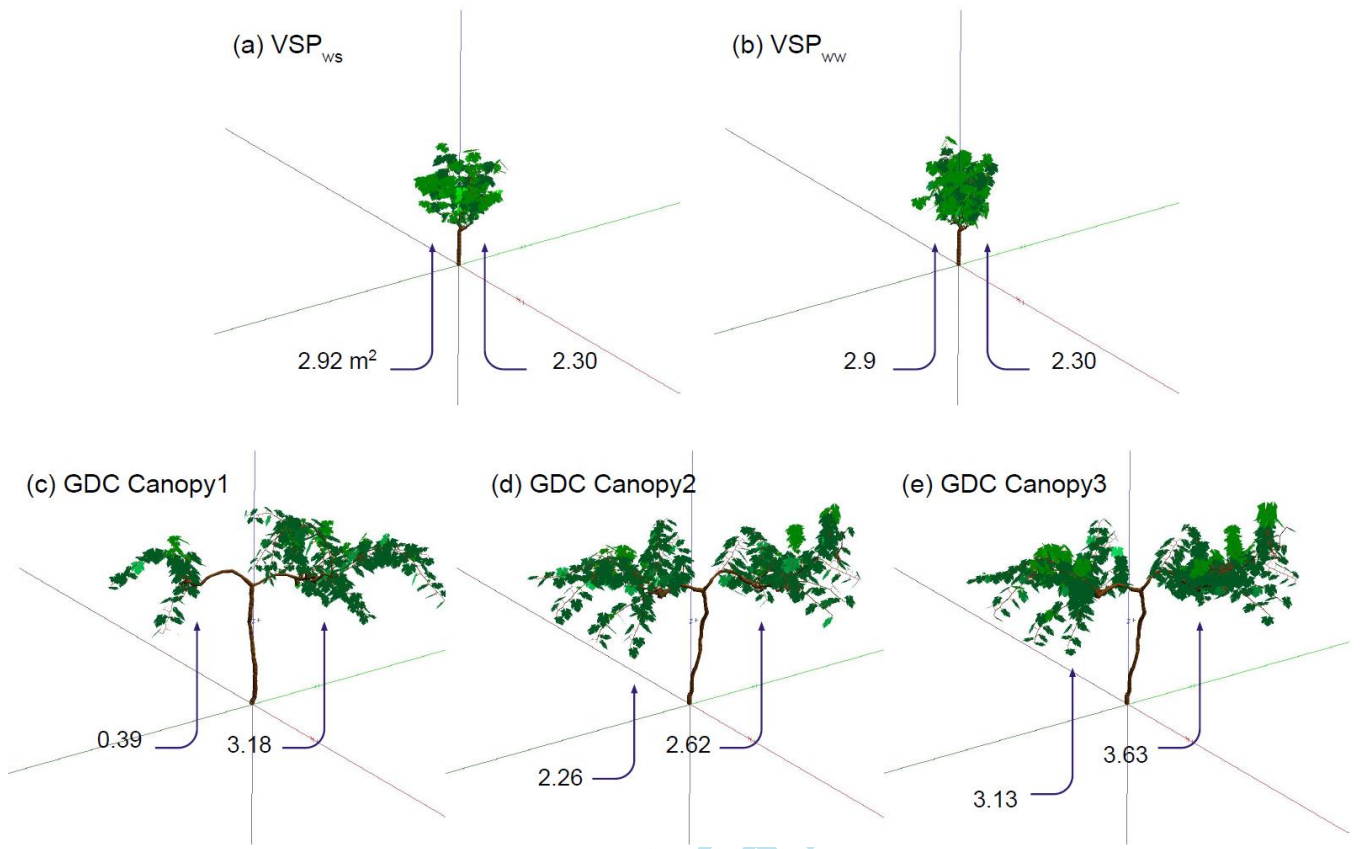


Fig 5

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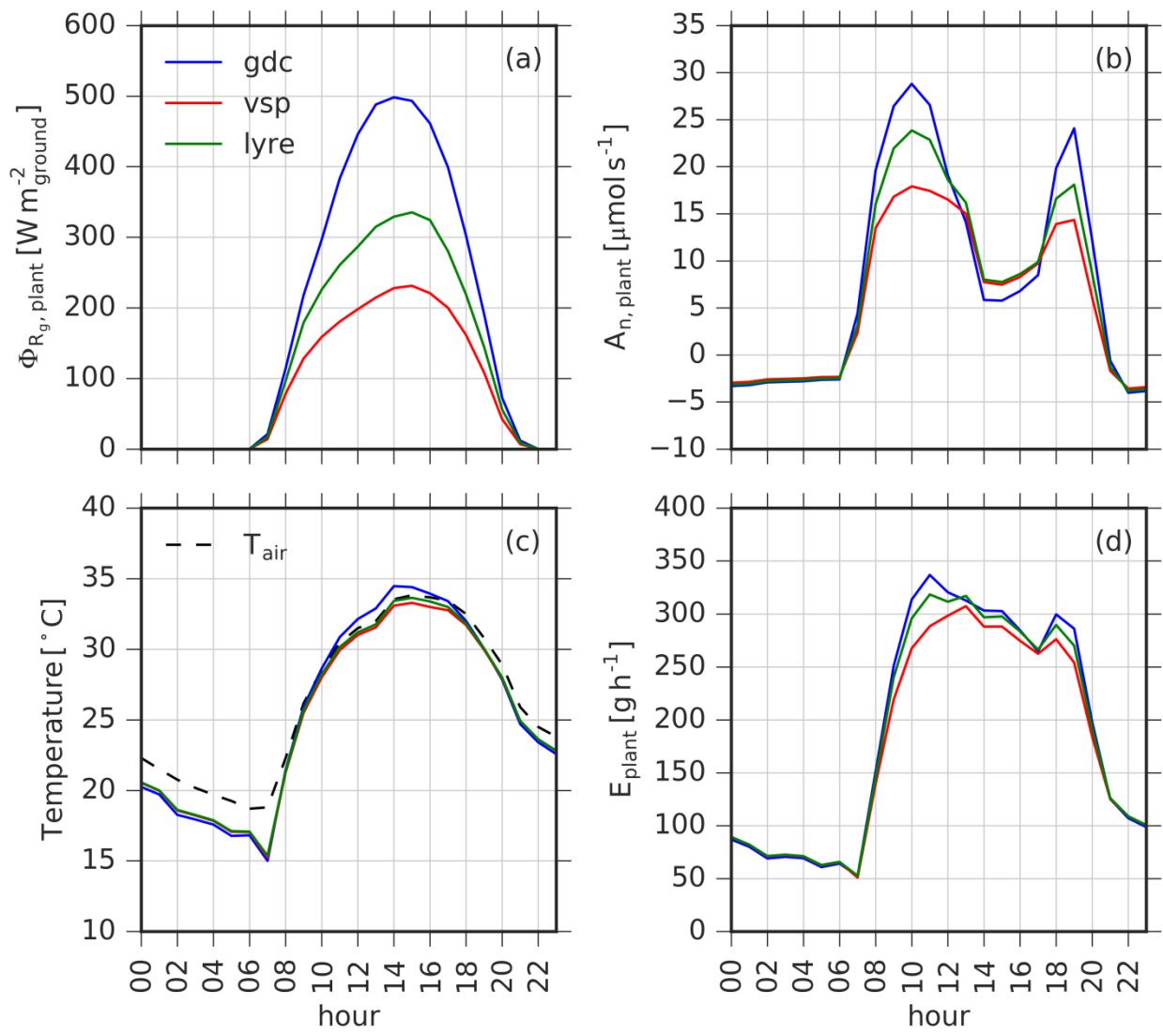


Fig 6

Accepted Article

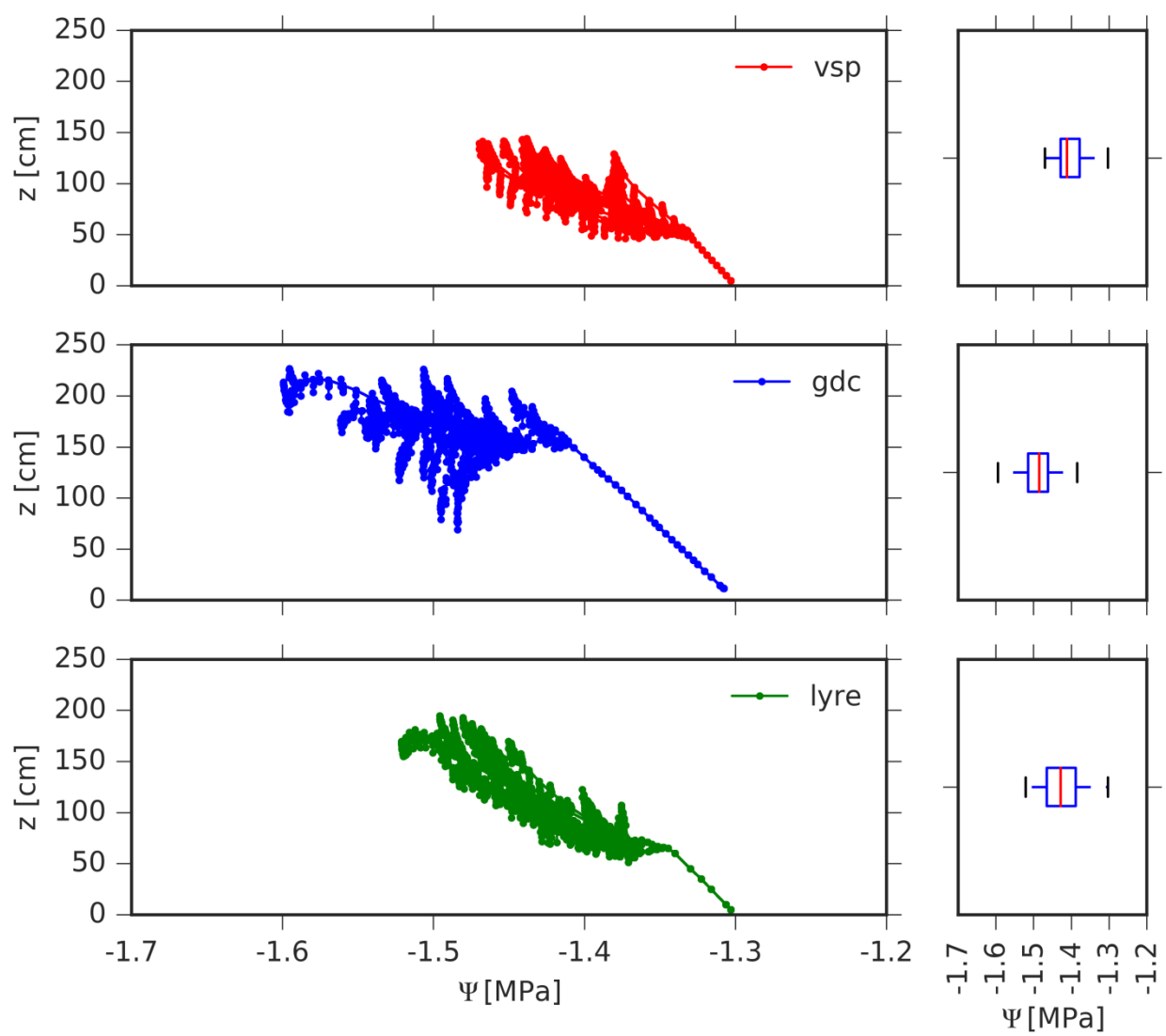


Fig 7

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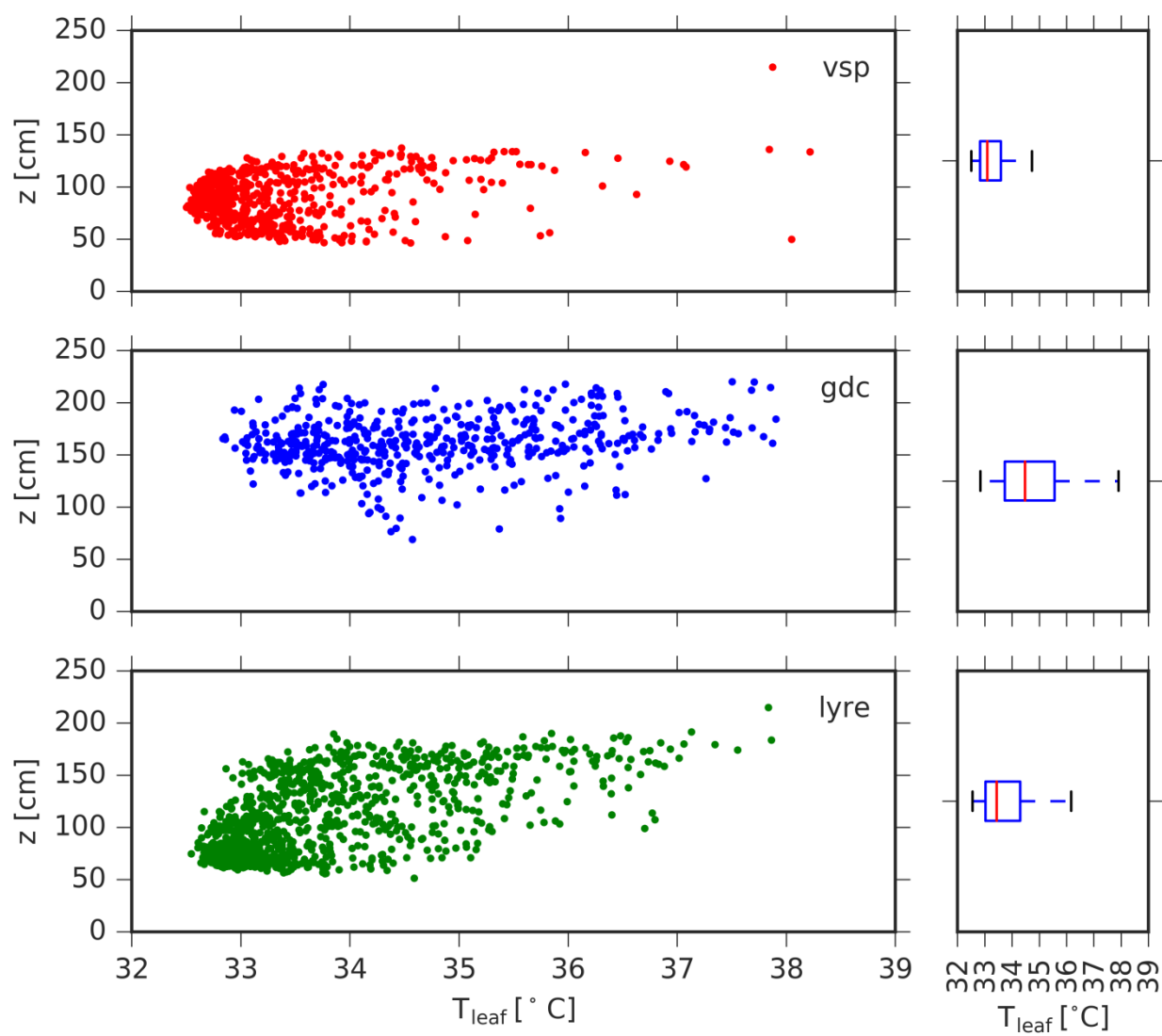


Fig 8

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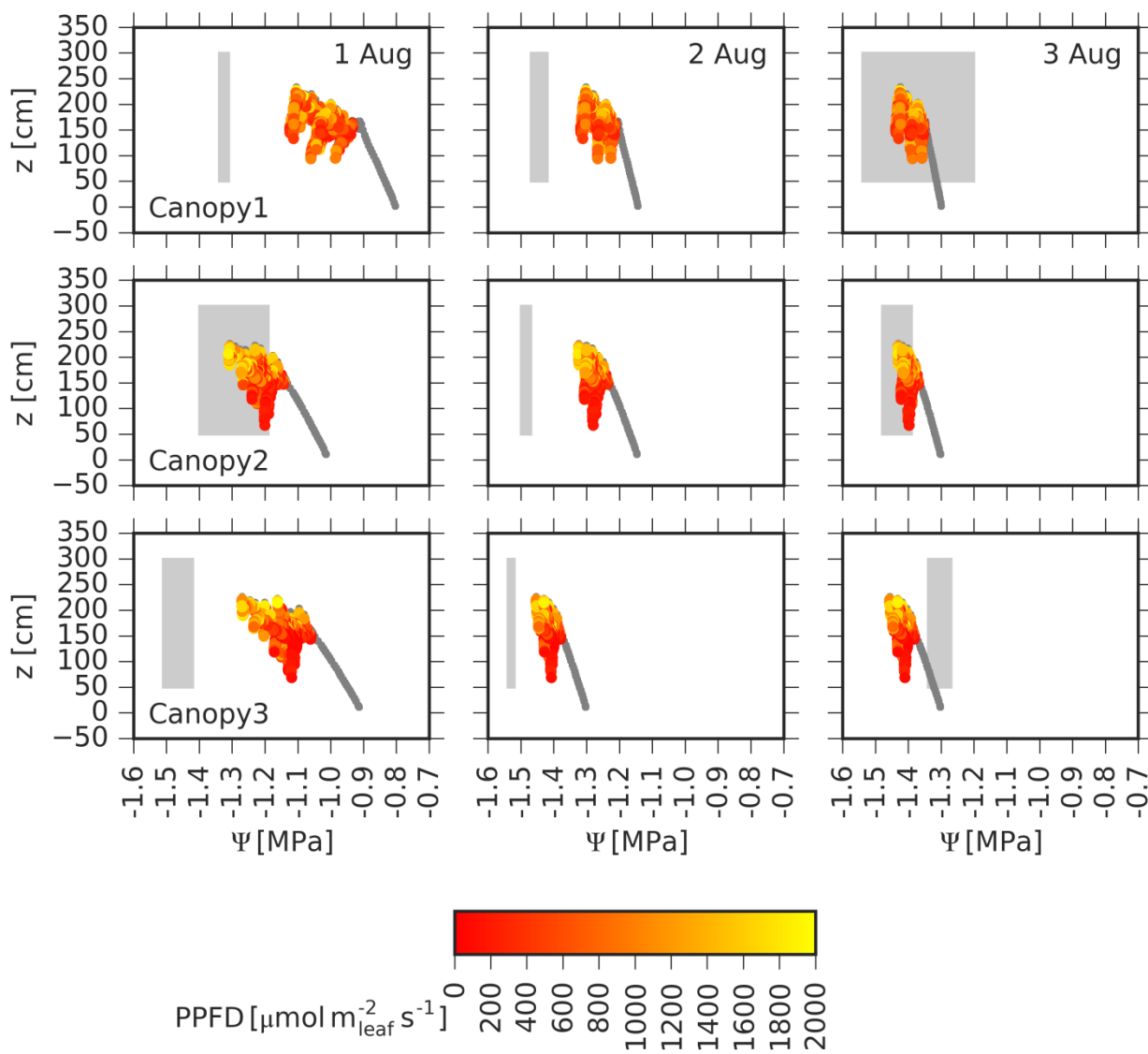


Fig 9

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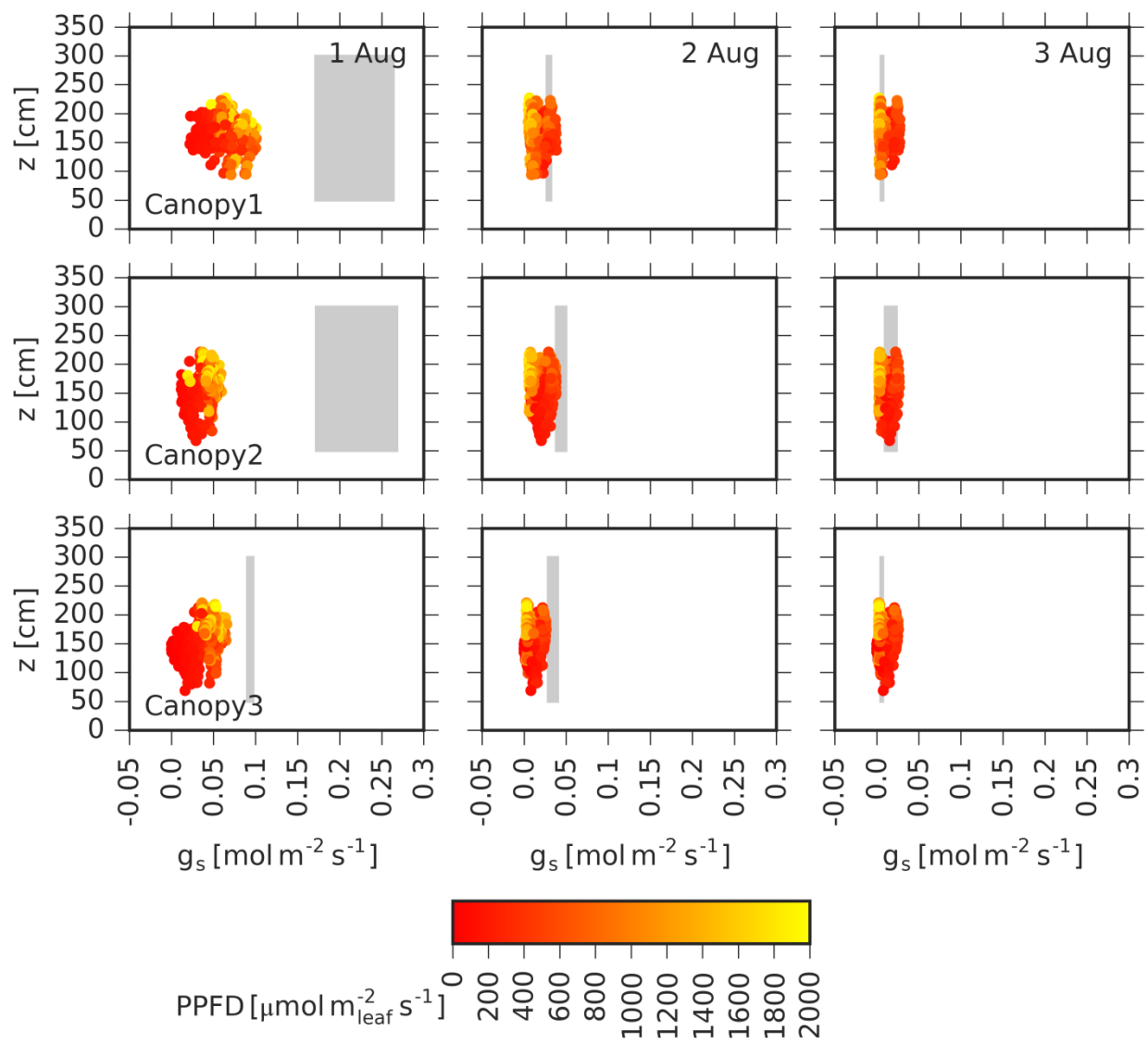


Fig 10

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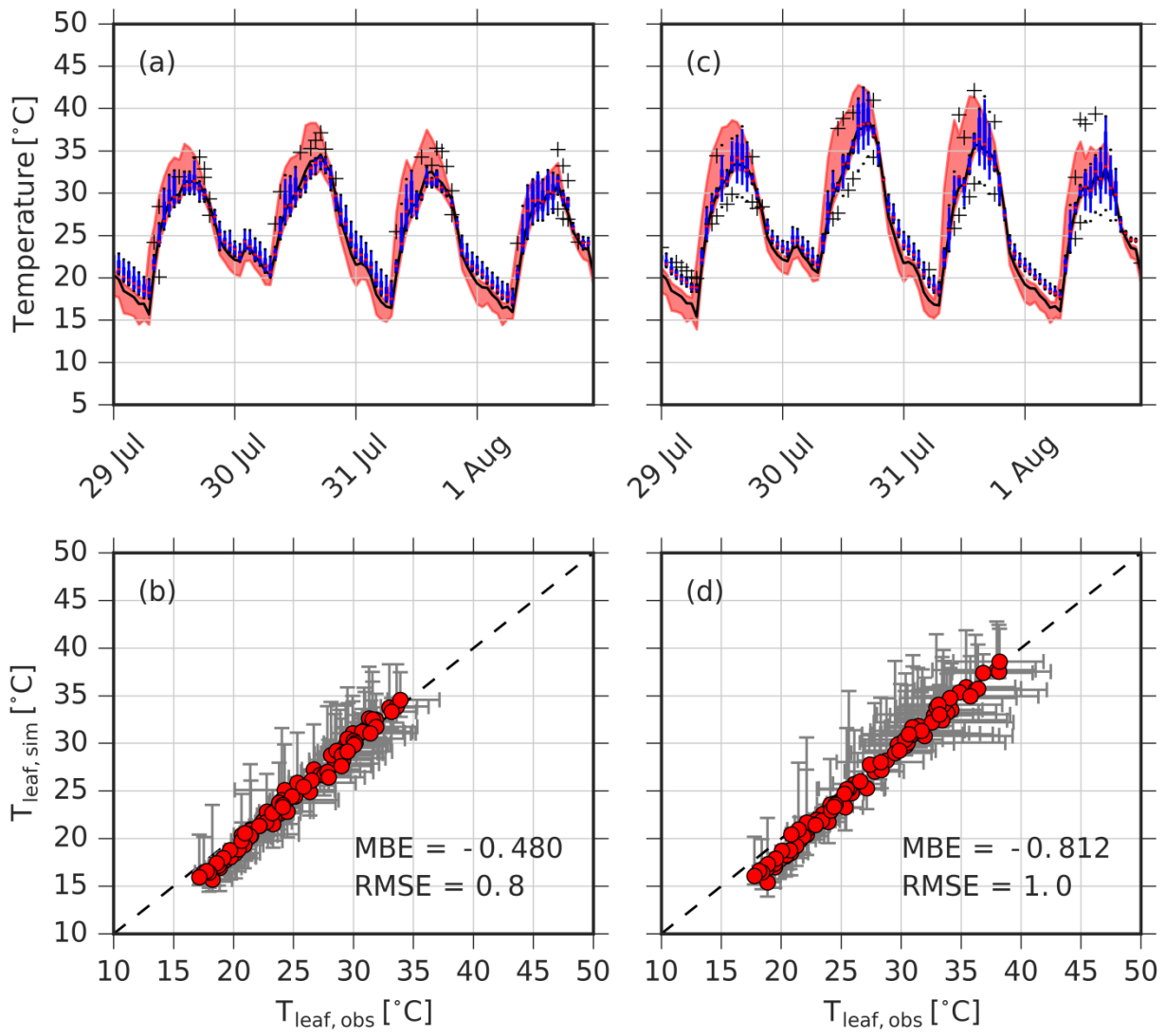


Fig 11

ACCEPTED

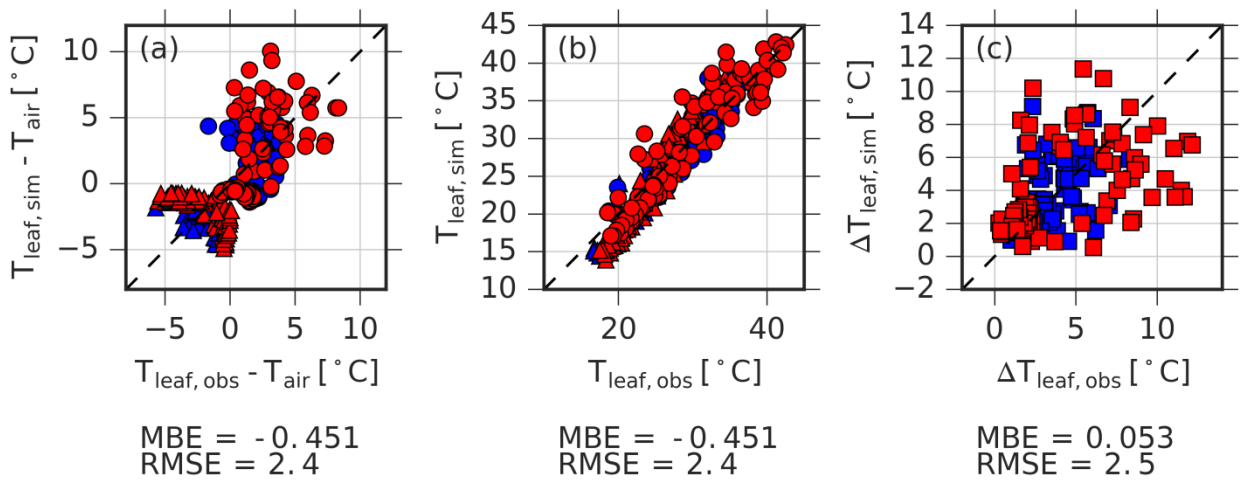


Fig 12

Accepted Manuscript

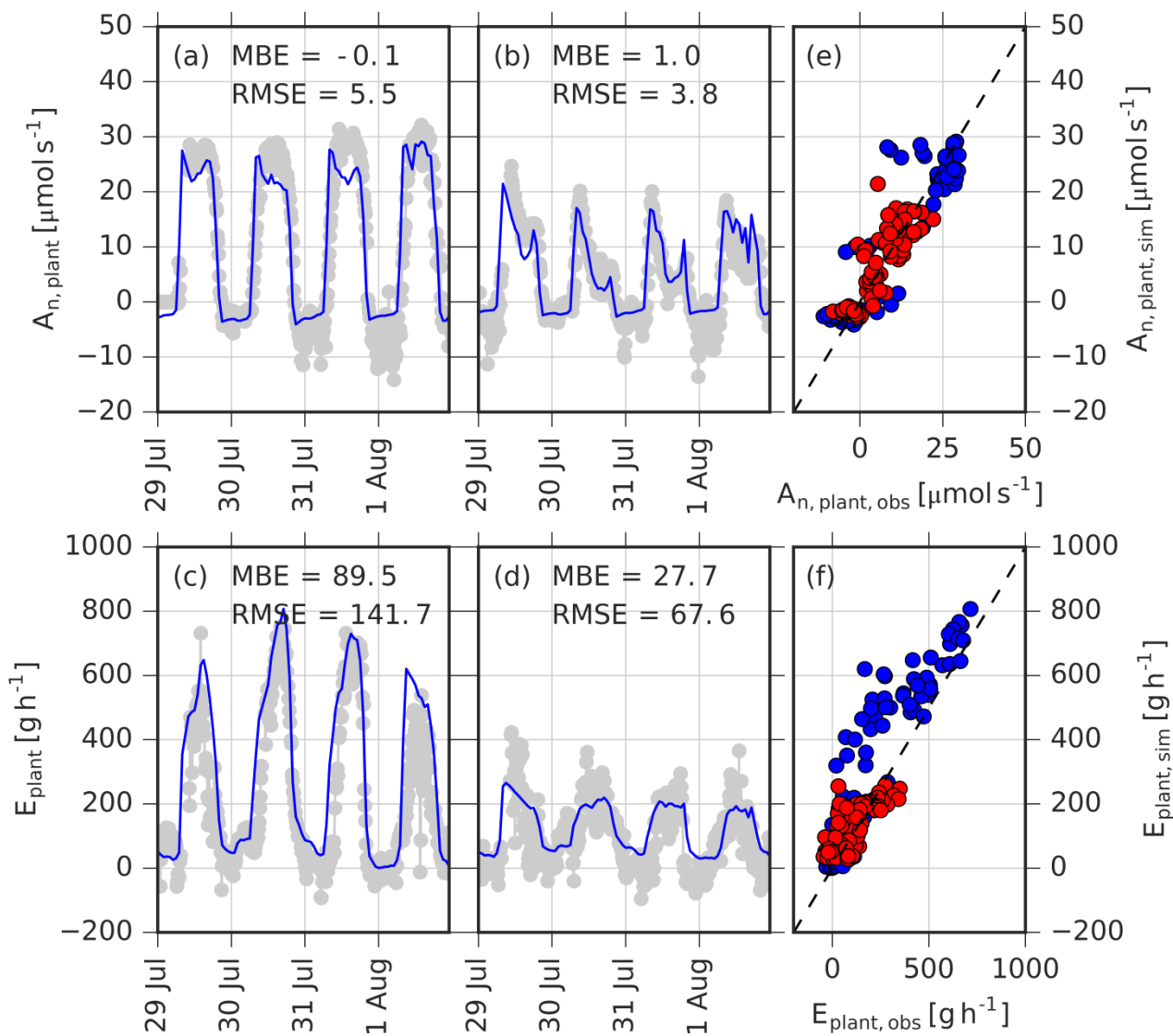


Fig 13

ACCEPTED

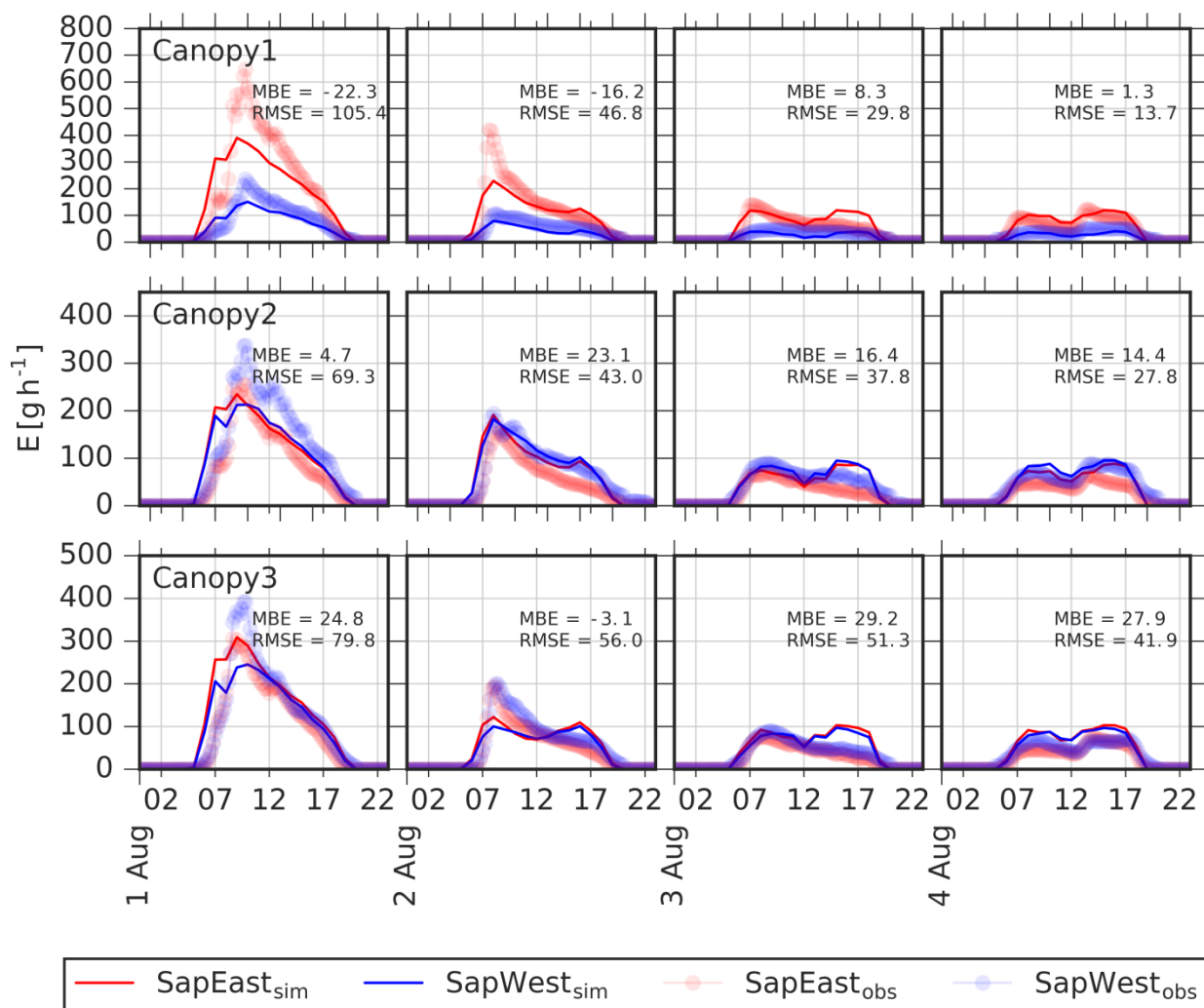


Fig 14

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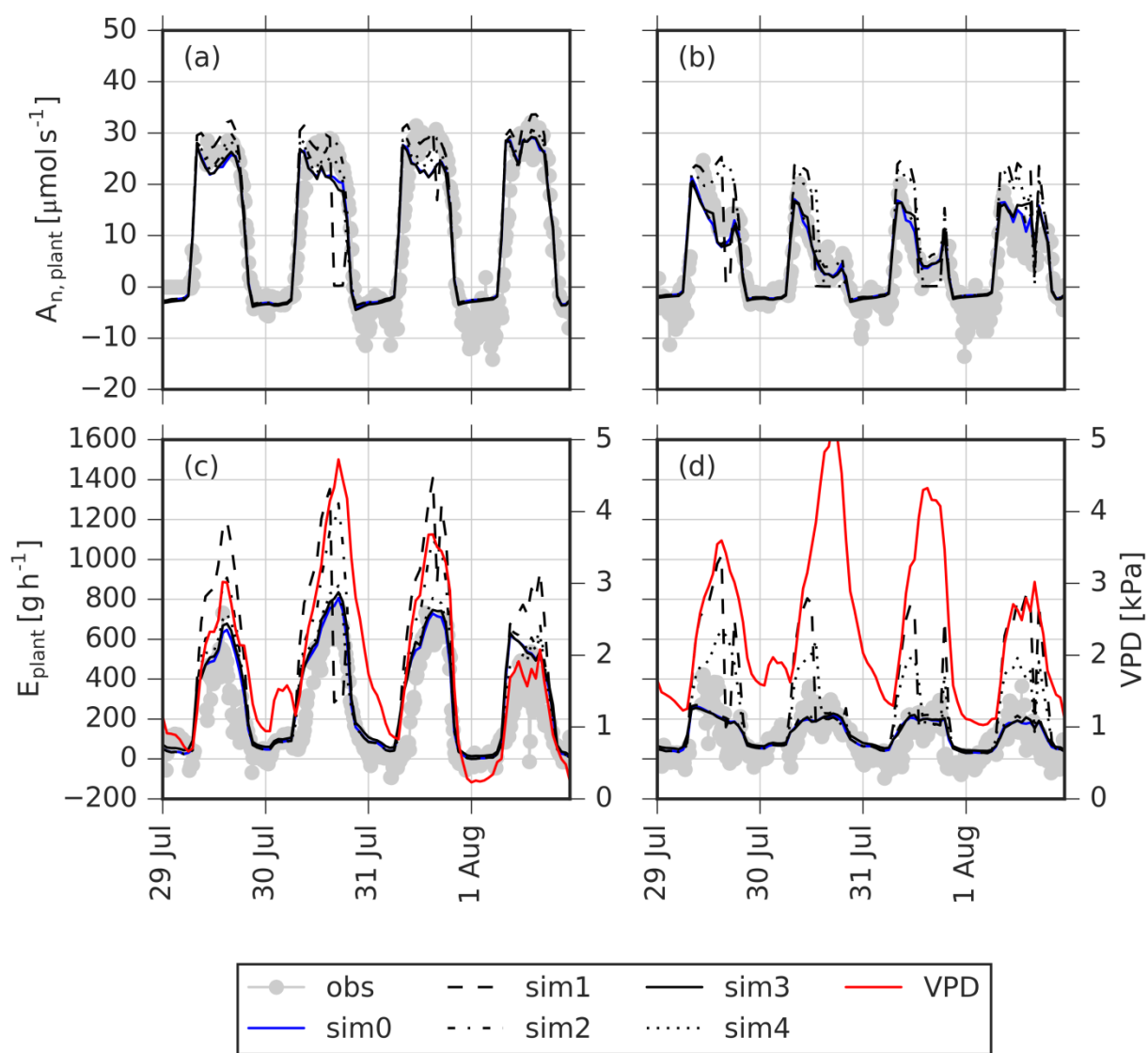


Fig 15

ACCEPTED MANUSCRIPT