

# Identification par assimilation de données de la sensibilité des paquets d'ondes aux effets non-linéaires dans les jets turbulents

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## Identification by data assimilation of the sensitivity of wavepackets in jets to non-linear effects

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### Colloque National d'Assimilation de Données September 28, 2018

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#### Motivations

Resolvent analysis

PSE-4D-Var

Conclusion

Context

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#### Context Wavepackets Non-linearity Motivations

### Jet noise:





São Paulo airport.



- Jet noise dominant during take off.
- Becomes limiting for specifications.
- Noise comes from the flow.

Motivations	Resolvent analysis	PSE-4D-Var	Conclusion
Context Wave	packets Non-linearity		3/20
Motivat	ions		Wavepackets

### Where does the noise come from?

- Turbulent stochastic eddies?
- Or something more organised?
- Wavepackets in pressure/velocity field.



Tinney & Jordan 2008; Co-axial transonic heated jet  $Re = 5 \times 10^6$ .



• Acoustic directivity as extended source (low azimuthal angles).

Jordan & Colonius (2013)

Cavalieri et al. (2012,2013) Tinney et al. (2008)

Motivations	Resolvent analysis	PSE-4D-Var	Conclusion
Context Wavepackets	Non-linearity		3/20
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### Where does the noise come from?

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Jordan & Colonius (2013)

Cavalieri et al. (2012,2013) Tinney et al. (2008)

Near-field pressure.

• Acoustic directivity as extended source (low azimuthal angles).

### Source: likely a wavepacket shape.

Motivations	Resolvent analysis	PSE-4D-Var	Conclusion
Context Wave	epackets Non-linearity		4/20
Motivat	tions		Wavepackets

Jordan & Colonius (2013) Cavalieri et al. (2013) Sinha et al. (2014) Baqui et al. (2015)

### Wavepackets: Propagated linear instability waves





Cavalieri et al. (2013) Sinha et al. (2014) Baqui et al. (2015)

## Wavepackets: Propagated linear instability waves



Non-linearities important for far-field prediction... ...toward low-order non-linear wavepacket model. Gilles Tissor, CNA, September, 2018

Motivations	Resolvent analysis	PSE-4D-Var	Conclusion
Context Wave	packets Non-linearity		5/20
Motivat	ions		Non-linearity

### Non-linearity as an "external forcing"

Landhal (1967) McKeon & Sharma (2010,2013) Moarref et al. (2013) Towne et al. (2015)

Navier-Stokes in the frequency-azimuthal mode domain:

$$\mathcal{L}_{ar{q},\omega,m}\widetilde{q}_{\omega,m}=\mathcal{N}_{ar{q},\omega,m}(q').$$





### Identify relevant non-linearities.



#### Identify relevant non-linearities.



#### Identify relevant non-linearities.

Motivations	Resolvent analysis	PSE-4D-Var	Conclusion
Model Resolvent analysis			6/20
Locally parallel	resolvent analy	vsis	Model
Compressible 1	Navier-Stokes equ	ations:	
$\begin{cases} \frac{\partial \rho}{\partial t} + \nabla .(\rho) \\ \frac{\partial \rho \boldsymbol{u}}{\partial t} + (\boldsymbol{u}) \\ \rho \frac{\partial \gamma rT}{\partial t} + \rho \end{cases}$	$oldsymbol{u} = 0$ $ abla ( ho oldsymbol{u}) = - abla p +  abla .  au$ $ abla (oldsymbol{u}.  abla)( ho rT) = -p( abla . oldsymbol{u})$	$(\mu) + \tau :  abla oldsymbol{u} + rac{1}{RePr}  abla . (\mu)$	$\nabla T$ )

with  $\tau = \frac{1}{Re_a} \left( \mu \left( \nabla \boldsymbol{u} + (\nabla \boldsymbol{u})^T \right) + \left( \mu_B - \frac{2}{3} \mu \right) (\nabla \boldsymbol{.} \boldsymbol{u}) \mathbb{I} \right); p = \rho r T.$ 

rtesorvent analysis	1 DE-4D-Vai	Conclusion
rosolvent analy	raia	6/20
	616 1	Model
Navier-Stokes equ	ations:	
$\begin{aligned} \mathbf{u} &= 0 \\ 7)(\rho \mathbf{u}) &= -\nabla p + \nabla . \tau \\ (\mathbf{u} . \nabla)(\gamma r T) &= -p(\nabla . \mathbf{u}) \end{aligned}$	$oldsymbol{u}$ ) + $ au$ : $ abla oldsymbol{u}$ + $rac{1}{RePr} abla \cdot (\mu  abla T)$	Γ)
	resolvent analysis resolvent analysis Navier-Stokes equal $\mu = 0$ $7)(\rho u) = -\nabla p + \nabla . \tau$ $(u.\nabla)(\gamma rT) = -p(\nabla . u)$	resolvent analysis Navier-Stokes equations: $u = 0$ $7)(\rho u) = -\nabla p + \nabla . \tau$ $(u \cdot \nabla)(\gamma rT) = -p(\nabla . u) + \tau : \nabla u + \frac{1}{RePr} \nabla . (\mu \nabla T)$

with  $\tau = \frac{1}{Re_a} \left( \mu \left( \nabla \boldsymbol{u} + (\nabla \boldsymbol{u})^T \right) + \left( \mu_B - \frac{2}{3} \mu \right) (\nabla \boldsymbol{.} \boldsymbol{u}) \mathbb{I} \right); p = \rho r T.$ 

Linearised Navier-Stokes Equations: over mean flow U(y)

$$\left(\rho, \boldsymbol{u}, T\right)^{T} = \boldsymbol{q}_{\phi}(\boldsymbol{x}, t) = \bar{\boldsymbol{q}}(\boldsymbol{x}) + \boldsymbol{q}'(\boldsymbol{x}, t) \xrightarrow[r/D \ 1.0]{1.0}_{0.5}}_{0.5}$$

Motivations	Resolvent analysis	PSE-4D-Var	Conclusion
Model Resolvent an	alysis		6/20
Locally par	rallel resolvent analy	sis	Model
Compres	sible Navier-Stokes equa	ations:	
$\begin{cases} \frac{\partial \rho}{\partial t} \\ \frac{\partial \rho n}{\partial t} \\ \frac{\partial \rho n}{\partial t} \\ \rho \frac{\partial \gamma}{\partial t} \end{cases}$	$ + \nabla .(\rho \boldsymbol{u}) = 0 $ $ \frac{\boldsymbol{u}}{T} + (\boldsymbol{u}.\nabla)(\rho \boldsymbol{u}) = -\nabla p + \nabla .\tau $ $ \frac{\gamma rT}{\partial t} + \rho(\boldsymbol{u}.\nabla)(\gamma rT) = -p(\nabla .\boldsymbol{u}) $	$)+ au: abla u+rac{1}{RePr} abla.(\mu$	$\iota \nabla T)$
with $\tau = \frac{1}{R}$	$rac{1}{e_a}\left(\mu\left( abla oldsymbol{u}+( ablaoldsymbol{u})^T ight)+\left(\mu_B- ight)$	$\frac{2}{3}\mu\big)\left(\nabla .\boldsymbol{u}\right)\mathbb{I}\big)\;;\;p=\rho rT.$	

Linearised Navier-Stokes Equations: over mean flow U(y)

$$(\rho, \boldsymbol{u}, T)^T = \boldsymbol{q}_{\phi}(\boldsymbol{x}, t) = \bar{\boldsymbol{q}}(\boldsymbol{x}) + \boldsymbol{q}'(\boldsymbol{x}, t)$$

Locally parallel assumption + Fourier Transform:

$$\boldsymbol{q}'(\boldsymbol{x},\boldsymbol{r},\boldsymbol{\theta},t) = \frac{1}{(2\pi)^3} \sum_{m} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \widetilde{\boldsymbol{q}}_{\omega,m,\alpha}(\boldsymbol{r}) \, e^{i(m\boldsymbol{\theta}-\omega t+\alpha x)} \, \mathrm{d}\alpha \, \mathrm{d}\omega.$$

Motivations	Resolvent analysis	PSE-4D-Var	Conclusion
Model Resolvent analysis			7/20
Locally parallel	resolvent a	nalysis	Model

$$\mathcal{L}_{\bar{\boldsymbol{q}},\alpha,\omega,m}\widetilde{\boldsymbol{q}}_{\alpha,\omega,m}=0.$$



$$\mathcal{L}_{\bar{\boldsymbol{q}},\alpha,\omega,m}\widetilde{\boldsymbol{q}}_{\alpha,\omega,m}=0.$$

Non-linear problem:

$$\mathcal{L}_{ar{q},lpha,\omega,m}\widetilde{q}_{lpha,\omega,m}=\mathcal{N}_{ar{q},lpha,\omega,m}\left(q'
ight).$$



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Non-linear problem:

$$\mathcal{L}_{\bar{\boldsymbol{q}},\alpha,\omega,m}\widetilde{\boldsymbol{q}}_{\alpha,\omega,m} = \underbrace{\mathcal{N}_{\bar{\boldsymbol{q}},\alpha,\omega,m}\left(\boldsymbol{q}'\right)}_{B\widetilde{\boldsymbol{f}}_{\bar{\boldsymbol{q}},\alpha,\omega,m}} (B \text{ restricts on } \boldsymbol{u} \text{ comp.})$$



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Non-linear problem:

$$\mathcal{L}_{\bar{\boldsymbol{q}},\alpha,\omega,m}\widetilde{\boldsymbol{q}}_{\alpha,\omega,m} = \underbrace{\mathcal{N}_{\bar{\boldsymbol{q}},\alpha,\omega,m}\left(\boldsymbol{q}'\right)}_{B\widetilde{\boldsymbol{f}}_{\bar{\boldsymbol{q}},\alpha,\omega,m}} (B \text{ restricts on } \boldsymbol{u} \text{ comp.})$$

Linearised problem with external forcing:  $(D(\alpha, \omega, m) \neq 0)$ .

$$H\widetilde{q}_{\alpha,\omega,m} = H\mathcal{L}_{\bar{q},\alpha,\omega,m}^{-1}B\widetilde{f}_{\bar{q},\alpha,\omega,m}.$$

(*H* restricts on  $\boldsymbol{u}$  comp.)

Motivations	Resolvent analysis	PSE-4D-Var	Conclusion
Model Resolvent analysis			8/20
Locally parallel	resolvent analysis		Resolvent analysis

Linearised problem with external forcing:

$$H\widetilde{\boldsymbol{q}}_{\alpha,\omega,m} = \underbrace{H\mathcal{L}_{\overline{\boldsymbol{q}},\alpha,\omega,m}^{-1}B}_{\text{SVD}}\widetilde{\boldsymbol{f}}_{\overline{\boldsymbol{q}},\alpha,\omega,m}.$$

Motivations	Resolvent analysis	PSE-4D-Var	Conclusion
Model Resolvent analysis			8/20
Locally parallel	resolvent a	nalysis	Resolvent analysis

Linearised problem with external forcing:

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SVD to maximise Rayleigh quotient:

$$\max_{\widetilde{f}_{\alpha,\omega,m}} \frac{\|H\widetilde{q}_{\alpha,\omega,m}\|^2}{\|\widetilde{f}_{\alpha,\omega,m}\|^2} = \frac{\|\left(H\mathcal{L}_{\overline{q},\alpha,\omega,m}^{-1}B\right)\widetilde{f}_{\alpha,\omega,m}\|^2}{\|\widetilde{f}_{\alpha,\omega,m}\|^2}$$

Motivations	Resolvent analysis	PSE-4D-Var	Conclusion
Model Resolvent analysis			8/20
Locally parallel	resolvent a	nalysis	Resolvent analysis

Linearised problem with external forcing:

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SVD to maximise Rayleigh quotient:

$$\max_{\widetilde{f}_{\alpha,\omega,m}} \frac{\|H\widetilde{q}_{\alpha,\omega,m}\|^2}{\|\widetilde{f}_{\alpha,\omega,m}\|^2} = \frac{\|\left(H\mathcal{L}_{\overline{q},\alpha,\omega,m}^{-1}B\right)\widetilde{f}_{\alpha,\omega,m}\|^2}{\|\widetilde{f}_{\alpha,\omega,m}\|^2}$$

Most amplified harmonic forcing/response modes:

$$egin{aligned} & H\mathcal{L}_{ar{q},lpha,\omega,m}^{-1}B = U\Sigma V^* \ & H\mathcal{L}_{ar{q},lpha,\omega,m}^{-1}Boldsymbol{V}_i = \sigma_ioldsymbol{U}_i \end{aligned}$$

with  $U = (U_1, \ldots, U_N), V = (V_1, \ldots, V_N)$  and  $\Sigma = \text{diag}(\sigma_1, \ldots, \sigma_N).$ 





Motivations	Resolvent analysis	PSE-4D-Var	Conclusion
Model 4D-Var Sensitivity	Converged Orr mechanism		10/20
PSE-4D-Var			Model

Herbert (1997)

### Parabolised stability equations:

• Locally parallel  $\rightarrow$  Slowly divergent.

$$\widetilde{\boldsymbol{q}}_{\omega,m}(x,r) = \boldsymbol{q}(x,r) \, e^{i \int_0^x \alpha(\xi) \, \mathrm{d}\xi}.$$

• We neglect viscosity.

Motivations	Resolvent analysis	PSE-4D-Var	Conclusion
Model 4D-Var Sensitivity	Converged Orr mechanism		10/20
PSE-4D-Var			Model

Herbert (1997)

### Parabolised stability equations:

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• We neglect viscosity.

Model propagated downstream:

$$\begin{cases} E\frac{\partial \boldsymbol{q}}{\partial x} + (A + \boldsymbol{\alpha}B)\boldsymbol{q} = 0\\ \left(\boldsymbol{q}, \frac{\partial \boldsymbol{q}}{\partial x}\right)_r = 0\\ \boldsymbol{q}(0) = \boldsymbol{q}_{\text{K-H}}, \end{cases}$$

Inflow condition: Kelvin-Helmholtz mode from locally parallel stability analysis.

Motivations	Resolvent analysis	PSE-4D-Var	Conclusion
Model $4D-Var$	Sensitivity Converged Orr mechanism		11/20
PSE-4D-	-Var		4D-Var

Observations:  $\mathcal{Y}$ : PSD  $(|u|^2, |v|^2)^T$ 

Papadakis (2007) Ansaldi (2015)



Gilles TISSOT, CNA, September, 2018

Motivations	Resolvent analysis	PSE-4D-Var	Conclusion
Model 4D-Var S	Sensitivity Converged Orr mechanism		11/20
PSE-4D-	Var		4D-Var

Model: Parabolised Stability Equations (PSE)

 $\sim$ 

Papadakis (2007) Ansaldi (2015)

$$\begin{cases} E\frac{\partial \boldsymbol{q}}{\partial x} + (A + \alpha B)\boldsymbol{q} = \boldsymbol{f} \\ \left(\boldsymbol{q}, \frac{\partial \boldsymbol{q}}{\partial x}\right)_r = 0 & \text{with} \quad \tilde{\boldsymbol{q}}_{\omega,m}(x) = \boldsymbol{q}(x)e^{i\int_0^{\boldsymbol{\xi}}\alpha(\boldsymbol{\xi})\,\mathrm{d}\boldsymbol{\xi}} \\ \boldsymbol{q}(0, r) = \boldsymbol{q}_0 + \boldsymbol{\eta}, \quad \alpha(0) = \alpha_0, \end{cases}$$



Motivations	Resolvent analysis	PSE-4D-Var	Conclusion
Model 4D-Var Se	ensitivity Converged Orr mechanism		11/20
PSE-4D-V	Var		4D-Var

4D-Var: search for  $(\mathbf{f}_{\min}, \mathbf{\eta}_{\min}) = \operatorname{argmin}(\mathcal{J}(\mathbf{q}, \alpha, \mathbf{f}, \mathbf{\eta}))^{Papadakis} (2007)$ Ansaldi (2015)

$$\mathcal{J} = \frac{1}{2} \int_0^L \|\mathbb{H}(\boldsymbol{q}, \alpha) - \mathcal{Y}\|_{W_o}^2 \, \mathrm{d}x + \frac{1}{2} \|\mathbb{H}_L - \mathcal{Y}_L\|_{W_T}^2 \\ + \frac{1}{2} \int_0^L \|\boldsymbol{f}\|_{W_f}^2 \, \mathrm{d}x + \frac{1}{2} \|\boldsymbol{\eta}\|_{W_\eta}^2.$$



Motivations	Resolvent analysis	PSE-4D-Var	Conclusion
Model 4D-Var Sensitivity	Converged Orr mechanism		11/20
PSE-4D-Var			4D-Var

4D-Var: search for  $(\mathbf{f}_{\min}, \mathbf{\eta}_{\min}) = \operatorname{argmin}(\mathcal{J}(\mathbf{q}, \alpha, \mathbf{f}, \mathbf{\eta}))^{Papadakis} (2007)$ Ansaldi (2015)

$$\mathcal{J} = \frac{1}{2} \int_0^L \|\mathbb{H}(\boldsymbol{q}, \alpha) - \mathcal{Y}\|_{W_o}^2 \, \mathrm{d}x + \frac{1}{2} \|\mathbb{H}_L - \mathcal{Y}_L\|_{W_T}^2 \\ + \frac{1}{2} \int_0^L \|\boldsymbol{f}\|_{W_f}^2 \, \mathrm{d}x + \frac{1}{2} \|\boldsymbol{\eta}\|_{W_\eta}^2.$$

What are the missing non-linearities f in the linear model? Solved using adjoint method (adjoint PSE).



Motivations	Resolvent analysis	PSE-4D-Var	Conclusion
Model $4D-Var$	Sensitivity Converged Orr mechanism		12/20
PSE-4D-	-Var		4D-Var

### Adjoint equation:

$$\begin{cases} -E^{+}\frac{\partial \boldsymbol{\lambda}}{\partial x} + \left(A + \alpha B - \frac{\partial E}{\partial x}\right)^{+} \boldsymbol{\lambda} + \frac{\partial \boldsymbol{q}}{\partial x}(\zeta - \zeta^{*}) - \boldsymbol{q}\frac{\partial \zeta^{*}}{\partial x} = RHS_{1}, \\ (B\boldsymbol{q}, \boldsymbol{\lambda})_{r} = RHS_{2}, \\ E^{+}\boldsymbol{\lambda}(L, r) = RHS_{3}, \\ \zeta(L) = 0. \end{cases}$$

Optimality condition:

$$\begin{cases} \frac{\partial J}{\partial \boldsymbol{f}} = \boldsymbol{\lambda}(x, r) + W_{\boldsymbol{f}}\boldsymbol{f} \\ \frac{\partial J}{\partial \boldsymbol{\eta}} = E^{+}\boldsymbol{\lambda}(0, r) + \boldsymbol{q}_{0}\boldsymbol{\zeta}^{*}(0) + W_{\eta}\boldsymbol{\eta}. \end{cases}$$

- Solved iteratively (steepest descent).
- Weights determined by L-curve method.





 $|u|^2$ , grayscale=observation error.





 $|u|^2$ , grayscale=observation error, contour=sensitivity.





#### Predicted by locally parallel resolvent analysis.





#### Inflow condition not sensitive:

- Critical layer sensitivity when neutral  $(x \approx 3)$ .
- Kelvin-Helmholtz growth dominates upstream (modal behaviour).
- Homogeneous PSE works upstream.

Motivations	Resolvent analysis	PSE-4D-Var	Conclusion
Model 4D-Var	Sensitivity Converged Orr mechanism		15/20
PSE-4D-	-Var		Converged



Real(u), St=0.6

High forcing near:

- Critical layer.
- Centerline.

#### Converged results conserve the same trend.

#### Motivations

Resolvent analysis

Model 4D-Var Sensitivity Converged Orr mechanism

PSE-4D-Var

## PSE-4D-Var





Observation  $\mathcal{Y}^u$  Match experiments. Observation  $\mathcal{Y}^v$ 

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#### Converged





#### Orr mechanism:



#### Tilting suggesting Orr mechanism in space.

Motivations	Resolvent analysis	PSE-4D-Var	Conclusion
Model 4D-Var Se	ensitivity Converged Orr mechanism		18/20
PSE-4D-V	Var		Orr mechanism

Orr (1907) Case (1960)

Orr model: for Couette flow (U(y) = Sy).

Temporal Orr model: vorticity convected by shear

$$\begin{split} \left(\frac{\partial \cdot}{\partial t} - Sy\frac{\partial \cdot}{\partial x}\right) \nabla^2 \psi(x,y,t) &= 0, \quad \psi \text{ stream func.} \\ \nabla^2 \psi(x,y,t) &= F(x - Syt,y). \end{split}$$

Spatial Orr model: Fourier Transform in time

$$\nabla^2 \widetilde{\psi}(x, y, \omega) = \widetilde{F}_2(y) \, e^{i \frac{\omega x}{Sy}}.$$

with

$$\widetilde{F}_2(y) = \frac{1}{Sy} \widetilde{F}\left(\frac{\omega}{Sy}, y\right) \quad \text{FFT in } x \text{ of } F(x, y).$$
$$\boxed{\widetilde{F}_2(y) = \nabla^2 \widetilde{\psi}(0, y, \omega)}$$





#### Orr mechanism quantitatively confirmed.

## Conclusion

## Summary

- Forced wavepacket consistent with experiment.
- Critical layer highly sensitive region to non-linearity.
- Along the critical layer, shear convects and tilts the response to non-linearities, leading to an amplification by Orr mechanism.
- PSE-4D-Var powerful tool.