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# A note on Integer Linear Programming formulations for linear ordering problems on graphs\*

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### Abstract

In this paper, we present a new set of constraints for modeling linear ordering problems on graphs using Integer Linear Programming (ILP). These constraints express the membership of a vertex to a prefix rather than the exact position of a vertex in the ordering. We use these constraints to propose new ILP formulations for well-known linear ordering optimization problems, namely the PATHWIDTH, CUTWIDTH, BANDWIDTH, SUMCUT and OPTIMAL LINEAR ARRANGEMENT problems. Our formulations are not only more compact than previous proposals, but also more efficient as shown by our experimental evaluations on large benchmark instances.

## 1 Introduction

Linear ordering problems on graphs refer to optimization problems in which one aim at finding a bijection  $\pi$  from the set V of vertices of the graph to the set of integers  $\{1, 2, \dots, n\}$ , with n = |V|, that minimizes a cost function  $f(G, \pi)$ . The bijective mapping  $\pi$  is called a *linear ordering* and is also known as *linear layout* or simply *layout*, *permutation*, and *linear arrangement*. Examples of such optimization problems are BANDWIDTH, CUTWIDTH and PATHWIDTH.

The Operations Research community has investigated multiple approaches for defining and computing a bijection  $\pi: V \to \{1, \cdots, n\}$  in a mathematical program. In particular, the Constraint Programming (CP) and the Boolean Satisfiability Problem (SAT) communities have defined the all\_different predicate of constraint satisfaction that ensures that the n integer variables  $\{\nu_1, \cdots, \nu_n\}$  are assigned pairwise distinct integers from [1, n], unless some constraints of the problem are violated. Hence, the all\_different predicate models the problem of finding a valid linear ordering for the input graph, assigning each vertex a unique integer (i.e., position)  $\pi(u) = \nu_u$ . We refer to [3, 24, 32, 37-39] for more information on the all\_different predicate.

In this paper, we present a new set of constraints for modeling linear ordering problems on graphs that we use to propose new Integer Linear Programming (ILP) formulations for some linear ordering optimization problems on graphs, namely the PATHWIDTH, CUTWIDTH, BANDWIDTH, SUMCUT and OPTIMAL LINEAR ARRANGEMENT problems. We will show that these formulations are more efficient than previous proposals, thanks to our new set of constraints.

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Our work shall thus be useful for improving the implementation of the all\_different predicate in various solvers. Indeed, behind the scene, CP/SAT solvers transform the all\_different predicate applied to the set of variables  $\{\nu_1, \dots, \nu_n\}$  into a set of new (binary) variables and constraints (or clauses) to indicate whether  $\nu_u < \nu_v$  or  $\nu_u > \nu_v$ . For instance, if we represent each integer  $\nu_u$  as a bit-vector of size  $l = \lceil \log n \rceil$ , [37] shows how to reformulate the all\_different predicate, applied to the n bit-vectors, using  $O(n^2)$  propositional variables and  $O(n^2 \lceil \log n \rceil)$  clauses ensuring that the n resulting bit-vectors will be pairwise distincts (and so the  $\nu_u$  variables will be pairwise distincts).

This paper is organized as follows. We start in Section 3 with a survey on the sets of variables and constraints that are commonly used to express linear ordering problems. In particular, we present a formulation using variables and constraints expressing the exact position of a vertex in the ordering (Formulation 1), another based on the relative ordering of pairs of vertices (Formulation 3), and a new formulation using variables expressing the membership of a vertex to a prefix (Formulation 2). We also show the relationships between these models. Then, we use these formulations in Section 4 to present ILP formulations for the PATHWIDTH, CUTWIDTH, BANDWIDTH, SUMCUT and OPTIMAL LINEAR ARRANGEMENT problems. Our formulations use generally less variables and constraints than previous proposals for the same problems. After, in Section 5, we conduct an experimental evaluation of our ILP formulations using large benchmark instances, and we compare their performances with respect to other formulations found in the literature. We will show that formulations based on the membership of a vertex to a prefix are much more efficient than other proposals. Finally, we conclude this paper in Section 6 with a discussion on possible directions for future studies.

## 2 Notations and definitions

All graphs considered in this paper are simple, connected and loopless. A graph G = (V, E) has n = |V| vertices and m = |E| edges. For any set  $S \subseteq V$ , we let  $N_G(S)$  be the set of vertices in  $V \setminus S$  that have a neighbor in S. The neighborhood of a vertex  $u \in V$  is denoted  $N_G(u)$  and its degree  $\deg_G(u) = |N_G(u)|$ . The maximum degree of the graph is denoted  $\Delta_G = \max_{u \in V} \deg_G(u)$ . We omit the subscript when there is no ambiguity. We denote uv the edge between vertices u and v, and u and v are called the *endpoints* of edge uv. We denote G[S] the subgraph of G = (V, E) induced by  $S \subseteq V$ , i.e., such that  $V_{G[S]} = S$  and  $E_{G[S]} = \{uv \mid uv \in E \text{ and } u, v \in S\}$ .

A linear ordering (or layout) of a graph G=(V,E) is a bijection  $\pi:V\to [1,n]=\{1,2,\cdots,n\}$ , with n=|V|. So,  $\pi(u)$  is the position (or index) of vertex u in the linear ordering  $\pi$ , and  $\pi^{-1}(i)$  is the vertex with position i in  $\pi$ . We denote  $\Pi(V)$  the set of all permutations of V and so of all possible linear orderings for G. As in [5], we denote  $\pi_{<,v}$  the set of vertices that appear before vertex v in the ordering, and so  $\pi_{<,v}=\{u\in V\mid \pi(u)<\pi(v)\}$ . We define similarly  $\pi_{<,v}, \pi_{>,v}$ , and  $\pi_{\geq,v}$ , and we write  $\pi_{*,i}$  instead of  $\pi_{*,\pi^{-1}(i)}$  for each operator  $*\in \{<,\leq,\geq,>\}$ .

We now define some measures on a linear ordering  $\pi \in \Pi(V)$  of G = (V, E). The cardinality of the edge-cut at position i in the ordering  $\pi$  is defined as  $\theta(\pi, i) = |\{uv \in E \mid u \in \pi_{\leq, i} \land v \in \pi_{>i}\}|$ , and the cardinality of the modified edge-cut at position i as  $\zeta(\pi, i) = |\{uv \in E \mid u \in \pi_{\leq, i} \land v \in \pi_{>i}\}|$ . The cardinality of the vertex-cut at position i is  $|N(\pi_{\leq, i})|$ . We also define the length of edge uv in the linear ordering  $\pi$  as  $\lambda(\pi, uv) = |\pi(u) - \pi(v)|$ .

Using above definitions, we are now ready to give the definition, as linear ordering problems, of the optimization problems on graphs that are considered in this paper. Given a graph G = (V, E), each of these optimization problems asks to find a linear ordering  $\pi \in \Pi(V)$ 

minimizing a particular cost function  $f(G,\pi)$ , and so the optimum value for an optimization problem is  $f(G) = \min_{\pi \in \Pi(V)} f(G, \pi)$ . We summarize in Table 1 the cost function of each of these optimization problems, as well as the notations for the optimal values.

Problem name	Optimum	Cost function
Pathwidth	pw(G)	$\max_{i=1}^n  N(\pi_{\leq,i}) $
Ситwidth	cw(G)	$\max_{i=1}^n \theta(\pi,i)$
Modified Cutwidth	mcw(G)	$\max_{i=1}^n \zeta(\pi,i)$
Bandwidth	bw(G)	$\max_{uv \in E} \lambda(\pi, uv)$
OPTIMAL LINEAR ARRANGEMENT	ola(G)	$\sum_{uv \in E} \lambda(\pi, uv) = \sum_{i=1}^{n} \theta(\pi, i)$
SUMCUT	$\mathrm{sc}(G)$	$\sum_{i=1}^n  N(\pi_{\leq,i}) $
Profile	pr(G)	$\sum_{u \in V} \max \left\{ 0, \pi(u) - \min_{v \in N(u)} \pi(v) \right\}$

Table 1: Graph linear ordering optimization problems and associated cost functions.

The optimization problems presented in Table 1 are well known to be NP-complete for general graphs [12, 16, 17, 30], and we refer to [30] for a recent state-of-the-art survey on the complexity of these problems on particular graph classes. Notice that the Profile and the SumCut problems are known to be equivalent and so we have sc(G) = pr(G). This result follows from the fact that a vertex u belongs to  $\max\{0, \max_{v \in N(u)} \pi(u) - \pi(v)\}$  sets  $N(\pi_{\leq,i})$ . The SumCut problem is also known to be equivalent to the Minimum Interval Graph COMPLETION problem which asks for the minimum cardinality set of edges F such that the graph  $G' = (V, E \cup F)$  is an interval graph. Moreover, the OPTIMAL LINEAR ARRANGEMENT problem is also known as the MINIMUM LINEAR ARRANGEMENT problem.

#### 3 Linear ordering constraints

In this section, we present several approaches for modeling a linear ordering problem on graph using integer linear programing. These formulations will be used in Section 4 for modeling the linear ordering optimization problems on graphs defined in Section 2 with ILPs.

A classical method for modeling a linear ordering problem (or the all\_different predicate) using an ILP is Formulation 1 which has been used by many authors for modeling various linear ordering optimization problems on graphs. For instance, it has been used for the BANDWIDTH [26,31], CUTWIDTH [26,28], PATHWIDTH [20], and OPTIMAL LINEAR ARRANGE-MENT [1, 2, 29, 34] problems.

## Formulation 1

$$\sum_{i=1}^{n} a_{u}^{i} = 1 \qquad \forall u \in V$$

$$\sum_{u \in V} a_{u}^{i} = 1 \qquad \forall i \in [1, n]$$

$$\tag{1a}$$

$$\sum_{u \in V} a_u^i = 1 \qquad \forall i \in [1, n] \tag{1b}$$

where binary variable  $a_u^i = 1$  if  $\pi(u) = i$  and 0 otherwise.

Constraint (1a) ensures that vertex u is assigned a single position and Constraint (1b) ensures that position i is assigned to a single vertex. When  $a_u^i = 1$ , we have  $\sum_{j=1}^n j \cdot a_u^j = i \cdot a_u^i = i$ . So, the linear ordering  $\pi \in \Pi(V)$  yielded by Formulation 1 is such that  $\pi(u) = \sum_{i=1}^n i \cdot a_u^i$ . Formulation 1 uses  $n^2$  binary variables and 2n constraints

The next formulation uses binary variables encoding the membership of a vertex to  $\pi_{\leq,i}$ .

## Formulation 2

$$x_u^i \le x_u^{i+1} \qquad \forall u \in V, \ \forall i \in [1, n-1] \tag{2a}$$

$$x_u^i \le x_u^{i+1} \qquad \forall u \in V, \ \forall i \in [1, n-1]$$
 
$$\sum_{u \in V} x_u^i = i \qquad \qquad \forall i \in [1, n]$$
 (2a)

where binary variable  $x_u^i = 1$  if  $\pi(u) \leq i$  and 0 otherwise.

Constraints (2a) and (2b) ensure that all vertices get different positions. Indeed, Constraint (2a) ensures that as soon as  $x_u^i = 1$ , then  $x_u^j = 1$  for all  $j \in [i+1, n]$ . Also, if  $\pi(u) = i$ , we have  $\sum_{j=1}^{n} x_u^j = \sum_{j=i}^{n} x_u^j = n-i+1$ . Furthermore, Constraint (2b) ensures that i vertices are assigned a position in [1,i], i.e.,  $|\pi_{\leq,i}| = |\{u \in V \mid \pi(u) \leq i\}| = i$ . Consequently, Formulation 2 yields a linear ordering  $\pi \in \Pi(V)$  such that  $\pi(u) = n + 1 - \sum_{i=1}^{n} x_{i}^{i}$ . Formulation 2 uses  $n^2$  binary variables and  $n^2$  constraints.

To the best of our knowledge, Formulation 2 has only been used in [35] (actually a variant in which Constraint (2a) is replaced with " $x_u^i \leq x_u^j$  for all  $u \in V$  and  $1 \leq i < j \leq n$ " and so using  $O(n^3)$  constraints) to propose an ILP formulation for the so-called lightpath reconfiguration problem in optical networks. This problem is equivalent to the Vertex Separation problem in directed graphs [8–11], and so to the PATHWIDTH problem in undirected graphs [22].

Another approach for obtaining a linear ordering is to use the relative ordering of pairs of vertices as follows.

## Formulation 3

100

105

$$\alpha_{u,v} + \alpha_{v,u} = 1 \qquad \forall u, v \in V$$
 (3a)

$$\alpha_{u,v} + \alpha_{v,w} - \alpha_{u,w} \le 1 \qquad \forall u, v, w \in V$$
 (3b)

where binary variable  $\alpha_{u,v} = 1$  if  $\pi(u) < \pi(v)$  and 0 otherwise.

Constraints (3a) and (3b) ensure that all vertices get different positions. Indeed, Constraint (3a) ensures that each pair of vertices is ordered, and Constraint (3b) ensures the transitivity between variables and so a total ordering, i.e., if  $\pi(u) < \pi(v)$  and  $\pi(v) < \pi(w)$ then  $\pi(u) < \pi(w)$ . Now observe that if  $\pi(u) = i$ , i-1 vertices are positioned before u and so  $\sum_{v\in V|v\neq u} \alpha_{v,u}=i-1$ . Hence, Formulation 3 yields a linear ordering  $\pi\in\Pi(V)$  such that  $\pi(u) = 1 + \sum_{v \in V | v \neq u} \alpha_{v,u}$ . Formulation 3 uses  $n^2$  binary variables and  $O(n^3)$  constraints.

Formulation 3 has been used to propose an ILP formulation for the TREEWIDTH problem using  $O(n^3)$  binary variables and  $O(n^3)$  constraints [23] (see [14] for more details on this formulation). It has also been used in [25] to obtain an ILP formulation for the CUTWIDTH problem using  $O(n^4)$  variables and  $O(n^4)$  constraints. ILP formulations for the MINIMUM LINEAR AR-RANGEMENT problem using  $O(n^2)$  variables and  $O(n^3)$  constraints can be found in [34]. We also refer to [18, 19] and references therein for more insight on Formulation 3.

**Relationships between formulations.** Observe that given the assignment of the variables  $a_u^i$  provided by Formulation 1, we can deduce an assignment of the variables  $x_u^i$  of Formulation 2 using  $x_u^i = \sum_{j=1}^i a_u^j$ . Similarly, we can deduce an assignment of the variables  $a_u^i$  from the assignment of the variables  $x_u^i$  provided by Formulation 2 using  $a_u^1 = x_u^1$  and  $a_u^k = x_u^k - x_u^{k-1}$ , with  $k \in [2, n]$ .

Now, given an assignment of the variables  $\alpha_{u,v}$  provided by Formulation 3 we can construct an assignment of the variables  $x_u^i$ . Indeed, we have  $x_u^i = 1$  if  $\sum_{v \in V \mid v \neq u} \alpha_{v,u} < i$ , i.e., if at most i-1 vertices are positioned before u in  $\pi$ . Also, introducing intermediate variables  $p_u = 1 + \sum_{v \in V \mid v \neq u} \alpha_{v,u}$  storing the position of u, we have  $x_u^i = 1$  if  $i+1-p_u>0$  and 0 otherwise, and so we use the constraint  $i \cdot x_u^i \geq i+1-p_u$ , for all  $u \in V$  and  $i \in [1,n]$ , combined with the constraint  $\sum_{u \in V} \sum_{i=1}^n x_u^i = n(n+1)/2$ . Conversely, given an assignment of the variables  $x_u^i$  provided by Formulation 2 we can obtain an assignment of the variables  $\alpha_{u,v}$ . Again, we use intermediate variables  $p_u = n+1-\sum_{i=1}^n x_u^i$  to store the position of u, and we use the constraint  $n \cdot \alpha_{u,v} \geq p_v - p_u$  combined with  $\sum_{v,v \in V \mid u \neq v} \alpha_{u,v} = n(n-1)/2$ .

In Table 2, we summarize the formulations of some operations that will be useful in the next sections for modeling linear ordering optimization problems on graphs with respectively Formulations 1 to 3. We observe that some operations that are easy to model with one formulation are more complex with another formulation. For instance, it is easy to test if  $\pi(u) < \pi(v)$  with Formulation 3 (it suffices to check whether variable  $\alpha_{u,v} = 1$  or not) while Formulations 1 and 2 require to sum 2n variables. On the other hand, with Formulation 2 it suffices to check whether variable  $x_u^i = 1$  or not to know if  $u \in \pi_{\leq,i}$ , while Formulation 1 requires to sum i variables and Formulation 3 n variables.

		Formulation 1	Formulation 2	Formulation 3
$\pi(u)$	is	$\sum_{i=1}^{n} i \cdot a_u^i$	$n+1-\sum_{i=1}^{n} x_u^i$	$\sum_{v \in V} \alpha_{v,u}$
$\pi(u) - \pi(v)$	is	$\sum_{i=1}^{n} i \cdot (a_u^i - a_v^i)$	$\sum_{i=1}^{n} (x_v^i - x_u^i)$	$\sum_{w \in V \setminus \{u\}} \alpha_{w,u} - \sum_{w \in V \setminus \{v\}} \alpha_{w,v}$
$\pi(u) < \pi(v)$	True if	$\sum_{i=1}^{n} i \cdot (a_v^i - a_u^i) > 0$	$\sum_{i=1}^{n} (x_u^i - x_v^i) > 0$	$\alpha_{u,v} = 1$
$\pi(u) = i$	True if	$a_u^i = 1$	$x_u^i - x_u^{i-1} = 1$	$\sum_{v \in V} \alpha_{v,u} = i$
$\pi(u) \le i$	True if	$\sum_{j=1}^{i} a_u^j = 1$	$x_u^i = 1$	$\sum_{v \in V} \alpha_{v,u} \le i$
$\pi(u) \le i < \pi(v)$	True if	$\sum_{j=1}^{i} (a_u^j - a_v^j) = 1$	$x_u^i - x_v^i = 1$	$\begin{cases} \sum_{w \in V \setminus \{u\}} \alpha_{w,u} \le i - 1\\ \sum_{w \in V \setminus \{v\}} \alpha_{w,v} \ge i \end{cases}$

Table 2: Useful operations when using the variables of Formulations 1 to 3.

## 4 ILP formulations for graph linear ordering optimization problems

In this section, we present ILP formulations for several linear ordering optimization problems on graphs, based on the formulations presented in Section 3. We summarize in Table 3 the number of variables and constraints in each of these formulations, as well as previously proposed formulations.

				F	ormulati	on 1	Fo	ormulatio	on 2	F	ormulati	on 3
	Ref.	#var.	# constr.		# var.	# constr.		#var.	# constr.		#var.	# constr.
	[13, 20]	$O(n^2m)$	$O(n^2m)$									
Ратнуиртн	[4]	O(nm)	O(nm)	PW1	$O(n^2)$	O(nm)	PW2	$O(n^2)$	O(nm)	PW3	$O(n^2)$	$O(n^3)$
	[35]	$O(n^2)$	$O(n^3)$									
Ситwidth	[26]	$O(n^2m)$	$O(n^2m)$	CW1	O(nm)	O(nm)	CW2	O(nm)	O(nm)	CW3	O(nm)	$O(n^3)$
COTWIDTH	[25]	$O(n^3)$	$O(n^3)$	CW'1	$O(n^2)$	$O(n^2)$	CW'2	$O(n^2)$	$O(n^2)$	CWS	O(mm)	O(n )
	[26]	$O(n^2m)$	$O(n^2m)$									
Bandwidth	[4]	$O(n^2)$	O(nm)	BW1	$O(n^2)$	O(n+m)	BW2	$O(n^2)$	$O(n^2)$	BW3	$O(n^2)$	$O(n^3)$
	[31]	$O(n^2)$	O(n+m)									
SUMCUT				SC1	$O(n^2)$	O(n+m)	SC2	$O(n^2)$	$O(n^2)$	SC3	$O(n^2)$	$O(n^3)$
Profile				PR1	$O(n^2)$	O(n+m)	PR2	$O(n^2)$	$O(n^2)$	PR3	$O(n^2)$	$O(n^3)$
	[2]	$O(n^4)$	$O(n^3)$	OLA1	$O(n^2)$	O(n+m)	OLA2	$O(n^2)$	$O(n^2)$	OLA3	$O(n^2)$	$O(n^3)$
Opt. Lin. Arr.	[6]	$O(n^2)$	$O(n^2m)$	OLA'1	O(nm)	O(nm)	OLA'2	O(nm)	O(nm)	OLA'3	O(nm)	$O(n^3)$
	[1, 29]	$O(n^2)$	$O(n^3)$	OLA"1	$O(n^2)$	$O(n^2)$	OLA"2	$O(n^2)$	$O(n^2)$			

Table 3: Comparison of the number of variables and constraints of the ILP formulations.

#### 4.1 Pathwidth

Given a graph G = (V, E), the PATHWIDTH problem asks to find a linear ordering  $\pi \in \Pi(V)$  that minimizes  $\max_{i=1}^n |\{u \in V \mid \exists uv \in E \text{ such that } \pi(u) < i \leq \pi(v)\}| = \max_{i=1}^n |N(V \setminus \pi_{<,i})| =$  $\max_{i=1}^n |N(\pi_{\leq,i})|$ . The optimal value of this problem is  $\operatorname{pw}(G) = \min_{\pi \in \Pi(G)} \max_{i=1}^n |N(\pi_{\leq,i})|$ .

Several ILP formulations for the PATHWIDTH problem have already been proposed. The formulation presented in [13,20] is based on Formulation 1, and it uses overall  $O(n^2m)$  variables and constraints. Indeed, it uses  $n^2$  binary variables per edge  $uv \in E$  (i.e.,  $y_{uv}^{k,l} = 1$  if  $a_u^k = 1$  and  $a_v^l = 1$ ), and  $n^2$  additional binary variables are introduced to identify the vertices in  $N(\pi_{\leq,i})$ . The formulation proposed in [4] is based on the representation of a graph as an interval graph. Also, it associates to each vertex an interval and every edge forces the intervals of its two endpoints to intersect. The objective is to minimize the maximum number of intervals that intersect at any given point. This formulation uses O(nm) variables and constraints. The formulation proposed in [35] is based on the variant of Formulation 2 we have discussed in Section 2, and uses  $O(n^2)$  variables and  $O(n^3)$  constraints. It is similar to Formulation 4.

To model the PATHWIDTH problem as an ILP, we need a set of constraints to measure  $|N(\pi_{\leq,i})|$ . To do so, we introduce variable  $y_u^i=1$  if  $u\in\pi_{>,i}$  and at least one neighbor v of u is in  $\pi_{\leq,i}$ , and 0 otherwise. In other words,  $y_u^i = 1$  if  $u \in N(\pi_{\leq,i})$ . We can thus write the following

Formulation 4 Pathwidth: Minimize p subject to either Constraints (1a) and (1b) or Constraints (2a) and (2b) and

$$\tau(u, v, i) \le y_u^i \qquad \forall u \in V, \ \forall v \in N(u), \ \forall i \in [1, n]$$
(4a)

$$\tau(u, v, i) \le y_u^i \qquad \forall u \in V, \ \forall v \in N(u), \ \forall i \in [1, n]$$

$$\sum_{u \in V} y_u^i \le p \qquad \qquad \forall i \in [1, n]$$
(4a)
$$(4b)$$

where  $y_u^i = 1$  if  $u \in N(\pi_{\leq,i})$ , and 0 otherwise, and  $\tau(u,v,i)$  is either  $\sum_{i=1}^i (a_v^j - a_u^j)$  or  $x_v^i - x_u^i$ when using respectively the variables of Formulations 1 and 2.

With Constraint (4a) we identify the vertices in  $\pi_{>,i}$  that are also in  $N(\pi_{<,i})$ . Indeed, if  $u \in \pi_{>,i}$ , then  $\pi(u) > i$  and so  $\sum_{j=1}^{i} a_u^j = 0$  (resp.  $x_u^i = 0$ ). If furthermore  $v \in N(u)$  is such that  $v \in \pi_{\leq,i}$ , then  $\sum_{j=1}^{i} a_v^j = 1$  (resp.  $x_v^i = 1$ ) and we have  $y_u^i \geq \sum_{j=1}^{i} a_v^j - \sum_{j=1}^{i} a_u^j = 1$  (resp.  $y_u^i \ge x_v^i - x_u^i = 1$ ). With Constraint (4b) we count the number of vertices in  $N(\pi_{\le,i})$ . The optimal solution of Formulation 4 is pw(G). This formulation adds  $O(n^2)$  variables and O(nm)constraints to the variables and constraints of Formulations 1 and 2.

In the following, we refer to the ILP formulations resulting from Formulation 4 when using the variables and constraints of respectively Formulations 1 and 2 as PW1 and PW2. The sizes of these ILP formulations are reported in Table 3.

Now, when using Formulation 3, we need to introduce  $2n^2$  additional binary variables encoding the membership of a vertex to  $\pi_{\leq,i}$  and to  $\pi_{>,i}$ .

Formulation 5 Pathwidth: Minimize p subject to Constraints (3a), (3b) and (4b) and

$$i - \sum_{w \in V \mid w \neq u} \alpha_{w,u} \le n \cdot l_u^i \qquad \forall u \in V, \ \forall i \in [1, n]$$
 (5a)

$$\sum_{w \in V \setminus \{u\}} \alpha_{w,u} - i + 1 < n \cdot r_u^i \qquad \forall u \in V, \ \forall i \in [1, n]$$

$$l_v^i + r_u^i - 1 \le y_u^i \qquad \forall u \in V, \ \forall v \in N(u), \ \forall i \in [1, n]$$

$$(5b)$$

$$l_v^i + r_u^i - 1 \le y_u^i \qquad \forall u \in V, \ \forall v \in N(u), \ \forall i \in [1, n]$$
 (5c)

where binary variable  $\alpha_{w,u} = 1$  if vertex  $\pi(w) < \pi(u)$  and 0 otherwise, binary variable  $l_u^i = 1$  if  $u \in \pi_{>,i}$ , binary variable  $r_u^i = 1$  if  $u \in \pi_{>,i}$ , and  $y_u^i = 1$  if  $u \in N(\pi_{\le,i})$ , and 0 otherwise.

With the big-M Constraint (5a) we identify the vertices in  $\pi_{\leq,i}$ , with the big-M Constraint (5b) we identify the vertices in  $\pi_{>,i}$ , and with Constraint (5c) we identify the vertices in  $\pi_{>,i}$  that are also in  $N(\pi_{\leq,i})$ . Indeed, if  $u \in \pi_{>,i}$ , then  $\sum_{w \in V \setminus \{u\}} \alpha_{w,u} - i > 0$  and so  $r_u^i = 1$ . If furthermore  $v \in N(u)$  is such that  $v \in \pi_{\leq,i}$ , then  $l_v^i + r_u^i = 2$  and we have  $y_u^i \geq l_v^i + r_u^i - 1 = 1$ . The optimal solution of Formulation 5 is pw(G). This formulation uses  $O(n^2)$  binary variables and  $n^3 + 2n^2 + 2nm + 1 = O(n^3)$  constraints. In the following, we refer to Formulation 5 as PW3.

#### 4.2 Cutwidth

Given a graph G = (V, E), the CUTWIDTH problem asks to find a linear ordering  $\pi \in \Pi(V)$ that minimizes  $\max_{i=1}^n \theta(\pi, i) = \max_{i=1}^n |\{uv \in E \mid \pi(u) \le i < \pi(v)\}|$ , and so the optimal value is  $\operatorname{cw}(G) = \min_{\pi \in \Pi(G)} \max_{i=1}^{n} \theta(\pi, i)$ .

An ILP formulation for the Cutwidth problem has been proposed in [26]. This formulation, based on Formulation 1, uses  $n^2$  binary variables per edge  $uv \in E$  (i.e.,  $y_{uv}^{k,l} = 1$  if  $a_u^k = 1$ and  $a_v^l = 1$ ), and overall it uses  $O(n^2m)$  variables and  $O(n^2m)$  constraints. Another ILP formulation for the CUTWIDTH problem has been proposed in [25]. This formulation is based on Formulation 3. It improves upon the formulation of [26] since it uses  $O(n^3)$  variables and  $O(n^3)$  constraints. We will now present ILP formulations using fewer variables and constraints.

To model the Cutwidth problem as an ILP, we need a set of constraints to measure  $\theta(\pi,i)$ . To do so, a first approach is to introduce variable  $z_{uv}^i=1$  if either  $\pi(u)\leq i<\pi(v)$  or  $\pi(v) \leq i < \pi(u)$ , and 0 otherwise. In other words,  $z_{uv}^i = 1$  if one endpoint of edge uv is in  $\pi_{\leq,i}$ and the other endpoint is in  $\pi_{>,i}$ . We can thus write the following ILP formulation.

Formulation 6 Cutwidth: Minimize c subject to either Constraints (1a) and (1b) or Constraints (2a) and (2b) and:

$$\tau(u, v, i) \le z_{uv}^i \qquad \forall uv \in E, \ \forall i \in [1, n]$$
(6a)

$$\tau(u, v, i) \le z_{uv}^{i} \qquad \forall uv \in E, \ \forall i \in [1, n]$$

$$\tau(v, u, i) \le z_{uv}^{i} \qquad \forall uv \in E, \ \forall i \in [1, n]$$

$$(6a)$$

$$(5b)$$

$$\sum_{uv \in E} z_{uv}^i \le c \qquad \forall i \in [1, n]$$
 (6c)

where  $z_{uv}^i = 1$  if either  $\pi(u) \leq i < \pi(v)$  or  $\pi(v) \leq i < \pi(u)$ , and 0 otherwise, and  $\tau(u,v,i)$  is either  $\sum_{j=1}^{i} (a_v^j - a_u^j)$  or  $x_v^i - x_u^i$  when using respectively the variables of Formulations 1 and 2.

Constraints (6a) and (6b) force variable  $z_{uv}^i$  to 1 if one endpoint of edge uv is in  $\pi_{\leq,i}$  and the other endpoint is in  $\pi_{>,i}$ . With Constraint (6c) we count the number  $\theta(\pi,i)$  of edges in the cut  $(\pi_{<,i},\pi_{>,i})$ . The objective is to minimize the maximum number c of edges in a cut. The optimal solution of Formulation 6 is cw(G). This formulation adds O(nm) variables and O(nm)constraints to the variables and constraints of Formulations 1 and 2. In the following, we refer to the ILP formulations resulting from Formulation 6 when using the variables and constraints of respectively Formulations 1 and 2 as CW1 and CW2. The sizes of these ILP formulations are reported in Table 3.

When using Formulation 3, as in Section 4.1 for Formulation 5, we need to introduce  $2n^2$ additional binary variables  $l_u^i$  and  $r_u^i$  encoding the membership of a vertex to  $\pi_{\leq,i}$  and to  $\pi_{>,i}$ . Also, we get the following ILP formulation.

Formulation 7 Cutwidth: Minimize c subject to Constraints (3a), (3b), (5a), (5b) and (6c) and:

$$l_u^i + r_v^i - 1 \le z_{uv}^i \qquad \forall uv \in E, \ \forall i \in [1, n]$$
 (7a)

$$\begin{aligned} l_u^i + r_v^i - 1 &\leq z_{uv}^i & \forall uv \in E, \ \forall i \in [1, n] \\ l_v^i + r_u^i - 1 &\leq z_{uv}^i & \forall uv \in E, \ \forall i \in [1, n] \end{aligned} \tag{7a}$$

where  $\alpha_{w,u} = 1$  if vertex  $\pi(w) < \pi(u)$  and 0 otherwise,  $l_u^i = 1$  if  $u \in \pi_{\leq,i}$ ,  $r_u^i = 1$  if  $u \in \pi_{>,i}$ , and  $z_{uv}^i = 1$  if either  $\pi(u) \leq i < \pi(v)$  or  $\pi(v) \leq i < \pi(u)$ , and 0 otherwise.

With the big-M Constraints (5a) and (5b) we identify the vertices in  $\pi_{<,i}$  and  $\pi_{>,i}$ , and with Constraints (7a) and (7b) we identify edges in the cut  $(\pi_{\leq,i},\pi_{>,i})$ . With Constraint (6c) we count the number  $\theta(\pi,i)$  of edges in the cut  $(\pi_{\leq,i},\pi_{>,i})$ . The objective is to minimize the maximum number c of edges in a cut. Formulation 7 uses O(nm) binary variables and  $O(n^3)$ constraints. In the following, we refer to Formulation 7 as CW3. This formulation is similar to the formulation proposed in [25] but uses slightly less variables and constraints.

Another approach for measuring  $\theta(\pi,i)$  is based on the observation that the difference between the edge-cuts  $(\pi_{\leq,i-1},\pi_{>,i-1})$  and  $(\pi_{\leq,i},\pi_{>,i})$  is the removal of the edges incident to vertex  $u = \pi^{-1}(i)$  and with one endpoint in  $\pi_{\leq,i-1}$  (i.e., the edge-cut  $(\pi_{\leq,i-1},\{u\})$ ), and the addition of the edges incident to vertex u and with one endpoint in  $\pi_{>,i}$  (i.e., the edge-cut  $(\{u\},\pi_{>,i})$ ). Also, we have  $\theta(\pi, i) = \theta(\pi, i - 1) - |(\pi_{\leq, i-1}, \{u\})| + |(\{u\}, \pi_{>, i})| = \theta(\pi, i - 1) + \deg(u) - 2$ .  $|(\pi_{\leq,i-1},\{u\})|$ , since  $\deg(u)=|(\pi_{\leq,i-1},\{u\})|+|(\{u\},\pi_{>,i})|$ . Using this observation, we can model the Cutwidth problem as the following ILP.

**Formulation 8** Cutwidth: Minimize c subject to either Constraints (1a) and (1b) or Constraints (2a) and (2b) and:

$$\deg(u) \cdot \omega(u, i) - 2 \sum_{v \in N(u)} \eta(v, i) - 2 \cdot \Delta \cdot (1 - \omega(u, i)) \le \mu^{i} \qquad \forall u \in V, \ \forall i \in [2, n]$$
 (8a)

$$\sum_{u \in V} \deg(u) \cdot \omega(u, 1) = c^1 \tag{8b}$$

$$c^{i-1} + \mu^i = c^i \qquad \forall i \in [2, n] \qquad (8c)$$

$$c^N = 0 (8d)$$

$$c^i \le c$$
  $\forall i \in [1, n]$  (8e)

where variable  $c^i$  is a non-negative integer used to measure the cardinality  $\theta(\pi,i)$  of the edge-cut  $(\pi_{\leq,i},\pi_{>,i})$ , integer variable  $\mu^i$  measures the difference  $\theta(\pi,i)-\theta(\pi,i-1)$ , and either  $\omega(u,i)=a^i_u$  and  $\eta(v,i)=\sum_{j=1}^{i-1}a^j_v$  when using Formulation 1, or  $\omega(u,i)=x^i_u-x^{i-1}_u$  and  $\eta(v,i)=x^{i-1}_v$  when using Formulation 2. In other words,  $\omega(u,i)=1$  when  $\pi(u)=i$ , and  $\eta(v,i)=1$  when  $v\in\pi_{<,i}$ .

We have seen that  $\theta(\pi,i) = \theta(\pi,i-1) + \deg(u) - 2 \cdot |(\pi_{\leq,i-1},\{u\})|$ , when  $u = \pi^{-1}(i)$ . With Constraint (8a) we measure the difference in number of edges with previous position. More precisely, if vertex u is at position i, edges incident to v such that the other endpoint  $v \in N(u)$  has position j < i ends at position i and should no longer be taken into account. We have  $\sum_{v \in N(u)} \eta(v,i)$  such edges that we subtract from previous counting. In addition,  $\deg(u) - \sum_{v \in N(u)} \eta(v,i)$  edges incident to u have an endpoint in  $\pi_{>,i}$ , and so we must add them to the previous counting. Last, we subtract  $2 \cdot \Delta \cdot (1 - \omega(u,i))$  to ensure that if  $\pi(u) \neq i$ , the evaluation of the left-hand side of Constraint (8a) will have no impact on the value of  $\mu^i$ . Then, with Constraints (8b) to (8d) we measure the cardinality  $\theta(\pi,i)$  of the edge-cuts. The objective is to minimize the maximum number c of edges in an edge-cut. Formulation 8 uses  $O(n^2)$  variables and constraints. In the following, we refer to the ILP formulations resulting from Formulation 8 when using the variables and constraints of respectively Formulations 1 and 2 as CW'1 and CW'2.

From above formulations for the CUTWIDTH problem, one can easily model the Modified Cutwidth problem which asks for a linear ordering  $\pi \in \Pi(V)$  minimizing  $\max_{i=1}^n \zeta(\pi,i) = \max_{i=1}^n |\{uv \in E \mid \pi(u) < i < \pi(v)\}|$ . For instance, with Formulation 6, it suffices to use either  $\tau'(u,v,i) = \sum_{j=1}^{i-1} a_v^j - \sum_{j=1}^i a_u^j = \tau(u,v,i) - a_v^i$  or  $\tau'(u,v,i) = x_v^{i-1} - x_u^i$  when using respectively the variables of Formulations 1 and 2. Moreover, with Formulation 7, it suffices to use  $l_u^{i-1} + r_v^i - 1 \le z_{uv}^i$  and  $l_v^{i-1} + r_u^i - 1 \le z_{uv}^i$  instead of Constraints (7a) and (7b).

## 4.3 Bandwidth

Given a graph G = (V, E), the Bandwidth problem asks to find a linear ordering  $\pi \in \Pi(V)$  that minimizes the maximum distance between the endpoints of the edges of G in the linear ordering, i.e.,  $\lambda(\pi, uv) = |\pi(u) - \pi(v)|$ , and so the optimal value is  $\mathrm{bw}(G) = \min_{\pi \in \Pi(V)} \max_{uv \in E} |\pi(u) - \pi(v)|$ . A direct ILP formulation for this problem is as follows.

Formulation 9 BANDWIDTH: Minimize b subject to either Constraints (1a) and (1b), or Constraints (2a) and (2b), or Constraints (3a) and (3b) and

$$\ell(u, v) \le b \qquad \forall uv \in E \tag{9a}$$

$$\ell(v, u) \le b \qquad \forall uv \in E$$
 (9b)

where  $\ell(u,v)$  is either  $\sum_{i=1}^{n} i \cdot (a_u^i - a_v^i)$ , or  $\sum_{i=1}^{n} (x_v^i - x_u^i)$ , or  $\sum_{w \in V \setminus \{u\}} \alpha_{w,u} - \sum_{w \in V \setminus \{v\}} \alpha_{w,v}$  when using respectively the variables of Formulations 1, 2 and 3.

Constraints (9a) and (9b) ensure that the distance between the endpoints of any edge  $uv \in E$ is at most b and the objective is to minimize b. The optimal solution of Formulation 9 is bw(G). This formulation adds O(m) constraints to the constraints of Formulations 1 to 3. In the following, we refer to the ILP formulations resulting from Formulation 9 when using the variables and constraints of respectively Formulations 1 to 3 as BW1, BW2, and BW3. The sizes of these ILP formulations are reported in Table 3.

Formulation BW1 is almost the same as the formulation based on Formulation 1 proposed in [31]. The difference is that [31] introduce integer variables  $p_u = \sum_{i=1}^n i \cdot a_u^i$ , recording the position of vertex u in the linear ordering, and rewrite Constraints (9a) and (9b) as p(u) –  $p(v) \le b$  and  $p(v) - p(u) \le b$ . Another ILP formulation for the BANDWIDTH problem based on Formulation 1 has been proposed in [26]. It uses variable  $y_{uv}^{k,l} = 1$  when  $a_u^k = 1$  and  $a_v^l = 1$ . The goal is to minimize b where  $b \ge |k-l| \cdot y_{uv}^{k,l}$  for all  $uv \in E$  and  $k,l \in [1,n]$ . Overall it uses  $O(n^2m)$  variables and constraints. A different approach has been followed in [4], proposing an ILP formulation based on the representation of a graph as an interval graph. It associates to each vertex an interval and every edge forces the intervals of its two endpoints to intersect. In this formulation, the length of an interval is bounded by a parameter k, and the objective is to find the minimum k for which a feasible solution exists. Hence, this formulation must be solved for  $\log n$  values of k (or  $\mathrm{bw}(G)$  times if using only growing values of k). This formulation uses  $O(n^2)$  variables and O(nm) constraints.

#### 4.4 Profile and Sum Cut

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We have seen in Section 2 that the SumCut, Profile and Minimum Interval Graph Com-PLETION problems are equivalent [12]. Also, in this section we present two main formulations.

First, we obtain ILP formulations for the SUMCUT problem from the ILP formulations for the PATHWIDTH problem. Indeed, the SUMCUT problem asks for a linear ordering  $\pi \in \Pi(V)$  minimizing  $\sum_{i=1}^{n} |N(\pi_{\leq,i})|$ , while the PATHWIDTH problem asks for a linear ordering  $\pi \in \Pi(V)$  minimizing  $\max_{i=1}^{n} |N(\pi_{\leq,i})|$ . Also, it suffices to replace, in Formulations 4 and 5, Constraint (4b) with  $\sum_{i=1}^n \sum_{u \in V} y_u^i \leq p$ . In the following, we refer to the resulting ILP formulations when using the variables and constraints of respectively Formulations 1 to 3 as SC1, SC2, and SC3. The sizes of these ILP formulations are reported in Table 3.

Next, we use the definition of the Profile problem which asks for a linear ordering  $\pi \in \Pi(V)$ of a graph G = (V, E) that minimizes  $\sum_{u \in V} \max \{0, \max_{v \in N(u)} (\pi(u) - \pi(v))\}$ . Let  $d_u$  be an integer variable used to measure the largest distance between u and its neighbor v with the lowest position in  $\pi$  that is also at a lower position than u (i.e., such that  $\pi(v) < \pi(u)$ ). When  $\pi(v) > \pi(u)$  for all  $v \in N(u)$ , we have  $d_u = 0$ . In other words,  $d_u$  measures the number of sets  $\pi_{\leq,i}$  vertex u is a neighbor of. We obtain the following formulation.

Formulation 10 SUMCUT, PROFILE: Minimize s subject to either Constraints (1a) and (1b), or Constraints (2a) and (2b), or Constraints (3a) and (3b) and

$$\ell(u, v) \le d_u \qquad \forall u \in V, \ \forall v \in N(u)$$
 (10a)  
 $0 \le d_u \qquad \forall u \in V$  (10b)

$$0 \le d_u \qquad \forall u \in V \tag{10b}$$

$$\sum_{u \in V} d_u \le s \tag{10c}$$

where integer variable  $d_u$  measures the number of sets  $\pi_{\leq,i}$  vertex u is a neighbor of, and  $\ell(u,v)$ is either  $\sum_{i=1}^{n} i \cdot (a_u^i - a_v^i)$ , or  $\sum_{i=1}^{n} (x_v^i - x_u^i)$ , or  $\sum_{w \in V \setminus \{u\}} \alpha_{w,u} - \sum_{w \in V \setminus \{v\}} \alpha_{w,v}$  when using respectively the variables of Formulations 1, 2 and 3.

With Constraints (10a) and (10b) we measure the value  $d_u = \max \{0, \max_{v \in N(u)} (\pi(u) - \pi(v))\},\$ that is the number of sets  $\pi_{\leq,i}$  vertex u is a neighbor of, and with Constraint (10c) we count the sum of these memberships. The optimal solution of Formulation 10 is sc(G) = pr(G). This formulation adds O(n) integer variables and O(n+m) constraints to the variables and constraints of Formulations 1 to 3.

In the following, we refer to the ILP formulations resulting from Formulation 10 when using the variables and constraints of respectively Formulations 1 to 3 as PR1, PR2, and PR3. The sizes of these ILP formulations are reported in Table 3.

#### 4.5 Optimal linear arrangement

Given a graph G = (V, E), the Optimal Linear Arrangement problem asks for a linear ordering  $\pi \in \Pi(V)$  that minimizes the sum over all edges of the distance between the endpoints of the edges in the linear ordering  $\pi$  for G, and so the optimal value is ola(G) = $\min_{L \in \Pi(V)} \sum_{uv \in E} \lambda(\pi, uv) = \min_{L \in \Pi(V)} \sum_{uv \in E} |\pi(u) - \pi(v)|$ . The decision version of this optimization problem has been proved NP-complete in [15].

Several ILP formulations for the OPTIMAL LINEAR ARRANGEMENT problem, based on Formulation 1, have already been proposed [1,2,6,29,34]. [2] presents two formulations, one using  $O(n^6)$  variables and  $O(n^5)$  constraints and the other using  $O(n^4)$  variables and  $O(n^3)$  constraints. The formulation presented in [6] uses  $O(n^2 + m)$  variables and  $O(n^2 m)$  constraints.

The following formulation is similar to the formulations presented in [29] and that is based on Formulation 1.

Formulation 11 Optimal Linear Arrangement: Minimize o Subject to Constraints (1a) and (1b), or Constraints (2a) and (2b), or Constraints (3a) and (3b) and

$$\ell(u,v) \le d_{uv} \qquad \forall uv \in E \tag{11a}$$

$$\ell(u, v) \le d_{uv} \qquad \forall uv \in E$$
 (11a)  
 $\ell(u, v) \le d_{uv} \qquad \forall uv \in E$  (11b)

$$\sum_{uv \in E} d_{uv} \le o \tag{11c}$$

where integer variable  $d_{uv}$  measure the distance between the endpoints of edge  $uv \in E$ , and  $\ell(u,v)$  is either  $\sum_{i=1}^{n} i \cdot (a_{u}^{i} - a_{v}^{i})$ , or  $\sum_{i=1}^{n} (x_{v}^{i} - x_{u}^{i})$ , or  $\sum_{w \in V \setminus \{u\}} \alpha_{w,u} - \sum_{w \in V \setminus \{v\}} \alpha_{w,v}$  when using respectively the variables of Formulations 1, 2 and 3.

With Constraints (11a) and (11b) we measure the distance  $d_{uv}$  between the endpoints of edge  $uv \in E$ , and with Constraint (11c) we count the sum of these distances. The optimal solution of Formulation 11 is ola(G). This formulation adds O(m) integer variables and O(m) constraints to the variables and constraints of Formulations 1 to 3.

In the following, we refer to the ILP formulations resulting from Formulation 11 when using the variables and constraints of respectively Formulations 1 to 3 as OLA1, OLA2, and OLA3. The sizes of these ILP formulations are reported in Table 3.

As reported in Table 1, we have  $\sum_{uv \in E} \lambda(\pi, uv) = \sum_{i=1}^{n} \theta(\pi, i)$ , and so the optimal value for the Optimal Linear Arrangement problem is also  $\operatorname{ola}(G) = \min_{L \in \Pi(V)} \sum_{i=1}^{n} \theta(\pi, i)$  [12]. Therefore, we can derive another ILP formulation for this problem from the ILP formulations for the CUTWIDTH problem, replacing in Formulations 6 and 7 Constraint (6c) with  $\sum_{i=1}^{n} \sum_{uv \in E} z_{uv}^{i} \leq c$ , and in Formulation 8 Constraint (8e) with  $\sum_{i=1}^{n} c^{i} \leq c$ . We refer to the ILP formulation resulting from the modification of Formulations 6 and 7 as respectively OLA'1, OLA'2, and OLA'3, and to the formulations resulting from the modification of Formulation 8 as OLA"1 and OLA"2.

## <sup>335</sup> 5 Simulations and interpretation of results

In this section, we evaluate the performances of the ILP formulations presented in this paper. We start describing our experimental setting in Section 5.1. Then, we compare all proposed ILP formulations to previous proposals in Section 5.2 on small instances. Finally, in Section 5.3, we evaluate the best formulations for BANDWIDTH, CUTWIDTH and PATHWIDTH using a large data set of graphs.

## 5.1 Experimental setting

We have implemented all the ILP formulations presented in this paper, as well as formulations proposed by others, using the SageMath open-source mathematical software [36] combined with the CPLEX solver [21]. All computations have been performed on a computer equipped with two quad-cores Intel Xeon W5580 CPU operating at 3.20GHz and 64GB of RAM. We have forced the CPLEX solver to operate in sequential mode, setting parameter CPXPARAM\_Threads to 1, and we have used the <code>@parallel</code> function decorator of SageMath to enable the simultaneous resolution of up to 8 instances.

In our experiments, we use two data sets. The first one, Small has already been used for instance in [20, 27, 28, 31] for evaluating ILP formulations and algorithms for CUTWIDTH. This data set consists of 84 graphs introduced in the context of the bandwidth reduction problem. The number of vertices ranges from 16 to 24, and the number of edges ranges from 18 to 49. This data set can be found as part of the CMPLIB [7]. The second one is the  $Rome\ Graphs$  data set [33], that has been introduced by the graph drawing research community. This data set has been used in [4] for the evaluation of ILP formulations for BANDWIDTH and PATHWIDTH. It consists of 11,534 undirected graphs of order  $10 \le n \le 100$ .

In all our experiments, the computation time is limited to 5 minutes (300 seconds). When a problem is not optimally solved within this time limit, we report the relative optimality gap (% gap), that is computed as  $\frac{UB-LB}{UB}$ , where UB is the value of the best found feasible solution (an upper bound) and LB is the best relaxed bound of the ILP (best lower bound for the problem). When the problem is optimally solved, this gap is set to 0.

The source code and the benchmark instances used to conduct our experiments can be found at http://www-sop.inria.fr/members/David.Coudert/code/graph-linear-ordering/.

## 5.2 Experiments with the Small data set

We summarize in Tables 4 to 8, respectively for Pathwidth, Cutwidth, Bandwidth, Sum-Cut and Optimal Linear Arrangement problems, the computational results of each formulations on the graphs of the *Small* data set. Detailed results per graphs can be found in Appendix A. For each problem and each formulation, we indicate the number of graphs of the data set for which the problem is optimally solved, the average of the optimality gaps over all graphs, and the average computation time. Observe that this average computation time is biased since we count 300 seconds for each unsolved instance, independently of its optimality gap (i.e., the same weight is given to an instance with a small optimality gap and to an instance with a large one).

	[4]	[13]	[35]	PW1	PW2	PW3
# opt	17	1	83	78	84	1
% gap	56.0	98.5	0.3	2.3	0.0	84.0
CPU time	258.5	297.5	33.6	56.0	1.7	299.9

Table 4: Pathwidth.

	[25]	[26]	CW1	CW2	CW3	CW'1	CW'2
# opt	1	3	56	84	0	66	68
% gap	94.5	80.3	9.5	0.0	91.8	6.7	8.0
CPU time	298.4	293.8	143.7	3.2	300.0	104.6	96.3

Table 5: Cutwidth.

	[26]	[4]	[31]	[31] + F2	[31] + F3	BW1	BW2	BW3
# opt	37	75	84	84	58	84	84	68
% gap	52.5	2.4	0.0	0.0	11.0	0.0	0.0	5.3
CPU time	198.9	99.5	1.3	1.9	153.1	13.6	2.2	108.2

Table 6: BANDWIDTH.

	SC1	SC2	SC3	PR1	PR2	PR3
# opt	17	65	0	5	35	9
% gap	37.0	1.7	99.6	50.2	13.8	43.5
CPU time	266.0	125.8	300.0	293.3	216.2	285.6

Table 7: SumCut.

	OLA1	OLA2	OLA3	OLA4	OLA5	OLA6	OLA7	OLA8	[31]	[31]+F2	[31]+F3
# opt	34	81	0	0	43	25	0	0	1	29	14
% gap	17.9	0.3	99.2	57.7	11.6	23.8	92.1	94.0	36.6	20.8	33.3
CPU time	218.8	51.7	300.0	300.0	195.7	250.3	300.0	300.0	298.9	234.1	271.4

Table 8: Optimal Linear Arrangement.

We can see from reported results that formulations based on Formulation 2, and more precisely PW2, CW2, BW2, SC2 and OLA2 are among the best formulations, if not the best. On the other hand, the formulations we have presented based on Formulation 3 are not efficient. Indeed, these formulations are able to solve very few instances compared to other proposals.

More specifically, we observe from Table 4 for the PATHWIDTH problem and from Table 5 the CUTWIDTH problem that not only PW2 and CW2 are the only formulations able to solve the problems on all the graphs of the *Small* data set, but also that reported average computation time are between one and two orders of magnitude lower than other formulations. This shows that Formulation 2 is much more suited for these two linear ordering optimization problems than other proposals.

The conclusion is different for the BANDWIDTH problem. In Table 6, formulations [31]+F2 and [31]+F3 are straightforward modifications of the formulation proposed in [31] to use the variables and constraints of respectively Formulations 2 and 3. Here, four formulations are able to solve the problem on all the graphs of the *Small* data set, and the fastest one is the formulation proposed in [31], relying on Formulation 1. In particular, we can observe the significant speedup of [31] over BW1 thanks to the introduction of integer variables recording the position of a vertex in the linear ordering. These variables offer fewer improvement for the formulations based on Formulation 2 (BW2 compared to [31]+F2), and are not helpful at all for the formulations based on Formulation 3. Although the formulation proposed in [31] has better performances than BW2 in this experiment, we will see in Section 5.3 that there is actually no clear winner between [31], [31]+F2 and BW2.

For the SumCut problem, formulation SC2 is not able to solve all instances within the specified time limit. However, it allows us to solve significantly more instances than using other formulations. Similarly, formulation OLA2 is the best available formulation for the Optimal Linear Arrangement problem, although some instances (3) were not solved. Note that in Table 8, formulations [31], [31]+F2, and [31]+F3 are straightforward adaptations of the formulations OLA1, OLA2 and OLA3 with the introduction of integer variables recording the position of a vertex in the linear ordering.

## 5.3 Experiments with the Rome Graphs data set

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In this section we evaluate the best formulations for the Bandwidth, Cutwidth and Pathwidth problems on the  $Rome\ Graphs$  data set. More precisely, we report in Figure 1a the cumulative number of graphs for which optimal solutions are obtained using formulations PW2, CW2, BW2, [31] and [31]+F2, and in Figure 1b the average optimality gap of the unsolved instances. As in [4], we ordered the graphs by increasing size n+m (number of nodes + number of edges) and ran computations starting from the smallest. Then, as soon as 400 consecutive instances in this order produced timeouts, we stop computations for the formulation and evaluated only the so far obtained results. This explains why the plots have different lengths. We also report in Table 9, for each of these models, the total number and the percentage of solved instances of the  $Rome\ Graphs$  data set (which contains 11,534 graphs), as well as the size of the last solved instance (which is also the largest solved).

	BW2	[31]	[31]+F2	CW2	PW2
# solved	4,568	4,603	4,681	5,683	5,615
% solved	39.6	39.9	40.6	49.3	48.7
Larger solved $(n+m)$	124=53+71	137=63+74	132 = 56 + 76	149=64+85	142=61+81

Table 9: Total number and percentage of solved instances of the Rome Graphs data set.

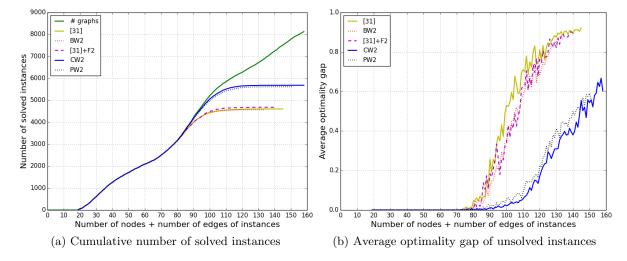


Figure 1: Cumulative number of solved instances and average optimality gap of unsolved instances of the Rome set of graphs for BANDWIDTH (Formulations [31], [31]+F2, and BW2), CUTWIDTH (CW2), and PATHWIDTH (PW2).

We observe from Table 9 and Figure 1a that the three models for the BANDWIDTH problem offer very similar performances on this data set with only 1% difference in the number of solved instances. As opposed to the results reported in Section 5.2 for the *Small* data set, here formulation [31]+F2 allows to solve slightly more instances than other models. Furthermore, we observe from Figure 1b that the average optimality gap of unsolved instances is lower for that formulation as well. This suggest that formulation [31]+F2 is asymptotically better than the other ones. In other words, longer computation times could lead to larger differences.

Concerning the CUTWIDTH and PATHWIDTH problems, we are able to solve almost all graphs such that n+m < 90, but very few with n+m > 120 within given time limit. This is a great improvement over [4] for PATHWIDTH. Indeed, the results reported in [4] for PATHWIDTH indicate that optimal solutions were obtained for only 17% of the instances of the *Rome Graphs* data set, solving almost all small graphs (n+m < 45) and almost no graphs with n+m > 70. Although such comparison lacks of fairness (different implementations, but comparable hardware), this confirm the results reported in Table 4 when using the *Small* data set.

## 6 Conclusion

In this paper we have presented different formulations for modeling linear ordering problems on graphs using integer linear programming. We have in particular proposed a new building block (Formulation 2) using variables expressing the membership of a vertex to a prefix rather than variables expressing the exact position of a vertex in the ordering (Formulation 1), or variables expressing a relative ordering (Formulation 3). Moreover, we have presented ILP formulations using less variables and contraints than other proposals. Then, we have compared these formulations using large benchmark instances. Our experiments show that Formulation 2 is very well suited for solving the Cutwidth and Pathwidth problems, and that it is also a good competitor for the Bandwidth problem. The performances of our formulations could certainly be improved with the addition of appropriate constraints (e.g., cutset inequalities).

We believe that Formulation 2 could help designing faster ILP formulations and branchand-bound algorithms for solving various optimization problems in which a linear ordering of the vertices of a graph is required. In particular, it is straightforward to modify the ILP formulations presented in this paper for solving similar linear ordering optimization problems on directed graphs (e.g., VERTEX SEPARATION). Moreover, our work shall help improving the implementation of the all\_different predicate in CP/SAT solvers.

## References

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- [1] A. R. Amaral. On the exact solution of a facility layout problem. European Journal of Operational Research, 173(2):508 518, 2006.
- [2] A. R. Amaral. A mixed 0-1 linear programming formulation for the exact solution of the minimum linear arrangement problem. *Optimization Letters*, 3(4):513–520, 2009.
- [3] G. Appa, D. Magos, and I. Mourtos. LP relaxations of multiple all\_different predicates. In J.-C. Régin and M. Rueher, editors, *Integration of AI and OR Techniques in Constraint Programming for Combinatorial Optimization Problems*, volume 3011 of *Lecture Notes in Computer Science*, pages 364–369. Springer Berlin Heidelberg, 2004.
- [4] T. C. Biedl, T. Bläsius, B. Niedermann, M. Nöllenburg, R. Prutkin, and I. Rutter. Using ILP/SAT to determine pathwidth, visibility representations, and other grid-based graph drawings. In *Graph Drawing*, volume 8242 of *LNCS*, pages 460–471. Springer, 2013.
  - [5] H. L. Bodlaender, F. V. Fomin, A. M. Koster, D. Kratsch, and D. M. Thilikos. A note on exact algorithms for vertex ordering problems on graphs. *Theory Comput. Syst.*, 50(3):420–432, 2012.
- [6] A. Caprara, A. N. Letchford, and J.-J. Salazar-González. Decorous lower bounds for minimum linear arrangement. *INFORMS Journal on Computing*, 23(1):26–40, 2011.
  - [7] CMPLIB. http://www.optsicom.es/cutwidth/.
  - [8] N. Cohen, D. Coudert, D. Mazauric, N. Nepomuceno, and N. Nisse. Tradeoffs in process strategy games with application in the WDM reconfiguration problem. *Theoretical Computer Science*, 412(35):4675–4687, 2011.
  - [9] D. Coudert, F. Huc, D. Mazauric, N. Nisse, and J.-S. Sereni. Reconfiguration of the routing in WDM networks with two classes of services. In *Optical Network Design and Modeling (ONDM)*, pages 1–6. IEEE, 2009.
- [10] D. Coudert, S. Perennes, Q.-C. Pham, and J.-S. Sereni. Rerouting requests in WDM networks. In *Proc. AlgoTel*, pages 17–20, 2005.
  - [11] D. Coudert and J.-S. Sereni. Characterization of graphs and digraphs with small process number. *Discrete Applied Mathematics*, 159(11):1094–1109, 2011.
  - [12] J. Díaz, J. Petit, and M. Serna. A survey on graph layout problems. *ACM Computing Surveys*, 34(3):313–356, 2002.
- [13] A. Duarte, L. F. Escudero, R. Martí, N. Mladenovic, J. J. Pantrigo, and J. Sánchez-Oro. Variable neighborhood search for the vertex separation problem. *Computers & Operations Research*, 39(12):3247–3255, 2012.
  - [14] M. Ganardi. Matching-based algorithms for computing treewidth. Master's thesis, Lehrune Forschungsgebeit Disktrete Optimierung, RWTH Aachen, 2012.

- [15] M. Garey, D. Johnson, and L. Stockmeyer. Some simplified NP-complete graph problems. Theoretical Computer Science, 1(3):237 – 267, 1976.
  - [16] M. R. Garey, R. L. Graham, D. S. Johnson, and D. E. Knuth. Complexity results for bandwidth minimization. SIAM Journal on Applied Mathematics, 34(3):477–495, 1978.
- [17] M. R. Garey and D. S. Johnson. Computers and intractability. W. H. Freeman and Co.,
   San Francisco, Calif., 1979. A guide to the theory of NP-completeness, A Series of Books in the Mathematical Sciences.
  - [18] M. Grötschel, M. Jünger, and G. Reinelt. A cutting plane algorithm for the linear ordering problem. *Operations Research*, 32(6):1195–1220, 1984.
- [19] M. Grötschel, M. Jünger, and G. Reinelt. Facets of the linear ordering polytope. *Mathematical Programming*, 33(1):43–60, 1985.
  - [20] F. Gurski. Linear programming formulations for computing graph layout parameters. *The Computer Journal*, 2015.
  - [21] IBM ILOG. CPLEX Optimization Studio 12.6.2. http://www-01.ibm.com/software/integration/optimization/cplex-optimizer/.
- [22] N. G. Kinnersley. The vertex separation number of a graph equals its pathwidth. *Information Processing Letters*, 42(6):345–350, 1992.
  - [23] A. M. C. A. Koster. ILP formulation for treewidth. private communication.
  - [24] J. Lee. All-different polytopes. Journal of Combinatorial Optimization, 6(3):335–352, 2002.
- [25] M. C. López-Locés, N. Castillo-García, H. J. Fraire H., P. Bouvry, J. E. Pecero, R. A. Pazos Rangel, J. J. G. Barbosa, and F. Valdez. A new integer linear programming model for the cutwidth minimization problem of a connected undirected graph. In O. Castillo, P. Melin, W. Pedrycz, and J. Kacprzyk, editors, Recent Advances on Hybrid Approaches for Designing Intelligent Systems, volume 547 of Studies in Computational Intelligence, pages 509–517. Springer, 2014.
- [26] J. Luttamaguzi, M. J. Pelsmajer, Z. Shen, and B. Yang. Integer programming methods for several optimization problems in graph theory. In G. Hu, editor, 20th International Conference on Computers and Their Applications (CATA), pages 50–55. ISCA, Mar. 2005.
- [27] R. Martí, V. Campos, and E. Piñana. A branch and bound algorithm for the matrix bandwidth minimization. *European Journal of Operational Research*, 186(2):513 528, 2008.
  - [28] R. Martí, J. J. Pantrigo, A. Duarte, and E. G. Pardo. Branch and bound for the cutwidth minimization problem. *Computers & Operations Research*, 40(1):137 149, 2013.
  - [29] M. Moeini, S. Gueye, and S. Michel. A new mathematical model for the minimum linear arrangement problem. In B. Vitoriano, E. Pinson, and F. Valente, editors, 3rd International Conference on Operations Research and Enterprise Systems (ICORES), pages 57–62. SciTePress, Mar. 2014.

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[30] J. Petit. Addenda to the survey of layout problems. Bulletin of the European Association for Theoretical Computer Science, (105):177–201, Oct. 2011.

- [31] E. Piñana, I. Plana, V. Campos, and R. Martí. GRASP and path relinking for the matrix bandwidth minimization. European Journal of Operational Research, 153(1):200 210, 2004.
  - [32] J. Régin. A filtering algorithm for constraints of difference in CSPs. In B. Hayes-Roth and R. E. Korf, editors, 12th National Conference on Artificial Intelligence (AAAI), volume 1, pages 362–367. AAAI Press / The MIT Press, 1994.
- [33] Rome Graphs. http://www.graphdrawing.org/download/rome-graphml.tgz.
  - [34] H. Seitz. Contributions to the Minimum Linear Arrangement Problem. PhD thesis, Heidelberg University, Apr. 2010.
  - [35] F. Solano and M. Pióro. Lightpath reconfiguration in WDM networks. *IEEE/OSA J. Opt. Commun. Netw.*, 2(12):1010–1021, 2010.
- [36] W. Stein et al. Sage Mathematics Software (Version 6.8). The Sage Development Team, 2015. http://www.sagemath.org.
  - [37] P. Surynek. Linear ordering in the SAT encoding of the all-different constraint over bit-vectors. *ALP Newsletter*, March/April, 2014.
  - [38] W. J. van Hoeve. The alldifferent constraint: A survey. CoRR, cs.PL/0105015, 2001.
- [39] H. P. Williams and H. Yan. Representations of the all\_different predicate of constraint satisfaction in integer programming. *INFORMS Journal on Computing*, 13(2):96–103, Mar. 2001.

## A Detailed results for the Small data set

In this section, we report in Tables 10 to 14, respectively for PATHWIDTH, CUTWIDTH, BAND-WIDTH, SUMCUT and OPTIMAL LINEAR ARRANGEMENT problems the computational results of each presented formulations on the graphs of the *Small* data set. For each graph, we indicate its numbers of vertices and edges. For each graph and each formulation, we report the best found feasible solution, the optimality gap (%) and the computation time. When an instance is optimally solved, the measured width is highlighted in bold face. We use the symbol "—" to indicate that the computation time limit has been reached.

Table 10: Detailed results for PATHWIDTH on the Small data set.

	time	I	I	I	1	292.24		I	I	I	I	I	1	1	I	I	I	I	I	I	I	I	I	1	I	I		I	1
PW3	gap	2.99	58.2	33.3	74.0	0.0	50.0	2.99	75.0	75.0	75.0	86.9	75.0	63.5	7.62	2.99	2.99	50.0	74.4	74.1	2.99	76.0	73.5	85.6	84.2	2.99	2.99	2.99	8.62
	$_{\rm best}$	က	က	33	22	2	2	က	4	4	4	4	4	3	5	က	33	2	4	4	က	4	4	4	9	က	3	က	4
	time	0.71	0.33	0.27	0.47	0.24	0.25	0.44	0.35	0.46	0.56	0.34	0.48	1.07	1.78	0.45	0.31	69.0	0.65	1.08	0.75	0.73	0.57	0.21	1.32	9.0	0.75	0.64	0.46
PW2	gap	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	$_{\rm best}$	က	က	က	4	2	2	2	2	က	က	က	က	က	4	2	7	7	က	က	က	7	3	2	ည	7	2	က	2
	time	17.15	5.64	2.02	2.85	1.67	1.25	2.49	2.57	11.47	10.47	5.33	4.39	14.35	8.78	1.33	1.73	4.34	13.28	12.32	11.19	3.73	3.3	2.6	20.46	2.81	3.5	37.8	4.41
PW1	gap	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	best	က	က	က	4	2	2	2	2	က	က	က	က	က	4	2	2	2	က	က	က	7	33	2	ည	7	2	က	7
	time	7.22	3.59	3.03	2.89	1.75	1.78	2.49	2.01	4.0	7.29	5.2	3.11	2.63	3.43	2.67	1.46	4.55	12.53	8.55	7.77	4.37	4.54	2.94	11.43	1.33	3.58	9.31	5.16
[35]	gap	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	best	က	က	က	4	2	2	2	2	က	က	က	က	က	4	2	2	2	က	က	က	7	က	2	ည	7	2	က	2
	time	I	I	I	I	ı	86.05	I	I	I	I	I	I	I	I	I	I	I	I	I	I	I	I	I	I	I	I	I	Ι
[13]	gap	100.0	86.7	100.0	100.0	100.0	0.0	97.2	100.0	98.2	100.0	100.0	100.0	100.0	986	100.0	100.0	2.96	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0
	$\mathbf{best}$	က	က	4	2	3	2	က	က	4	4	ಬ	4	ಬ	9	က	4	က	33	4	က	3	4	4	2	က	4	4	3
	time	I	I	I	I	21.07	6.84	55.78	163.93	I	I	I	I	I	I	78.5	15.98	40.77	I	I	I	35.84	I	38.91	I	45.81	97.43	I	163.23
[4]	gap	2.99	2.99	2.99	75.0	0.0	0.0	0.0	0.0	2.99	2.99	2.99	2.99	2.99	75.0	0.0	0.0	0.0	2.99	2.99	2.99	0.0	2.99	0.0	80.0	0.0	0.0	2.99	0.0
	$\mathbf{best}$	3	3	3	4	2	2	2	2	3	3	3	3	3	4	2	2	2	3	3	3	7	3	2	ಒ	7	2	3	7
	m	18	19	21	24	18	18	19	19	19	19	20	20	23	29	19	19	19	20	20	20	21	21	21	32	20	20	21	21
	n	16	16	16	16	17	17	17	17	17	17	17	17	17	17	18	18	18	18	18	18	18	18	18	18	19	19	19	19
	Name	p20_16_18	p19_16_19	p18_16_21	p17_16_24	p28_17_18	p29_17_18	p22_17_19	p26_17_19	p27_17_19	p30_17_19	p21_17_20	p25_17_20	p23_17_23	p24_17_29	p35_18_19	p38_18_19	p39_18_19	p32_18_20	p36_18_20	p37_18_20	p31_18_21	p33_18_21	p34_18_21	p40_18_32	p41_19_20	$p46_{-19}20$	p47_19_21	p48_19_21

Table 10 – Continued from previous page

	$_{ m time}$	I	1	I				I	ı	I	I				I	I	1	I			1	I	I	I	I			I	ı	I
PW3	gap	0.96	91.1	100.0	80.0	0.77	80.0	2.99	78.8	75.0	98.4	96.2	91.0	96.0	93.8	98.3	7.79	83.3	84.7	94.2	75.0	80.0	75.0	100.0	75.0	85.7	6.98	94.2	100.0	100.0
	$\mathbf{best}$	4	4	4	5	4	3	က	4	4	2	4	4	4	4	9	9	က	4	3	4	5	4	5	4	7	6	2	7	9
	time	0.82	0.62	1.26	2.76	0.7	0.91	1.39	0.5	1.13	3.22	1.24	1.0	0.68	0.0	0.98	0.87	1.53	0.65	0.95	1.53	1.17	1.24	1.02	1.89	1.63	8.09	0.98	3.24	11.23
PW2	gap	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	$\mathbf{best}$	က	အ	4	4	က	က	က	7	က	4	က	3	3	3	4	3	က	2	7	3	3	3	က	က	4	9	က	4	4
	time	8.38	99.2	46.35	63.81	10.63	4.47	38.64	4.75	27.67	116.13	51.96	6.58	9.5	5.73	32.34	14.3	103.98	3.95	3.08	26.55	17.5	15.49	30.17	4.77	45.47	107.53	63.23	I	I
PW1	gap	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	25.0	0.09
	best g	က	3	4	4	က	က	က	7	အ	4	က	3	3	3	4	3	အ	2	7	3	3	3	အ	က	4	9	က	4 2	4 6
	$_{ m time} \mid  angle$	10.52	7.93	96.61	13.62	11.97	14.58	9.59	5.01	12.54	92.02	17.75	11.47	6.21	13.44	13.34	9.48	15.53	12.66	7.74	13.54	29.26	12.82	17.19	18.32	22.99	167.99	29.29	35.99	176.3
[35]	gap t	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	best g	အ	3	4	4	က	က	က	2	အ	4	က	3	3	3	4	3	က	2	7	3	3	3	အ	က	4	9	က	4	4
	time   b	I	I	I	I	I	I	I	I	I	ı	I	I	ı	I	I	I	1	1	I	ı	I	I	I	I	-	1	I	I	I
[13]	gap ti	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	98.4	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0
	best	5 1	5 1	5 1	5 1	5 1	6 1	4 1	4 1	4 1	5 1	4 1	5 1	5 1	5 1	7	6 1	4	4 1	4	4 1	5 1	6 1	7	6 1	6 1	10 1	5 1	7	7
	time	I		-		1		I	123.96	I		I	I		I	I	_	I	159.87	198.95	1	I	I	I	I			I	I	I
4	gap	2.99	2.99	75.0	75.0	2.99	2.99	2.99	0.0	2.99	75.0	2.99	2.99	2.99	2.99	80.0	75.0	2.99	0.0	0.0	2.99	2.99	2.99	2.99	2.99	75.0	85.7	2.99	75.0	75.0
	best	က	3	4	4	ಣ	က	က	2	က	4	က	3	3	3	5	4	က	2	2	3	3	3	က	က	4	7	ಣ	4	4
	m	9 22	9 22	9 24	9 25	9 25	9 25	0 21	0 22	0 22	0 23	0 23	0 24	0 24	0 27	0 28	0 28	1 22	1 22	1 22	1 23	1 24	1 25	1 27	1 28	1 30	1 42	2 25	2 29	2 29
	u	2 19	2   19	1   19	5 19	5 19	5 19	1 20	2 20	2 20	3 20	3 20	1 20	1 20	7 20	3 20	3 20	2 21	$2 \mid 21$	2 21	3 21	1 21	5 21	7 21	3 21	) 21	2 21	5 22	) 22	) 22
	Name	p43_19_22	p49_19_22	p42_19_24	p44_19_25	$p45_{-}19_{-}25$	$p50_{-}19_{-}25$	$p58_20_21$	p53_20_22	$p60_{-}20_{-}22$	$p56_{-}20_{-}23$	p59-20-23	$p55_{-}20_{-}24$	p57_20_24	$p52_{-}20_{-}27$	p51_20_28	$p54_{-}20_{-}28$	$p61_21_2$	$p64_21_22$	p67_21_22	$p69_21_23$	$p65_21_24$	$p70_{-}21_{-}25$	p68_21_27	p66-21-28	p62_21_30	$p63_21_42$	$p75_{-}22_{-}25$	p71_22_29	p73_22_29

Table 10 – Continued from previous page

73	time				-	- (	-	- 2	- (			- 1	- 2		- (		- 6			- (	- (		_					
PW3	t gap	9.68	83.3	98.0	95.3	100.0	99.5	98.2	100.0	87.7	100.0	97.1	96.2	100.0	100.0	95.4	88.9	100.0	100.0	100.0	100.0	99.5		100.0	100.0	100.0 100.0 100.0	100.0 100.0 100.0 100.0	100.0 100.0 100.0 100.0 100.0
	best	2	9	ಒ	9	7	$\infty$	6	ಬ	ಒ	ಒ	4	4	9	9	7	6	11	9	ಬ	5	ಬ	٠	0				
21	$_{ m time}$	1.4	1.33	1.6	1.84	2.65	3.49	4.0	1.69	1.35	0.89	1.92	3.29	1.15	1.41	2.2	2.17	14.32	1.45	2.08	1.95	1.57	1.7		1.44	1.44	1.44	1.44
PW2	gap	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0 0.0 0.0 0.0
	$\mathbf{best}$	3	က	က	4	4	ည	4	7	7	7	က	က	က	အ	4	4	7	က	7	2	က	က		က	ကက	w w 4	w w 4 4
	time	10.69	14.13	11.12	193.85	-	93.9	211.51	8.38	10.37	5.13	74.11	I	185.66	22.99	176.68	159.72	I	41.93	11.16	27.91	55.62	38.02		21.65	21.65	21.65	21.65 26.88 - 244.26
PW1	gap	0.0	0.0	0.0	0.0	25.0	0.0	0.0	0.0	0.0	0.0	0.0	33.3	0.0	0.0	0.0	0.0	22.4	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0 0.0 25.0	1 1 1 1
	$\mathbf{best}$	3	က	က	4	4	ಌ	~	7	7	7	က	က	က	33	4	4	7	က	7	7	က	က		က	ကက	w w 4	w   w   4   4
	time	13.2	19.43	38.68	46.03	134.88	49.89	191.36	6.91	7.39	86.7	104.02	35.97	30.22	51.13	47.85	55.02	201.25	24.8	24.96	21.11	31.52	49.59		37.47	37.47	37.47 20.5 263.08	37.47 20.5 263.08 45.27
[35]	gap	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0		
	best	3	က	က	4	4	ಸರ	7	2	7	7	က	က	က	3	4	4	7	က	2	7	က	3		က	က	ස ස 4	ည
	time	I	I	I	I		1	I	I	I	I	I	I	ı	I	I	I	I	I	1	I	I	I		ı	1 1	1 1 1	1 1 1 1
[13]	gap	100.0	100.0	8.86	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0		100.0	100.0	100.0	100.0 100.0 100.0 100.0
	$\mathbf{best}$	$\infty$	9	2	7	2	10	15	4	ಬ	4	ಬ	ಬ	ಬ	2	22	12	22	ಬ	2	4	9	13		9	9	0 0 2	6 6 53 23
	time	I	I	I	1	1	I	I	168.74	196.09	I	1	1	1	I	I	I	I	1	1	I	I	I			1 1		
[4]	gap	2.99	2.99	2.99	75.0	75.0	83.3	87.5	0.0	0.0	2.99	2.99	2.99	2.99	2.99	75.0	80.0	87.5	2.99	50.0	2.99	2.99	2.99		2.99	7.99	66.7 66.7 75.0	66.7 66.7 75.0 80.0
	$\mathbf{best}$	3	3	3	4	4	9	$\infty$	7	2	3	3	3	3	3	4	5	$\infty$	3	2	3	3	3		က	m m	8         8         4	w w 4 v
	m	56	30	30	30	31	37	49	24	24	24	56	56	56	27	30	35	46	56	26	27	27	27		27			
	$\frac{u}{}$	22	22	22	22	22	22	22	23	23	23	23	23	23	23	23	23	23	24	24	24	24	24		24	24	24 24 24	24 24 24 24
	Name	p79_22_29	p74_22_30	$p76_{-}22_{-}30$	p80-22-30	p78-22-31	p77_22_37	p72_22_49	p82_23_24	p83_23_24	$p86_{-}23_{-}24$	p84_23_26	p85_23_26	p88_23_26	$p89_{-}23_{-}27$	p87_23_30	p90-23-35	$p81_{-}23_{-}46$	p92_24_26	p97_24_26	p93.24.27	p95_24_27	$p96_{-}24_{-}27$		p99_24_27	p99_24_27 p98_24_29	p99-24-27 p98-24-29 p94-24-31	p99-24-27 p98-24-29 p94-24-31 p91-24-33

Table 11: Detailed results for Cutwidth on the Small data set.

	time	4.48	4.28	7.98	5.25	1.83	1.32	7.29	2.49	4.37	4.63	2.83	17.82	5.26	30.13	5.11	3.61	18.82	16.84	3.51	8.74	3.29	2.48	7.59	11.13	2.8	12.65	27.0	10.41	page
CW'2	gap	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	n next
	best	4	4	ಬ	7	က	က	4	4	4	4	4	4	ಸು	∞	3	က	က	4	4	4	3	4	4	∞	က	3	4	4	ned o
	time	3.67	2.99	10.01	9.07	2.39	1.73	3.99	4.08	6.87	15.0	3.97	3.54	3.77	14.19	2.36	1.44	2.23	3.06	15.99	2.77	2.28	3.17	10.51	17.75	3.93	4.51	101.92	26.9	Continued on next page
CW'1	gap	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
	best	4	4	က	4	က	က	4	4	4	4	4	4	ಸಾ	œ	က	က	က	4	4	4	အ	4	4	œ	က	3	4	4	
	time   1	I	I	I	I	-	1	I	I	I	I	I	I	1	I	I	I	I	I	1	1	I	I	I	I	I	ı	1	I	
CW3	gap t	84.7	57.1	8.02	84.5	79.1	75.0	80.0	75.0	7.68	77.1	6.77	81.5	2.99	77.1	0.06	77.1	75.0	87.5	80.0	81.7	8.98	84.3	91.7	92.3	91.1	92.9	87.5	89.4	
	$\mathbf{best}$	9	4	2	6	4	4	ಒ	ಬ	ಒ	4	2	9	9	10	2	4	4	7	5	9	9	ಒ	7	13	9	9	25	$\infty$	
	time	0.42	0.51	0.53	0.57	0.39	0.44	1.35	1.44	0.42	0.7	0.63	0.57	0.7	0.7	0.78	1.14	0.58	0.78	0.59	0.79	0.45	1.74	0.58	1.42	0.62	1.81	3.84	2.4	
CW2	gap ti	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
	best g	4	4	ທ	2	3	3	4	4	4	4	4	4	5	<b>∞</b>	3	3	3	4	4 (	4	3	4	4	<b>∞</b>	က	3	4	4	
	time   b	13.97	6.55	19.11	41.96	1.87	2.58	23.93	14.4	21.85	39.26	9.85	3.09	18.08	36.08	9.22	3.65	14.19	14.57	11.43	14.05	13.42	24.69	12.74	56.84	5.17	4.81	.49	35.08	
V1																												0 192.49		
CW	t gap	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
	best	3	4	ro	-	က	က	4	4	4	- 4	- 4	4	70	<b>∞</b>	. 3			4	- 4	- 4	. 3	4	4	<b>∞</b>	٠ د	- 3	4	4	
	$_{ m time}$	40.63	253.5	ļ	ļ		87.52			I		ı				ı	1	I				!			1	ļ	I		1	
[26]	gap	0.0	0.0	0.09	56.3	50.0	0.0	37.5	37.5	25.0	87.5	80.0	25.0	50.0	55.6	25.0	50.0	25.0	90.0	87.5	30.0	50.0	70.0	0.09	63.6	25.0	90.0	100.0	87.5	
	best	4	4	5	$\infty$	4	က	4	4	4	4	5	4	9	6	4	4	4	2	4	5	5	5	5	11	4	5	5	4	
	time	I	168.03	I	I	ı	ı	I	I	I	I	I	I	ı	I	I	I	I	I		1	I	I	I	I	I		ı	I	
[22]	$\operatorname{gap}$	50.0	0.0	46.7	93.6	75.0	77.1	87.4	91.3	91.9	80.0	77.3	92.9	97.1	94.8	95.0	75.0	86.7	9.76	0.06	0.06	87.9	91.0	88.5	8.66	97.1	98.6	90.4	100.0	
	$\mathbf{best}$	4	4	ಬ	$\infty$	4	4	4	ಬ	ಬ	4	2	ಬ	2	10	5	4	ಬ	2	5	5	4	ಬ	ಬ	10	ಬ	5	4	9	
	m	3 18	9 19	3 21	3 24	7 18	7 18	7 19	7 19	7 19	7 19	20	20	7 23	29	3 19	3 19	3 19	3 20	3 20	3 20	3 21	3 21	3 21	3 32	9 20	) 20	) 21	) 21	
	n	8 16	9 16	1 16	4 16	8 17	8 17	9 17	9 17	9 17	9 17	) 17	) 17	3 17	9 17	9 18	9 18	9 18	0 18	$0 \mid 18$	) 18	1 18	1 18	1 18	2 18	0 19	)   19	1 19	1 19	
	Name	p20_16_18	p19_16_19	p18_16_2]	p17_16_24	p28_17_18	p29_17_18	p22_17_19	p26_17_19	p27_17_19	p30_17_19	p21_17_20	p25_17_20	p23_17_23	p24_17_29	p35_18_19	p38_18_19	p39_18_19	p32_18_20	p36.18.20	p37_18_20	p31_18_21	p33_18_21	p34_18_21	p40_18_32	p41_19_20	$p46_{-19-20}$	p47_19_21	p48_19_21	

Table 11 -Continued from previous page

CW'2	time	29.2	0 32.09	0 7.83	0 22.27	0  36.01	0 2.93	0   4.65	0 20.32	0 18.31	69.79 0	0 7.09	0 20.44	0 9.89	0 13.44	0 17.95	0 269.02	0 124.34	0 9.42	0 9.04	- 0	0 12.07	0 162.74	0 220.88		0 144.57		- 0	0 73.61	02 96 0
CV	st gap	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	40.0	0.0	0.0	0.0	16.7	0.0	2 66.7	40.0	0.0	0.0
	best	4	4	ည	9	ಬ	4	က	4	4	τυ	4	4	4	ည	9	9	4	3	က	55	4	ည	9	9	7	12	5	ည	7.3
	$_{ m time}$	71.17	22.31	11.79	29.74	23.15	4.93	3.9	16.7	32.3		27.21	5.91	7.86	5.53	41.06	169.14	132.47	6.93	5.3		7.28	6.96	192.87	I	112.5			27.73	
CW'1	gap	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	20.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	20.0	0.0	0.0	0.0	16.7	0.0	41.7	40.0	0.0	20.0
	$\mathbf{best}$	4	4	ಬ	9	ည	4	က	4	4	ಬ	4	4	4	ಬ	9	9	4	က	က	ಬ	4	ည	9	9	7	12	ಬ	ည	rc.
	time	Ι	-	I	I	I		Ι	Ι	1	I	1	1	1	Ι	Ι	I	1	1	1	I	I	I	I	1	I	I	I	Ι	I
CW3	gap t	9.76	95.0	90.4	87.3	9.76	94.0	97.9	98.0	7.68	95.7	92.4	84.9	91.1	88.9	90.0	100.0	100.0	6.96	100.0	100.0	6.68	100.0	100.0	87.5	7.76	100.0	100.0	100.0	99.5
	best	9	9	7	$\infty$	$\infty$	9	9	9	5	7	9	9	7	6	10	10	$\infty$	7	2	$\infty$	2	6	10	$\infty$	10	18	6	$\infty$	19
þ	time b	1.32	0.83	1.81	0.72	1.08	1.6	0.45	1.17	1.81	2.66	26.0	0.91	1.13	0.79	1.64	2.72	2.81	0.92	0.85	4.78	1.34	2.67	5.08	6.27	5.44	4.96	3.85	99.9	3 05
CW2	gap ti	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5	best ga	4 0.	4 0.	5	0 9	5	4 0.	3 0.	4	4 0.	5	4 0.	4	4 0.	5	0 9	0 9	4 0.	3 0.	3 0.	<b>5</b>	4 0.	5	0 9	0 9	7	<b>12</b> 0.	5	5	5
-						55					ı						I	I			1	.46	1	I	T	1		ı	1	1
7.1	$_{ m time}$	72.16	8.77	104.46	40.21	17.65	47.07	32.15	186.63	43.7		234.98	46.38	42.07	16.72	202.53			109.24	15.94		83								
CW <sub>1</sub>	t gap	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	20.0	0.0	0.0	0.0	0.0	0.0	16.7	25.0	0.0	0.0	20.0	0.0	20.0	16.7	16.7	14.3	30.3	20.0	40.0	0.06
	best	4	4	ro	9	ಬ	4	က	4	4	5	4	4	4	v	9	9	4	က	က	5	4	5	9	9	7	12	5	5	ъ
	time			l				I	I		ı	I			I	I	l					I	I	l				ı	I	
[26]	•	75.0	40.0	100.0	100.0	50.0	78.6	100.0	50.0	100.0	100.0	100.0	100.0	64.3	100.0	100.0	100.0	100.0	100.0	2.99	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100 0
	$\mathbf{best}$	9	ಬ	2	2	2	2	ಬ	ಬ	ಬ	9	5	9	2	2	6	$\infty$	ಬ	9	9	9	2	7	$\infty$	10	10	15	$\infty$	2	X
	time	I	1	Ι				I	I	ı	I	1	1	1	I	I	I	ı	1	1	I	I	I	I	ı	1	1	I	I	I
[22]	gap	98.0	100.0	100.0	100.0	100.0	93.4	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100 0
	best	5	2	2	2	$\infty$	9	9	2	2	9	9	9	$\infty$	$\infty$	2	2	2	$\infty$	ಬ	7	$\infty$	$\infty$	$\infty$	6	6	17	7	6	0
$\vdash$	$\frac{1}{m}$	22	22	24	25	25	25	21	22	22	23	23	24	24	27	28	28	22	22	22	23	24	25	27	28	30	42	25	29	56
	u	19	19	19	19	19	19	20	20	20	20	20	20	20	20	20	20	21	21	21	21	21	21	21	21	21	21	22	22	66
	Name	p43_19_22	p49_19_22	p42_19_24	p44_19_25	p45_19_25	p50_19_25	p58_20_21	p53_20_22	p60_20_22	$p56_20_23$	p59_20_23	p55_20_24	p57_20_24	p52_20_27	p51_20_28	p54_20_28	$p61_21_22$	p64_21_22	p67_21_22	p69_21_23	$p65_21_24$	$p70_21_25$	p68_21_27	p66_21_28	p62_21_30	p63_21_42	p75_22_25	p71_22_29	p73 22 29

Table 11 – Continued from previous page

			[26]			[96]		+	CW1		1	6/M	0 -		CW13			CW71	_		G(/M)	
	a a	hest	Ö	time	hest		time	heet	997	time	heet	0 v o	time	hest		time	hest	2 6	ı time	hest		time
179 22 29 3			100 0	- CITITE	x x	100 0		200	8ap		Z Z	8aP	4 88	11	100 O		re re	gap	67 10	_		39.4
		10	100.0	I	6	100.0	I	9	16.7	I	ြင	0.0	4.3	1	100.0	-	9	16.7			33.3	1.10
		6	100.0	I	6	100.0	1	9	16.7	I	9	0.0	7.53	12	100.0	1	9	33.3		9	33.3	1
	22 30	$\infty$	100.0		11	100.0	I	ည	0.0	254.29	ಸರ	0.0	4.63	10	97.5		73	0.0	84.27	က	0.0	26.44
p78_22_31 2	22 31	11	100.0		2	100.0	ı	9	0.0	254.95	9	0.0	96.9	11	100.0	-	9	0.0	128.77	9	16.7	
p77_22_37 2	22 37	14	100.0		12	100.0	I	$\infty$	25.0		œ	0.0	2.46	15	100.0		œ	0.0	115.57	œ	0.0	66.5
p72_22_49 2	22 49	21	100.0	I	18	100.0	Ι	14	51.6	I	14	0.0	42.03	21	100.0	I	14	42.9	I	14	42.9	I
p82_23_24 2	23 24	$\infty$	100.0	I	2	100.0	I	4	0.0	29.96	4	0.0	1.06	10	2.96	1	4	0.0	132.47	4	0.0	121.47
p83_23_24 2	23 24	7	100.0	I	9	100.0	I	4	0.0	69.29	4	0.0	2.3	7	100.0	1	4	0.0	288.48	4	0.0	271.95
p86_23_24 2	23 24	9	100.0	I	9	100.0	I	က	0.0	20.52	က	0.0	2.82	7	100.0	I	က	0.0	10.41	က	0.0	22.1
	23 26	$\infty$	100.0	I	$\infty$	100.0	I	4	25.0	1	4	0.0	3.29	10	96.4	I	4	0.0	173.43	4	50.0	
p85_23_26 2	23 26	6	100.0	I	7	100.0	I	4	0.0	262.3	4	0.0	1.81	6	100.0		4	0.0	181.97	4	0.0	38.11
p88_23_26 2	23 26	7	100.0		7	100.0	I	4	0.0	181.32	4	0.0	2.63	$\infty$	95.9	1	4	0.0	33.18	4	0.0	53.81
p89_23_27 2	23 27	6	100.0	I	$\infty$	100.0	I	5	20.0	I	က	0.0	5.38	$\infty$	87.5	1	ಬ	0.0	205.47	ည	0.0	6.89
p87_23_30   2	23 30	12	100.0	I	6	100.0	Ι	9	33.3	Ι	9	0.0	2.63	11	6.06	_	9	33.3	I	9	0.0	253.43
$p90_{-}23_{-}35$   2	$23 \ 35$	11	100.0	_	11	100.0	-	2	42.9	_	2	0.0	4.29	14	100.0	_	2	28.6	_	2	14.3	-
	23 46	21	100.0	I	16	100.0	_	14	83.3	_	13	0.0	12.64	18	2.66	_	13	53.8	_	13	53.8	I
$p92_24_26   2$	24 26	8	100.0	I	2	100.0		4	50.0	_	4	0.0	2.96	10	100.0	-	4	0.0	70.45	4	0.0	70.65
	24 26	9	100.0	_	8	100.0	Ι	5	23.8	_	4	0.0	4.82	6	100.0	_	4	25.0	I	4	0.0	191.34
$p93_{-}24_{-}27$   2	24 27	2	100.0	I	$\infty$	100.0	I	4	0.0	71.95	4	0.0	4.85	6	100.0	1	4	0.0	118.0	4	25.0	ı
$p95_{-}24_{-}27 \mid 2$	24 27	$\infty$	100.0	I	2	100.0	I	4	0.0	110.36	4	0.0	3.2	$\infty$	100.0	1	4	25.0	I	4	0.0	139.3
$p96_24_27   2$	24 27	2	100.0	I	6	100.0	I	4	25.0	I	4	0.0	2.32	13	100.0	1	4	0.0	273.03	4	0.0	170.3
p99_24_27   2	24 27	6	100.0	I	$\infty$	100.0	I	5	40.0	I	ည	0.0	16.52	6	100.0	I	3	40.0	I	2	0.09	ı
$p98_24_29 \mid 2$	24 29	10	100.0	I	6	100.0	_	2	0.0	241.65	2	0.0	5.83	11	100.0	_	2	0.0	161.69	2	40.0	I
p94_24_31 2	$24 \ 31$	10	100.0	1	10	100.0	ı	9	0.0	207.14	9	0.0	5.0	13	100.0	I	9	50.0	I	9	2.99	ı
p91_24_33   2	24 33	13	100.0	I	$\infty$	100.0	1	9	35.0	-	9	0.0	6.84	10	100.0	-	9	16.7		9	0.0	182.05
p100_24_34 24	4 34	11	100.0	I	6	100.0	Ι	7	28.6	I	7	0.0	4.26	16	100.0	I	7	42.9	I	7	71.4	I
-																						

Table 12: Detailed results for BANDWIDTH on the Small data set.

		[26]			[4]			[31]		<u></u>	[31]+F2	2	3.5	[31]+F3	8		BW1			BW2			BW3	
best gap	82	d	time	$_{\mathrm{best}}$	gap	time	$\mathbf{best}$	gap	time	$\mathbf{best}$	gap	time	best	gap	time	$\mathbf{best}$	gap	time	$\mathbf{best}$	gap	$_{ m time}$	$\mathbf{best}$	gap	time
4		0.0	6.22	4	0.0	7.64	4	0.0	0.46	4	0.0	0.57	4	0.0	8.45	4	0.0	1.05	4	0.0	0.59	4	0.0	3.97
4		0.0	7.19	4	0.0	10.26	4	0.0	0.48	4	0.0	0.63	4	0.0	13.6	4	0.0	1.34	4	0.0	0.55	4	0.0	3.37
4		0.0	5.8	4	0.0	7.21	4	0.0	0.19	4	0.0	0.54	4	0.0	7.72	4	0.0	0.85	4	0.0	0.58	4	0.0	4.56
2		0.0	13.92	5	0.0	25.14	2	0.0	0.56	5	0.0	0.74	2	0.0	15.29	5	0.0	2.19	5	0.0	0.69	2	0.0	18.42
3		0.0	5.91	3	0.0	3.68	3	0.0	0.4	3	0.0	89.0	3	0.0	4.71	3	0.0	1.71	3	0.0	0.54	3	0.0	4.46
က		0.0	8.89	က	0.0	68.9	က	0.0	0.29	က	0.0	0.52	က	0.0	7.59	က	0.0	0.99	က	0.0	0.47	က	0.0	4.2
4		0.0	15.95	4	0.0	18.04	4	0.0	0.26	4	0.0	0.74	4	0.0	42.11	4	0.0	2.62	4	0.0	0.75	4	0.0	11.89
4	1	0.0	13.92	4	0.0	15.78	4	0.0	0.33	4	0.0	0.64	4	0.0	29.21	4	0.0	1.9	4	0.0	0.63	4	0.0	13.83
4	ı	0.0	60.21	4	0.0	9.22	4	0.0	0.5	4	0.0	9.0	4	0.0	26.48	4	0.0	2.06	4	0.0	0.61	4	0.0	16.85
က	1	0.0	8.01	က	0.0	10.94	က	0.0	0.39	က	0.0	0.51	က	0.0	6.17	က	0.0	1.45	အ	0.0	0.62	က	0.0	5.57
4	1	0.0	93.5	4	0.0	16.26	4	0.0	0.49	4	0.0	0.64	4	0.0	18.18	4	0.0	2.02	4	0.0	0.62	4	0.0	13.54
4		0.0	99.6	4	0.0	10.59	4	0.0	89.0	4	0.0	99.0	4	0.0	11.79	4	0.0	1.4	4	0.0	0.65	4	0.0	14.82
4	1	0.0	19.81	4	0.0	13.9	4	0.0	0.34	4	0.0	0.63	4	0.0	17.87	4	0.0	2.19	4	0.0	0.58	4	0.0	7.59
9		83.3	I	9	0.0	38.88	9	0.0	1.46	9	0.0	1.22	9	0.0	177.55	9	0.0	7.0	9	0.0	1.65	9	0.0	91.69
4		0.0	18.16	4	0.0	16.01	4	0.0	0.48	4	0.0	0.72	4	0.0	82.72	4	0.0	1.69	4	0.0	0.9	4	0.0	23.24
က		0.0	7.8	3	0.0	12.57	3	0.0	0.36	3	0.0	0.58	3	0.0	18.36	3	0.0	2.11	3	0.0	0.49	3	0.0	5.24
3		0.0	89.9	3	0.0	8.46	3	0.0	0.44	3	0.0	0.56	3	0.0	17.65	3	0.0	0.89	3	0.0	0.51	8	0.0	8.56
4		0.0	11.45	4	0.0	13.91	4	0.0	0.54	4	0.0	0.65	4	0.0	21.11	4	0.0	1.82	4	0.0	0.82	4	0.0	12.67
4		0.0	106.82	4	0.0	21.54	4	0.0	0.41	4	0.0	29.0	4	0.0	49.9	4	0.0	2.78	4	0.0	0.82	4	0.0	41.13
က		0.0	253.29	ಸು	0.0	34.19	ಬ	0.0	1.11	ಸಾ	0.0	1.44	ಬ	0.0	224.21	ಸು	0.0	5.86	ಬ	0.0	1.03	ಸಾ	0.0	107.21
4		0.0	21.19	4	0.0	33.56	4	0.0	0.47	4	0.0	0.7	4	0.0	25.69	4	0.0	3.81	4	0.0	0.69	4	0.0	12.78
4		0.0	114.09	4	0.0	27.17	4	0.0	0.34	4	0.0	0.7	4	0.0	17.55	4	0.0	1.31	4	0.0	0.72	4	0.0	27.54
4		0.0	13.41	4	0.0	13.6	4	0.0	0.83	4	0.0	0.75	4	0.0	20.41	4	0.0	3.22	4	0.0	0.84	4	0.0	15.34
ည		0.0	24.65	ಬ	0.0	31.1	ಬ	0.0	0.0	ಬ	0.0	1.23	ಬ	0.0	33.98	ಬ	0.0	4.54	ಬ	0.0	0.7	ಒ	0.0	14.92
က		0.0	23.25	အ	0.0	10.5	က	0.0	0.49	3	0.0	0.61	က	0.0	10.6	အ	0.0	3.99	3	0.0	0.72	အ	0.0	10.64
က		0.0	107.31	က	0.0	19.96	က	0.0	0.51	က	0.0	0.64	က	0.0	9.55	က	0.0	4.63	က	0.0	0.72	က	0.0	6.57
3		0.0	15.39	3	0.0	21.31	3	0.0	0.3	3	0.0	1.14	3	0.0	4.19	3	0.0	2.48	3	0.0	0.59	3	0.0	22.69
4		0.0	127.29	4	0.0	22.16	4	0.0	0.48	4	0.0	0.85	4	0.0	45.61	4	0.0	3.25	4	0.0	0.78	4	0.0	25.65
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Table 12 – Continued from previous page

			[96]			Ξ			[31]		[31	31] TE9		[3	31] TE3			RW1			RW9			RW3	
-		-				Ξ					3	1	-	_	)		-	4		-	1				
Name		best	90	time	pest	gap	tıme	pest		$\rightarrow$	pest g			pest g		-	pest		time	pest		-	pest	gap	time
p43_19_22	19 22	4	0.0	144.77	4	0.0	40.67	4	0.0	0.53	4	0.0	1.09	4	0.0	60.72	4	0.0	2.22	4	0.0	0.93	4	0.0	27.28
$p49_{-}19_{-}22$	19 22	4	0.0	181.73	4	0.0	20.25	4	0.0	0.48	4	0.0	1.01	4	0.0	21.82	4	0.0	2.63	4	0.0	0.74	4	0.0	19.04
p42_19_24	19 24	4	0.0	189.53	4	0.0	99.48	4	0.0	1.15	4	0.0	0.73	4	0.0	34.52	4	0.0	3.26	4	0.0	69.0	4	0.0	11.82
p44_19_25	19 25	20	100.0	I	2	0.0	136.25	25	0.0	1.14	2	0.0	1.57	25	0.0	169.95	ಬ	0.0	5.47	2	0.0	1.23	2	0.0	43.0
p45_19_25	19 25	20	80.0	I	2	0.0	28.12	ಬ	0.0	1.42	2	0.0	96.0	25	0.0	142.68	ಬ	0.0	11.39	2	0.0	1.03	2	0.0	93.18
p50_19_25	19 25	4	0.0	27.78	4	0.0	32.49	4	0.0	1.29	4	0.0	0.72	4	0.0	29.48	4	0.0	3.55	4	0.0	76.0	4	0.0	18.82
p58-20-21	20 21	4	25.0		4	0.0	50.42	4	0.0	0.47	4	0.0	8.0	4	0.0	145.78	4	0.0	10.74	4	0.0	0.83	4	0.0	29.26
p53_20_22	20 22	4	0.0	230.73	4	0.0	24.68	4	0.0	69.0	4	0.0	0.72	4	0.0	64.7	4	0.0	1.69	4	0.0	0.92	4	0.0	40.48
p60_20_22	20 22	4	75.0	I	4	0.0	27.68	4	0.0	0.56	4	0.0	0.74	4	0.0	157.64	4	0.0	5.73	4	0.0	1.32	4	0.0	92.99
p56_20_23	20 23	4	25.0	I	4	0.0	37.96	4	0.0	0.64	4	0.0	0.91	4	0.0	44.0	4	0.0	12.06	4	0.0	89.0	4	0.0	25.5
p59-20-23	20 23	4	0.0	247.78	4	0.0	33.65	4	0.0	1.26	4	0.0	0.77	4	0.0	60.64	4	0.0	4.25	4	0.0	0.88	4	0.0	18.73
p55_20_24	20 24	4	0.0	129.89	4	0.0	49.6	4	0.0	0.49	4	0.0	0.61	4	0.0	68.06	4	0.0	6.63	4	0.0	1.77	4	0.0	80.93
p57_20_24	20 24	4	0.0	17.55	4	0.0	41.13	4	0.0	0.53	4	0.0	1.22	4	0.0	48.81	4	0.0	12.31	4	0.0	1.02	4	0.0	41.14
p52_20_27	20 27	20	95.0	I	33	0.0	23.41	ಬ	0.0	1.41	ಸಾ	0.0	2.99	ಬ	0.0	100.57	2	0.0	6.24	ಸಾ	0.0	3.07	ಸ	0.0	141.42
p51_20_28	20 28	9	100.0	ı	2	0.0	56.38	ಬ	0.0	1.59	ಬ	0.0	1.61	ಬ	0.0 - 18	184.68	2	0.0	10.93	ಬ	0.0	1.71	2	0.0	164.43
$p54_{-}20_{-}28$	20 28	2	94.9	ı	2	0.0	74.16	2	0.0	1.55	2	0.0	1.1	22	0.0 - 28	286.71	2	0.0	10.51	2	0.0	1.13	2	0.0	60.92
p61_21_22	21 22	4	0.0	27.09	4	0.0	42.79	4	0.0	0.56	4	0.0	0.79	4	0.0	76.49	4	0.0	7.51	4	0.0	1.07	4	0.0	163.73
$p64_21_22$	21 22	4	93.2		4	0.0	43.32	4	0.0	0.54	4	0.0	0.83	4	0.0	110.19	4	0.0	11.12	4	0.0	1.48	4	0.0	56.92
$p67_21_22$	21 22	4	75.0		4	0.0	54.36	4	0.0	0.67	4	0.0	0.87	4	0.0 - 1'	179.65	4	0.0	7.17	4	0.0	1.12	4	0.0	45.45
$p69_21_23$	21 23	4	94.2	_	4	0.0	43.86	4	0.0	0.57	4	0.0	1.24	5 2	20.0	ı	4	0.0	21.94	4	0.0	1.67	4	0.0	59.09
$p65_{-}21_{-}24$	21 24	4	100.0	_	4	0.0	61.42	4	0.0	1.03	4	0.0	0.7	4	0.0	52.32	4	0.0	5.89	4	0.0	1.43	4	0.0	2.69
$p70\_21\_25$	21 25	1 4	0.0	288.27	4	0.0	44.08	4	0.0	1.07	4	0.0	2.54	4	0.0	54.71	4	0.0	8.66	4	0.0	1.42	4	0.0	22.27
p68-21-27	21 27	5	100.0	ı	2	0.0	30.57	2	0.0	1.95	2	0.0	1.44	5 2	20.0	I	2	0.0	3.89	2	0.0	1.29	2	0.0	110.94
p66_21_28	21 28	73	100.0	ı	ಬ	0.0	173.52	ಸು	0.0	26.0	ಸರ	0.0	2.16	5 2	20.0	I	ಬ	0.0	12.48	ಸಾ	0.0	2.05	ಸಾ	0.0	104.49
$p62_21_30$	21 30	9	100.0	ı	2	0.0	155.41	5	0.0	5.03	5	0.0	3.75	5	0.0	118.34	2	0.0	12.38	2	0.0	3.21	2	0.0	94.03
$p63_21_42$	21 42	11	100.0		2	14.3		7	0.0	1.13	7	0.0	2.76	7 3	38.1	I	7	0.0	53.2	7	0.0	8.08	7	14.3	1
$p75_{-}22_{-}25$	22 25	4	93.4	_	4	0.0	50.19	4	0.0	1.66	4	0.0	1.84	4	0.0	283.5	4	0.0	6.31	4	0.0	0.93	4	0.0	52.85
p71_22_29	22 29	2	100.0	_	2	0.0	263.73	2	0.0	3.13	2	0.0	2.02	2	0.0	212.13	2	0.0	30.07	2	0.0	2.86	5	20.0	1
$p73_22_229$	22 29	2	100.0	_	2	0.0	166.72	2	0.0	1.0	2	0.0	1.09	5 3	30.0	ı	2	0.0	17.51	2	0.0	1.52	2	0.0	217.1
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Table 12 – Continued from previous page

			[96]			[4]			[31]		[2]	31]+F2		E	31]+F3			RW1			RW9			RW3	
Name	u	best	0.0	time	best	90	time	best	_	time	$_{ m pest}$	gap t	ime	best 8	gap t	ime	best		time 1	best g	gap ti	time b	best		time
p79_22_29	22 29	7	100.0		4	0.0	60.69	4	0.0	1.31	4		1.52	5 3	38.0	ı	4		7.61			96.0	4		219.69
p74_22_30	22 30	20	100.0		ಬ	0.0	41.19	ಬ	0.0	2.24	ಬ	0.0	1.63	5 2	20.0	I	ಒ	0.0	37.04	ಒ	0.0	1.31	ಬ	0.0	211.92
p76_22_30	22 30	2	100.0		ಸು	0.0	84.07	ಸಾ	0.0	0.91	2	0.0	2.15	5 3	30.0	I	ಬ	0.0	20.37	ಒ	0.0	1.54	ಬ	0.0	141.76
p80_22_30	22 30	20	100.0	I	4	0.0	83.55	4	0.0	1.74	4	0.0	1.31	5 4	40.0	I	4	0.0 1	11.98	4	0.0	1.97	4	0.0	135.47
p78_22_31	22 31	7	100.0		ಸಾ	0.0	83.51	ಸಾ	0.0	1.17	ಒ	0.0	1.99	ಬ	0.0	155.81	ಬ	0.0	9.23	ಒ	0.0	1.27	ಬ	0.0	97.84
p77_22_37	22 37	∞	100.0		9	16.7		9	0.0	1.68	9	0.0	2.77	3 9	33.6	I	9	0.0	86.78	9	0.0	2.55	9	28.4	1
p72_22_49	22 49	10	98.1		$\infty$	25.0		œ	0.0	4.09	∞	0.0	6.73	∞ ∞	34.8	I	œ	0.0	45.17	∞	8 0.0	8.86	∞	43.3	
p82_23_24	23 24	20	96.5		က	0.0	51.28	ಬ	0.0	0.84	2	0.0	1.62	5 3	30.0	1	ಬ	0.0	9.14	ಬ	0.0	2.53	5	23.3	1
p83_23_24	23 24	4	100.0	I	4	0.0	46.1	4	0.0	86.0	4	0.0	1.36	4	0.0 14	143.98	4	0.0	4.61	4	0.0	0.99	4	0.0	46.17
p86_23_24	23 24	4	100.0	I	4	0.0	73.04	4	0.0	1.71	4	0.0	1.87	4	25.0	I	4	0.0	9.16	4	0.0	1.34	4	0.0 1	111.28
p84_23_26	23 26	4	94.7		4	0.0	102.2	4	0.0	98.0	4	0.0	0.94	4	0.0 18	187.92	4	0.0	7.44	4	0.0	1.3	4	25.0	1
p85_23_26	23 26	20	100.0		4	0.0	39.88	4	0.0	1.69	4	0.0	1.45	4	0.0 28	288.62	4	0.0	10.04	4	0.0	1.22	4	0.0	226.94
p88_23_26	23 26	20	100.0		4	0.0	80.39	4	0.0	1.03	4	0.0	1.09	4	0.0	294.9	4	0.0	9.38	4	0.0	1.26	4	25.0	1
p89_23_27	23 27	7	100.0		ಬ	20.0		ಸರ	0.0	1.83	ಒ	0.0	2.42	5 2	21.3	1	ಸು	0.0	21.5	ಸಾ	0.0	1.79	5	20.0	
p87_23_30	23 30	8	100.0		2	28.6	1	9	0.0	3.35	9	0.0	5.1	3 9	35.5	ı	9	0.0 4	44.81	9	0.0	7.74	9	31.5	1
p90_23_35	23 35	10	100.0		5	20.0	-	2	0.0	2.18	2	0.0	2.37	3 9	34.9	-	2	0.0	23.61	2	0.0	3.51	2	0.0	137.02
p81_23_46	23 46	10	6.79		8	25.0	-	8	0.0	11.12	8	0.0	22.2	8	51.4	-	8	0.0 5	56.23	8	0.0 45	43.05	8	38.8	1
p92_24_26	24 26	2	96.1		4	0.0	126.68	4	0.0	1.28	4	0.0	2.17	4 5	37.3	1	4	0.0	13.07	4	0.0	1.54	4	0.0	127.98
p97_24_26	24 26	9	100.0	I	4	0.0	279.03	4	0.0	4.16	4	0.0	2.12	5 5	54.5	I	4	0.0	64.81	4	0.0	3.93	5	32.0	ı
p93_24_27	24 27	9	100.0		4	0.0	67.86	4	0.0	1.66	4	0.0	1.09	4	0.0 29	291.29	4	0.0	7.27	4	0.0	1.91	4	0.0	100.79
p95_24_27	24 27	5	95.8		2	0.0	212.53	2	0.0	1.4	2	0.0	3.05	5 4	40.0	ı	2	0.0	53.54	2	0.0	1.69	5 ;	26.0	1
p96_24_27	24 27	. 4	100.0		4	0.0	220.26	4	0.0	0.93	4	0.0	2.58	4 2	25.0	1	4	0.0	10.71	4	0.0	3.14	4	0.0	227.05
p99_24_27	24 27	9	100.0	I	4	0.0	114.95	4	0.0	2.15	4	0.0	5.48	5 4	41.2	I	4	0.0	17.72	4	0.0	1.53	4	0.0	77.58
p98_24_29	24 29	5	100.0	I	5	0.0	114.38	5	0.0	1.5	2	0.0	3.02	5 4	40.0	I	2	0.0 1	14.17	2	0.0	2.42	5	28.0	I
p94_24_31	24 31	2	96.7		2	0.0	283.6	2	0.0	1.31	2	0.0	2.42	3 9	8.73	1	2	0.0	53.0	2	0.0	5.02	5 ;	20.0	1
p91_24_33	24 33	2	100.0	ı	∞	37.5	1	9	0.0	2.99	9	0.0	8.29	9	55.8	I	9	0.0	60.19	9	0.0	9.58	9	36.7	ı
p100_24_34	24 34	10	100.0	1	9	16.7	1	9	0.0	4.43	9	0.0	60.6	9	50.0	-	9	0.0	51.39	9	0.0	6.13	9	33.3	1

Table 13: Detailed results for SumCut on the Small data set.

c         n         n         pest         gap         time         best         gap         time         pest         gap         gap         time         gap	1				SC1			SC2			SC3			PR1			PR2	\$2			PR3	
16         18         24         0.0         18.3         96         96         24         0.0         18.46         97         98.9         24         0.0         18.46         97         0.0         18.40         18.46         36         98.9         2         70         0.0         31.6         18.7         0.0         6.89         30         98.9         2         70         0.0         31.2         0.0         18.47         41         0.0         18.98         2         2         0.0         29.52         27         0.0         29.93         2         2         2         0.0         9.0	16   18   24   0.0   0.04.92   24   0.0   8.38   25   969   9-2   24   0.0   0.630   24   0.0   31.65   24   0.0   0.04.92   12   0.0   0.04.83   12   0.0   0.04.83   12   0.0   0.04.83   12   0.0   0.04.83   12   0.0   0.04.83   12   0.0   0.04.83   13   0.0   0.04.83   14   0.0   0.04.83   0.0   0.0   0.04.83   0.0   0.0   0.04.83   0.0   0.0   0.04.83   0.0   0.0   0.04.83   0.0   0.0   0.04.83   0.0   0.0   0.04.83   0.0   0.0   0.04.83   0.0   0.0   0.04.83   0.0   0.0   0.04.83   0.0   0.0   0.04.83   0.0   0.0   0.04.83   0.0   0.0   0.04.83   0.0   0.04.83   0.0   0.0   0.04.83   0.0   0.0   0.04.83   0.0   0.0   0.04.83   0.0   0.0   0.04.83   0.04.83								time	$\mathbf{best}$	gap	time			$_{ m time}$	bes					gap	time
16 19         27 0.0 60.81         27 0.0 66.81         27 0.0 6.69         30 98.9 - 32         27 0.0 299.52         27 0.0 267.7         20 0.0 267.9         27 0.0 18.46         34 99.8 - 32 28.8 - 32         32 0.0 299.53         32 0.0 18.46         34 99.8 - 32 28.8 - 32         32 0.0 18.40         32 0.0 18.46         34 99.8 - 32 28.8 - 32         32 0.0 18.40         33 0.0 18.40         33 0.0 18.40         34 0.0 18.40         34 0.0 18.40         34 0.0 18.40         34 0.0 18.40         34 0.0 18.40         34 0.0 18.40         34 0.0 18.40         34 0.0 18.40         34 0.0 18.40         34 0.0 18.40         34 0.0 18.40         34 0.0 18.40         34 0.0 18.40         34 0.0 18.40         34 0.0 18.40         34 0.0 18.40         34 0.0 18.40	16 19   27 0.0 0.088   27 0.0 0   6.69   30 98.9   -2 27 0.0 239.52   27 0.0 26.7   27 0.0 18.46   34 99.8   -3 28.8   -3 2 0.0 12.29   32 27.0     16 21   32 0.0 269.33   32 0.0 18.46   34 99.8   -3 2 8.8   -3 2 0.0 12.29   32 27.0     17 18   23 0.0 297.19   23 0.0 18.89   28 10.00   -2 23 24.7   -2 23 0.0 40.24   24 0.0 17.18     17 18   20 0.0 17.70   20 0.0 0.0 18.83   30 96.9   -2 20 0.0 193.84   20 0.0 31.94   20 0.0 17.19     17 19   26 0.0 46.76   26 0.0 12.83   30 96.9   -2 7 12.7   -2 29 0.0 21.11   26 0.0 17.11     17 19   24 0.0 34.73   23 0.0 12.84   39 96.9   -2 7 12.7   -2 29 0.0 21.11   26 0.0 17.11     17 19   24 0.0 34.73   24 0.0 12.84   32 96.9   -2 7 12.7   -2 29 0.0 21.11   26 0.0 17.11     17 10   24 0.0 34.73   24 0.0 12.84   32 96.9   -2 7 12.7   -2 29 0.0 21.11   26 0.0 17.11     17 10   24 0.0 34.73   24 0.0 12.84   32 99.7   -2 24 0.0 237.6   24 0.0 33.16   27 23.2     17 10   24 0.0 34.73   24 0.0 12.84   32 99.7   -2 24 0.0 237.6   24 0.0 33.16   27 23.2     17 10   27 0.0 117.85   27 0.0 12.84   32 100.0   -2 27 44   -2 32 0.0 34.48   32 30.3     17 20   37 0.0 117.85   27 0.0 12.84   31 10.00   -2 17 20.6   27 0.0 33.16   27 23.2     18 19   25 0.0 20.24.4   32 0.0 18.8   32 90.7   -2 17 20.6   24.4   -2 32 0.0 34.48   27 23.2     18 19   25 0.0 20.27.4   25 0.0 20.27.1   27 20.0   27 20.0   27 20.0   27 20.0     18 19   25 0.0 20.27.4   25 0.0 33.24   26 98.2   -2 25 34.7   -2 25 0.0 0.0 199.5   27 23.3     18 20   33 48.5   -3 2 0.0 31.25   33 100.0   -3 3 43.2   -3 25 0.0 199.8   27 0.0 199.5     18 21   27 0.0 16.22   27 0.0 3.9   27 0.0 0.0 193.5   27 0.0 199.5   27 0.0 199.5     18 21   27 0.0 16.22   27 0.0 0.0 199.5   27 0.0 199.5   27 0.0 199.5   27 0.0 199.5     18 21   27 0.0 18.2   27 0.0 19.2   27 0.0 0.0 199.5   27 0.0 199.5   27 0.0 199.5   27 0.0 199.5   27 0.0 199.5   27 0.0 199.5   27 0.0 199.5   27 0.0 199.5   27 0.0 199.5   27 0.0 199.5   27 0.0 199.5   27 0.0 199.5   27 0.0 199.5   27 0.0 199.5   27 0.0 199.5   27 0.0 199.5   27 0.0 199.5   27 0.0 199.5	3_18				1.92	24	0.0	8.38	25	96.9	I	24	0.0	163.01	<u> </u>				24	l	141.27
16         32         0.0         0.09.3         32         0.0         18.4         99.8         -9         23         28.8         -9         10         116         21         32         0.0         10.0         18.1         41         0.0         18.1         41         0.0         18.1         41         0.0         18.2         41         0.0         18.2         41         0.0         18.2         41         0.0         18.2         41         0.0         18.2         42         96.8         -4         1         0.0         40.24         42         96.8         -4         1         0.0         1.0         40.0         1.0         20.0         1.0         20.0         1.0         90.0         1         20.0         1.0         90.0         1.0         90.0         1         20.0         1.0         90.0         1         20.0         1.0         90.0         1         20.0         1.0         90.0         1.0         90.0         90.0         90.0         90.0         90.0         90.0         90.0         90.0         90.0         90.0         90.0         90.0         90.0         90.0         90.0         90.0         90.0         90.0	16 2   32 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	3_19				181	27	0.0	69.9	30	98.9	I	27	0.0	239.52					27		142.13
16         41         10         18.1.78         41         0.0         18.1.89         42         96.8         -         41         1.0         6.4         41         0.0         18.1.78         41         0.0         18.1.78         41         0.0         18.1.89         28         10.0         2         24.7         2         3         0.0         40.24         23         0.0         40.24         23         0.0         40.24         25         0.0         11.83         20         0.0         1.83         30         96.0         2         0.0         10.93         2         2         0.0         10.93         2         0.0         10.93         2         2         0.0         10.93         2         2         0.0         10.93         2         2         0.0         10.93         2         2         0.0         10.93         2         2         0.0         10.93         2         2         0.0         10.93         2         2         0.0         10.93         2         2         0.0         10.93         2         2         0.0         10.93         2         2         0.0         10.93         2         2         2         0.0<	14   10   181.78   41   10   16.89   42   96.8   -4   1   21.1   -4   1   1   10   54.16   41   37.4     17   18   23   0.0   97.19   23   0.0   10.89   28   100.0   -2   29   24.1   23   0.0   0.0   31.94   20   0.0     17   18   20   0.0   127.01   20   0.0   1.83   30   96.9   -2   20   0.0   193.3   27   0.0   0.0   31.94   20   0.0     17   19   24   0.0   34.76   24   0.0   3.09   24   99.5   -2   24   0.0   0.37.61   24   0.0   0.0   0.0     17   19   24   0.0   34.76   24   0.0   3.09   24   99.5   -2   24   0.0   0.37.61   24   0.0   0.0     17   10   24   0.0   34.76   24   0.0   3.09   24   99.5   -2   24   0.0   0.37.61   24   0.0   0.0     17   10   24   0.0   34.76   24   0.0   12.86   31   97.4   -2   91.5   -2   29   0.0   0.0     17   10   24   0.0   34.76   24   0.0   12.86   31   97.4   -2   91.5   -2   29   0.0   0.0     17   10   24   0.0   34.76   24   0.0   13.69   32   99.7   -3   24.4   -3   24   0.0   0.0     17   10   24   0.0   17.78   24   0.0   13.89   32   99.7   -3   24.4   -3   24   0.0   0.0     17   10   24   0.0   0.0   24.16   33   100.0   -4   27   24.5   -4   25   0.0   0.0     17   20   27   0.0   17.85   27   0.0   24.16   31   100.0   -4   27   24.5   -4   25   0.0   0.0     17   20   27   0.0   24.16   31   100.0   -4   27   24.5   -4   25   0.0   0.0     18   19   27   10.4   -4   25   0.0   33.24   26   98.2   -4   25   34.7   -4   25   0.0   0.0     18   19   25   0.0   26.24   25   24   0.0   24.16   24   25   24   24   24     18   19   24   24   24   24   24   24   24   2	6_21				.33	32	0.0	18.46	34	8.66	I	32	28.8	ı	32			16.3		27.0	I
17         18         23         0.0         97.19         23         0.0         1.08         28         100.0         -         23         24.7         0         40.24         25         0.0         40.24         20         0.0         1.0         0	17   8   23   0.0   97.19   23   0.0   10.89   28   100.0   0.0   24.7   0.0   25.9   0.0   31.94   20   0.0   0	6_24				78	41	0.0	16.89	42	8.96	I	41	21.1		41			.16		37.4	I
17         18         20         0.0         127         18         20         0.0         127         19         20         0.0         127         18         20         0.0         427         20         0.0         127         19         26         0.0         4.0         6.7         20         0.0         1.2         20         0.0         4.0         6.7         20         0.0         1.2         20         0.0         1.	17   18   20   0.0   127.01   20   0.0   6.79   21   100.0   20   0.0   105.16   26   0.0   31.94   20   0.0   17.1   26   0.0   17.2   26   0.0   1.83   30   96.0   26   0.0   105.16   26   0.0   105.16   26   0.0   105.16   26   0.0   105.16   26   0.0   105.16   26   0.0   105.16   26   0.0   105.16   26   0.0   105.16   26   0.0   105.16   26   0.0   105.16   26   0.0   105.16   26   0.0   105.16   26   0.0   105.16   27   0.0   105.16   27   0.0   105.16   28   0.0   105.17   29   29   29   29   29   29   29   2	7_18				7.19	23	0.0	10.89	28	100.0	ı	23	24.7		23				23	0.0	213.7
17         26         0.0         46.76         26         0.0         183         96.0         -         26         0.0         169.16         27         0.0         169.16         26         0.0         169.17         27         0.0         183         36.9         96.9         -         27         0.0         187.1         36.9         96.9         -         27         10.0         68.73         27         0.0         68.73         27         0.0         18.73         27         0.0         27.2         0.0         18.74         28         0.0         18.74         29         18.74         29         18.75         18         18.74         29         18.75         20         18.74         20         18.74         20         18.74         20         18.74         20         18.74         20         18.74         20         18.74         20         18.74         20         18.74         20         18.74         20         18.74         20         18.74         20         18.74         20         18.74         20         18.74         20         18.74         20         18.74         20         18.74         20         20         20         20 <th< td=""><td>  17   19   26   0.0   46.76   26   0.0   1.83   30   96.0   26   0.0   169.16   26   0.0</td><td>7_18</td><td></td><td></td><td></td><td>7.01</td><td>20</td><td>0.0</td><td>6.79</td><td>21</td><td>100.0</td><td>ı</td><td>20</td><td>0.0</td><td>128.34</td><th></th><td></td><td></td><td></td><td>20</td><td>0.0</td><td>85.61</td></th<>	17   19   26   0.0   46.76   26   0.0   1.83   30   96.0   26   0.0   169.16   26   0.0	7_18				7.01	20	0.0	6.79	21	100.0	ı	20	0.0	128.34					20	0.0	85.61
17         19         27         0.0         112.7         27         0.0         9.92         35         96.9         2         12.7         2         0.0         68.73         24         0.0         237.01         24         0.0         34.7         2         4         99.5         2         4         0.0         24.4         0.0         34.7         2         2         15.5         0         15.4         0.0         15.6         3.0         15.6         3.0         15.6         3.0         15.6         3.0         15.2         3.0         15.2         3.0         15.2         3.0         15.2         3.0         15.2         3.0         15.2         3.0         15.2         3.0         15.2         3.0<	17   19   27   10.0   112.7   27   10.0   9.92   35   96.9   27   12.7   27   12.7   24   0.0   16.47   24   0.0   12.7   24   0.0   34.76   24   0.0   34.76   24   0.0   34.76   24   0.0   34.76   24   0.0   34.76   24   0.0   34.76   24   0.0   34.76   24   0.0   34.76   24   0.0   34.76   24   0.0   34.76   24   0.0   34.74   32   0.0   12.36   31   97.4   0.0   24.44   32   0.0   12.36   31   97.4   0.0   24.44   32   0.0   12.36   31   97.4   0.0   24.44   32   0.0   12.36   31   0.0   0.0   47.5   0.0   17.20   31   0.0   0.0   47.5   0.	7_19				3.76	26	0.0	1.83	30	96.0	I	26	0.0	169.16				-	26		107.41
17         19         24         0.0         34.76         24         0.0         34.76         24         0.0         34.76         24         0.0         34.76         24         0.0         237.61         24         0.0         240.43         29         0.0         12.36         31         97.4         0         20         10.4         32         0.0         240.44         32         0.0         13.69         32         0.0         27         0.0         11.78         0.0         31.80         0.0	17         19         24         0.0         34.76         24         0.0         34.76         24         0.0         34.76         24         0.0         34.76         24         0.0         34.76         24         0.0         32.0         0.0         12.36         31         97.4         0         29.7         0         29.7         0         29.7         0         29.7         0         29.7         0         29.7         0         20.0         20.0         20.0         17.27         29         99.7         0         27.4         0	7_19				2.7	27	0.0	9.92	35	96.9	I	27	12.7		27				27		153.72
17         29         0.0         240.43         29         0.0         12.36         31         97.4         -         29         15.5         -         29         0.0         240.44         32         0.0         17.5         3         24.4         32         0.0         17.5         3         24.4         3         20.0         17.5         3         0.0         20.4.44         32         0.0         17.5         3         0.0         17.5         3         0.0         17.5         3         0.0         17.5         3         0.0         0.0         24.44         3         0.0         0.0         24.44         3         0.0         0.0         24.44         3         0.0         0.0         24.44         3         0.0         20.7         0.0         24.44         3         0.0         0.0         24.0         0.0         0.0         14.5         10.0         0.0         14.5         10.0         0.0         14.5         10.0         0.0         14.0         10.0         0.0         14.0         10.0         0.0         14.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0         10.0	17         19         29         0.0         240.43         29         0.0         12.36         31         97.4         -         29         15.5         -         29         0.0         6         0         12.36         32         99.7         -         29         15.5         -         29         0.0         32         24.4         -         29         0.0         32         24.4         -         29         0.0         32         24.4         -         29         0.0         32         0.0         32         24.4         -         29         0.0         32         0.0         32         24.4         -         27         45.2         0.0         32         0.0         31         10.0         44         31         100.0         41         31         100.0         44         31         100.0         44         31         0.0         11         10         10         24.1         33         100.0         44         31         0.0         31         10         0         31         0.0         31         0.0         32         31         0.0         31         0.0         32         31         0.0         32         32	7_19				1.76	24	0.0	3.09	24	99.5	I	24	0.0	237.61					24		167.54
17         20         42         0.0         13.69         32         99.7         -         32         24.4         9         4.48         32         99.7         -         32         24.4         9         34.48         32         30.0         34.85         37.5         -         27         0.0         34.16         33         100.0         -         45         37.5         -         45         0.0         62.44         45         100.0         -         45         10.0         24.16         33         100.0         -         45         37.5         -         45         0.0         62.45         45         100.0         -         45         10.0         24.16         31         10.0         -         45         37.5         -         45         0.0         15.24         45         100.0         22.2         22.0         45         37.5         47         37         30.0         27         20.0         27         20.0         30.0         20.0         30.0         20.0         30.0         30.0         30.0         30.0         30.0         30.0         30.0         30.0         30.0         30.0         30.0         30.0         30.0         <	17         20         32         0.0         204.44         32         0.0         13.69         32         99.7         -         32         24.4         -         32         0.0         31         20         32         24.4         -         32         0.0         31         17         20         37         0.0         31         18         19         27         0.0         17.27         29         97.9         -         27         45         0.0         26.54         45         100.0         -         45         37.5         -         45         0.0         36.34         45         100.0         -         45         37.00         -         45         30.0         26.54         45         100.0         -         45         30.0         36.54         45         100.0         -         45         30.0         36.54         45         100.0         -         45         30.0         37.5         45         30.0         37.5         45         30.0         37.5         45         30.0         37.5         45         30.0         37.5         47.5         30.0         37.5         47.5         30.0         37.5         47.7         25	7_19				.43	29	0.0	12.36	31	97.4	I	29	15.5	ı	29			.71		10.3	I
17         20         47         0.0         17.27         29         97.9         27         45.2         2         7         6.0         33.16         27         23.1         20         27         45.0         45         0.0         17.27         31         10.0         24.16         33         100.0         45         37.5         45         0.0         62.44         31         10.0         45         37.5         45         0.0         62.44         31         10.0         45         37.5         45         0.0         15.3         45         24.0         45         0.0         62.40         45         10.0         45         37.5         45         0.0         10.20         45         10.0         20.2         45         10.0         20.2         27         20.0         20.2         27         10.0         20.2         27         20.0         10.2         20.2         10.0         20.2         20.0         10.2         20.0         20.0         20.0         20.0         20.0         20.0         20.0         20.0         20.0         20.0         20.0         20.0         20.0         20.0         20.0         20.0         20.0         20.0	17         20         27         0.0         17.27         29         97.9         -         27         45.2         -         27         0.0         5.4         0         7.23         31         9.0         -         31         10.0         -         45         10.0         -         45         10.0         -         45         10.0         -         45         10.0         -         45         10.0         -         45         10.0         -         45         10.0         -         45         10.0         -         45         10.0         -         45         10.0         -         45         10.0         -         45         10.0         -         45         10.0         6         11         11         11         11         11         11         12         12         10.0         11         10         10         11         10         10         10         11         10 <t< td=""><td>7_20</td><td></td><td></td><td></td><td>1.44</td><td>32</td><td>0.0</td><td>13.69</td><td>32</td><td>99.7</td><td>I</td><td>32</td><td>24.4</td><td></td><th>32</th><td></td><td></td><td>.48</td><td></td><td>30.3</td><td>I</td></t<>	7_20				1.44	32	0.0	13.69	32	99.7	I	32	24.4		32			.48		30.3	I
17         23         31         9.0         -         31         9.0         -         4.1         33         100.0         -         4.1         9.0         -         4.1         3.1         9.0         -         4.1         9.0         -         4.1         9.0         -         4.1         9.0         -         4.1         9.0         -         4.1         9.0         9.2         1.2         9.0 <td>17         23         31         9.0         -         31         0.0         24.16         33         100.0         -         45         37.5         -         45         0.0         11         20         45         31         19.8         -         31         0.0         11         20         45         0.0         26.54         45         100.0         -         45         37.5         -         45         0.0         11         18         19         27         10.4         -         27         0.0         20         20         27         20         0.0         20         20         18         19         26         10.0         10         20         20         10         20</td> <td>17-20</td> <td></td> <td></td> <td></td> <td>7.85</td> <td>27</td> <td>0.0</td> <td>17.27</td> <td>29</td> <td>97.9</td> <td></td> <td>27</td> <td>45.2</td> <td></td> <th>27</th> <td></td> <td></td> <td></td> <td></td> <td>23.5</td> <td></td>	17         23         31         9.0         -         31         0.0         24.16         33         100.0         -         45         37.5         -         45         0.0         11         20         45         31         19.8         -         31         0.0         11         20         45         0.0         26.54         45         100.0         -         45         37.5         -         45         0.0         11         18         19         27         10.4         -         27         0.0         20         20         27         20         0.0         20         20         18         19         26         10.0         10         20         20         10         20	17-20				7.85	27	0.0	17.27	29	97.9		27	45.2		27					23.5	
17         29         45         6.4         4         6.4         4         6.4         4         6.4         4         6.4         4         6.4         4         6.4         4         17         29         6         4         3.7.5         4         17         29         0         27         10.0         22.21         27         99.0         27         29.0         27         0.0         59.55         27         14.0         27         20.0         27.0         20.0         27.0         20.0         27.0         20.0         27.0         20.0         27.0         20.0         <	17         29         45         6.4         -         45         0.0         26.54         45         100.0         -         45         37.5         -         45         0.0         11         20         27         10.0         20.221         27         99.0         -         27         29.0         -         27         0.0         31.2         31         100.0         -         27         29.0         -         27         0.0         31.2         31         100.0         -         26         27         0.0         32         0.0         26         27         0.0         32         0.0         31.2         32         100.0         -         26         30         0.0         31.2         32         100.0         -         27         29         0.0         30         32         30         0.0         32.2         100.0         32         30	7_23			9.0	1	31	0.0	24.16	33	100.0	ı	31	19.8		31			.45		14.5	I
18         19         27         10.4         -         27         0.0         22.21         27         99.0         -         27         29.6         -         27         0.0         25.5         27         14.0         -         26         24.0         -         26         24.0         -         26         13.6	18         19         27         10.4         -         27         0.0         22.21         27         99.0         -         27         20         20         27         0.0         31         40         20         22.1         20	7.29			3.4	I	45	0.0	26.54	45	100.0	I	45	37.5		45			.13		24.6	1
18         19         26         15.3         -         26         0.0         17.08         31         100.0         -         24.0         -         26         24.0         -         26         24.0         -         26         24.0         -         25         0.0         78.3         2         28.3         2         28.2         2         20.0         33.24         26         98.2         -         25         34.7         -         25         0.0         63.94         25         10.0         33.24         2         20.0         10.851         29         10.0         10.15         35         100.0         33         48.2         -         26         0.0         18.2         2         20         10.0         31.25         33         100.0         33         48.2         30         0.0         10.15         37         10.0         33         48.2         30         0.0         10.0         30	18         19         26         15.3         -         26         0.0         17.08         31         100.0         -         26         24.0         -         26         24.0         -         26         0.0         6         0.0         17.08         31         100.0         -         25         34.7         -         25         0.0         10         18         20 <td>8_19</td> <td></td> <td></td> <td>).4</td> <td>I</td> <td>27</td> <td>0.0</td> <td>22.21</td> <td>27</td> <td>99.0</td> <td>I</td> <td>27</td> <td>29.6</td> <td>   </td> <th>27</th> <td></td> <td></td> <td></td> <td></td> <td>14.0</td> <td>I</td>	8_19			).4	I	27	0.0	22.21	27	99.0	I	27	29.6		27					14.0	I
18         26         6.0         6.2         9.7         25         34.7         2         25         0.0         63.94         25         19.2         2         34.7         2         25         0.0         63.94         25         19.2         2         34.7         2         34.7         2         34.7         2         34.7         3         48.7         3         48.2         3         48.2         3         48.2         3         48.2         3         48.2         3         60.0         18.3         3         48.2         3         60.0         18.3         3         48.2         3         60.0         18.3         3         48.2         3         60.0         18.3         3         48.2         3         60.0         18.3         18.3         18.2         18.2         19.2	18         19         25         0.0         262.74         25         0.0         33.24         26         98.2         -         25         34.7         -         25         0.0         6           18         20         20         82.99         29         0.0         10.15         35         100.0         33         43.2         -         29         0.0         10.15         33         100.0         33         43.2         -         29         0.0         10.15         33         100.0         33         43.2         -         29         0.0         11.2         33         43.2         -         32         0.0         13         13         100.0         33         43.2         -         30         0.0         11         30         100.0         33         100.0         33         43.2         -         30         0.0         11         30         100.0         30 <td>8_19</td> <td></td> <td></td> <td>5.3</td> <td>1</td> <td>26</td> <td>0.0</td> <td>17.08</td> <td>31</td> <td>100.0</td> <td>Ι</td> <td>26</td> <td>24.0</td> <td>1</td> <th>26</th> <td></td> <td></td> <td>8.3</td> <td></td> <td>13.6</td> <td>I</td>	8_19			5.3	1	26	0.0	17.08	31	100.0	Ι	26	24.0	1	26			8.3		13.6	I
18         20         90         0.0         82.99         29         0.0         10.15         35         100.0         30         58.0         2         29         0.0         198.51         39         20         30         10.98.51         30         20.0         198.51         30         31.23         31.23         30	18         20         90         82.99         29         0.0         10.15         35         100.0         -         30         58.0         -         29         0.0         11         32         100.0         -         33         43.2         -         20         10         11         11         12         20         10         31.25         33         100.0         -         31         24.2         -         32         0.0         10         11         12         13         24.2         -         30         0.0         10         10         11         11         12         13         14.1         -         27         0.0         11         14 <t< td=""><td>8_19</td><td></td><td></td><td></td><td>2.74</td><td>25</td><td>0.0</td><td>33.24</td><td>26</td><td>98.2</td><td>-</td><td>25</td><td>34.7</td><td></td><th>25</th><td></td><td></td><td>.94</td><td></td><td>19.3</td><td>1</td></t<>	8_19				2.74	25	0.0	33.24	26	98.2	-	25	34.7		25			.94		19.3	1
18         20         33         48.5         -         48.5         -         48.5         -         48.5         -         48.5         -         48.5         -         48.2         -         43.2         -         43.2         -         43.2         -         34.3         100.0         -         31         24.2         -         30         0.0         18.3         30         0.0         26.1         37         0.0         27         41.1         -         27         0.0         28.5         27         0.0         27.5         27         0.0         27.5         27         0.0         27.5         27         0.0         27.5         27         0.0         27.5         27         0.0         27.5         27         0.0         27.5         27         0.0         27.5         27         0.0         27.5         27         0.0         27.5         27         0.0         27.5         27         0.0         27.5         27         27.5         27.5         27.5         27.5         27.5         27.5         27.5         27.5         27.5         27.5         27.5         27.5         27.5         27.5         27.5         27.5         27.5	18         20         33         48.5         -         32         0.0         31.25         33         100.0         -         33         43.2         -         32         0.0         125.88         30         0.0         26.15         37         98.1         -         31         24.2         -         30         0.0         18         20         0.0         26.15         37         98.1         -         31         24.2         -         30         0.0         18         20         0.0         26.15         37         0.0         32         100.0         -         27         41.1         -         27         0.0         18         18         21         17.8         -         27         0.0         33         20         100.0         -         36.8         -         37         17.6         37         17.6         37         17.6         37         17.6         37         17.6         37         17.6         37         17.6         37         17.6         38         17.0         18.2         18.0         18.0         18.0         18.0         18.0         18.0         18.0         18.0         18.0         18.0         18.0	8_20				66.7	59	0.0	10.15	35	100.0		30	58.0		29			.51		21.8	-
18         20         30         0.0         215.88         30         0.0         26.15         37         98.1         -         31         24.2         -         30         0.0         183.65         30         37.9         37.9           18         21         27         0.0         61.62         27         0.0         59.4         100.0         -         27         41.1         -         27         0.0         22.5         27         0.0           18         21         27         0.0         81.64         25         0.0         53.6         25         100.0         -         25         0.0         22.9         29         0.0         25         25         0.0         25.8         -         25         0.0         25.8         -         25         0.0         25.8         -         25         0.0         25.9         0.0         25.9         25         100.0         25.8         25         100.0         25.8         25         100.0         25.9         25         25.9         25         25.9         25         25.9         25         25.9         25         25.9         25         25.9         25         25.9         <	18         20         30         0.0         215.88         30         0.0         26.15         37         98.1         -         31         24.2         -         30         0.0         11           18         21         27         0.0         61.62         27         0.0         3.9         100.0         -         27         41.1         -         27         0.0           18         21         27         0.0         61.62         27         0.0         56.41         39         100.0         -         38         36.8         -         37         17.6           18         21         25         0.0         81.64         25         0.0         124.63         65         100.0         -         58         51.3         -         25         0.0         25         4.5         -         25         100.0         -         58         10.0         25         4.5         -         25         100.0         26         26         4.5         -         25         10.0         26         4.5         -         25         4.5         -         25         4.5         -         26         26         9.0         -	8-20			3.5	I	32	0.0	31.25	33	100.0		33	43.2					.94		23.3	_
18         21         27         0.0         61.62         27         0.0         3.9         100.0         -         27         41.1         -         27         0.0         22.5         27         0.0         27         0.0         27         41.1         -         27         0.0         22.3         28.3         28.3         36.8         -         37         17.6         -         37         28.3           18         21         25         0.0         3.36         25         100.0         25         35.8         -         25         0.0         22.9         25         0.0         22.9         25         0.0         22.9         25         0.0         22.9         25         0.0         25         35.8         25         35.8         25         35.8         25         35.8	18         21         27         0.0         3.9         100.0         -         27         41.1         -         27         0.0           18         21         37         17.8         -         37         0.0         56.41         39         100.0         -         27         41.1         -         27         0.0           18         21         37         17.8         -         37         0.0         56.41         39         100.0         -         25         35.8         -         25         0.0         37         17.6           18         21         25         0.0         3.36         25         100.0         25         35.8         -         25         0.0         37         17.6           19         20         26         0.0         124.63         65         98.0         -         56         30.9         25         4.5         90.0         30.0	8-20				88.	30	0.0	26.15	37	98.1	I	31	24.2	l	30			.65		37.9	_
18         21         37         17.8         3         66.41         39         100.0         38         36.8         3         37         17.6         3         38         38.8         36.8         37         17.6         3         38         38.8         36.8         36.8         36.8         36.8         36.8         36.9         36.9         36.8         36.8         36.9         36.9         36.8         36.8         36.9         36.8         36.8         36.9         36.9         36.8         36.9<	18         21         37         17.8         -         37         0.0         56.41         39         100.0         -         38         36.8         -         37         17.6           18         21         25         0.0         81.64         25         0.0         3.36         25         100.0         -         25         35.8         -         25         0.0         25         0.0         25         0.0         25         0.0         25         0.0         25         0.0         25         0.0         25         0.0         25         0.0         25         0.0         25         0.0         25         0.0         25         0.0         26         44.8	8-21				62	27	0.0	3.9	59	100.0	-	27	41.1	1	27				27		68.89
18         21         25         0.0         81.64         25         0.0         33.8         25         100.0         25         35.8         2         25         0.0         25.8         2         25         0.0         22.91         25         0.0         20.91         20	18         21         25         0.0         8.36         25         100.0         -         25         100.0         -         25         35.8         -         25         0.0         26         0.0         23.6         25         100.0         -         25         21.3         -         25         0.0         26         27         26         0.0         269.9         32         100.0         -         26         36         3	8-21			8.7	Ι	37	0.0	56.41	39	100.0		38	36.8		- 37		<u>;</u>	_		28.3	
18 32         56 72.0         45         0.0         124.63         65         98.0         5         51.3         5         4.	18 32         56 72.0         -         55 0.0         124.63         65 98.0         -         58 51.3         -         55 4.5         4.5         4.5         -         4.5         -         56 0.0         124.63         65 98.0         -         58 51.3         -         55 4.5         4.5         -         59 4.5         -         56 9.6         -         56 9.6         -         56 9.6         -         56 9.6         -         56 9.6         -         56 9.6         -         50 9.6         -         50 9.6         -         50 9.0         -         50 9.7         -         50 9.0         -         50 9.7         -         30 9.7         -         30 9.7         -         30 9.0         -         30 9.7         -         30 9.7         -         30 9.0         -         -         30 9.7         -         30 9.7         -         30 9.7         -         -         30 9.0         -         -         -         -         30 9.0         -	8-21				64	25	0.0	3.36	25	100.0	-	25	35.8		25			1	25		211.79
19 20         26 45.0         26 45.0         269.9         32 100.0         269.9         26 26.9         26 26.9         26 9.6         26 9.6         26 9.6         26 9.6         26 9.6         26 26.9         26 9.6         26 9.6         26 9.6         26 9.6         26 9.6         26 9.6         26 9.6         27 34.8         29 9.6         27 34.8         27 34.8         29 9.7         28 34.8         29 9.0         27 34.8         29 9.7         28 34.8         29 9.0         23 4.6         28 9.0         23 4.8         29 9.7         28 34.8         29 9.0         28 4.8         28 9.0         28 4.8         29 9.0         28 4.8         29 9.7         29 9.7         20 9.0         20 9.0         28 4.9         30 9.7	19 20         26 45.0         -         26         0.0         269.9         32         100.0         -         26         26         9.6 </td <td>8-32</td> <td></td> <td></td> <td>5.0</td> <td>I</td> <td>22</td> <td></td> <td>24.63</td> <td>65</td> <td>98.0</td> <td>I</td> <td>28</td> <td>51.3</td> <td>1</td> <th>- 55</th> <td></td> <td>)</td> <td>Ι</td> <td>22</td> <td>59.4</td> <td>I</td>	8-32			5.0	I	22		24.63	65	98.0	I	28	51.3	1	- 55		)	Ι	22	59.4	I
19         20         29         7.2         29         0.0         14.46         30         99.2         -         29         44.8         -         29         0.0         73.48         29           1         19         21         30         11.3         -         30         0.0         16.27         42         99.1         -         30         50.0         30         0.0         84.98         30           1         21         30         8.1         -         30         0.0         16.37         30         96.7         -         30         34.6         -         30         0.0         65.3         30	19         20         29         7.2         29         0.0         14.46         30         99.2         29         244.8         29         20         20         20         20         20         20         20         20         20         20         20         20         20         20         20         30	9_20			5.0	I	26	0.0	269.9	32	100.0	I	26	26.9	1	26		3	Ι	26	37.1	I
. 19 21 30 8.1 a	19 21     30 11.3     -     30 0.0 16.22     42 99.1     -     30 50.0     -     30 0.0 8       19 21     30 8.1     -     30 0.0 16.37     30 96.7     -     30 34.6     -     30 0.0	9-20			7.2		29	0.0	14.46	30	99.2	-	29	44.8		- 29			.48		35.3	ı
$21$ $  19 \ 21   30 \ 8.1 \ -  30 \ 0.0 \ 16.37   30 \ 96.7 \ -  30 \ 34.6 \ -  30 \ 0.0 \ 65.3   30$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	9-21			1.3	I	30	0.0	16.22	42	99.1	I	30	50.0	l	30			86.		23.0	_
	Continued on next page	9-21			3.1	I	30	0.0	16.37	30	96.7	I	30	34.6		30			5.3		40.6	I

Table 13 – Continued from previous page

	SC1		SC2			SC3	1		PR1			PR2	2		PR3	
QU)	gap time	best	gap	time	$\mathbf{best}$	gap	$_{ m time}$	best	gap	time	$\mathbf{best}$	t gap	$_{ m time}$	best	gap	time
$\overline{}$	14.3	32	0.0	20.01	35	100.0	I	32	45.7	I	32	0.0	27.66	32	40.0	1
$\mathcal{L}$	54.8	31	0.0	21.05	32	100.0	I	31	41.9	I	31	0.0	136.72	31	40.3	1
	- $        -$	46	0.0	134.75	59	100.0	I	46	62.4	I	46	4.9	1	46	38.4	1
	55.6	45	0.0	58.64	46	99.3	1	48	59.8	I	45	8.1		45	55.5	1
	17.6	35	0.0	75.2	36	8.66	1	36	55.7	ı	35	5.7		36	37.7	1
ı - '	26.0	36	0.0	50.32	20	100.0	1	36	40.3	ļ	36	0.0	108.17	36	39.4	1
ı - '	-0.06	30	0.0	41.0	43	100.0	I	31	35.5	I	30	0.0	129.2	30	44.3	I
ı	59.8	32	0.0	26.76	35	100.0	1	34	47.1	I	32	8.4		33	50.5	ı
ı - '	-22.9	34	0.0	75.2	37	100.0	I	34	26.1	I	34	7.8	1	34	35.0	1
1 -	35.3 –	43	0.0	257.15	46	100.0	I	46	65.2	I	43	0.0	240.87	44	52.3	1
1 7 1	26.0	34	0.0	192.32	53	100.0	1	35	45.0	I	34	10.1		34	51.5	
	-12.9	34	0.0	29.79	34	100.0	1	88	68.4	1	34	0.0	166.28	34	44.8	
	51.4 $-$	35	0.0	21.54	36	100.0	1	32	45.7	1	35	0.0	145.01	35	40.5	1
	56.1 $-$	42	0.0	91.43	52	100.0	Ι	24	0.69	I	42	39.0	ı	42	50.4	I
1	73.2	54	3.4	-	59	100.0	1	$^{24}$	63.7	I	54	15.4	1	54	51.4	1
_	- 2.99	43	0.0	46.47	44	100.0	_	77	55.3	_	43	0.0	199.73	44	57.4	
- 1	-1.11	32	0.0	171.65	36	100.0	1	33	59.1	I	32	15.6	I	32	44.0	ı
	17.5 –	33	0.0	29.97	41	100.0	_	88	57.2	_	33	45.4	_	33	52.9	
` `	27.7	31	0.0	39.74	26	100.0	-	32	63.3	1	31	0.0	198.29	32	48.5	
• •	-20.8	36	0.0	114.02	43	100.0	Ι	88	50.0	I	36	19.1	I	36	61.6	I
-	63.4 $-$	39	0.0	63.46	45	100.0	1	68	55.9	Ι	39	29.3	1	39	37.5	1
_	63.4 $-$	40	0.0	44.01	99	100.0	_	40	8.79	_	40	0.0	231.48	40	53.2	Ι
- •	32.7 —	45	0.0	92.86	22	100.0	_	09	68.3	-	45	15.1	_	47	64.5	-
,	7.07	45	0.0	78.58	61	98.4	_	09	63.5	_	45	9.4	_	45	45.9	-
•	34.4	54	1.8	I	54	100.0	1	54	63.3	ı	54	16.4		54	55.0	
1	76.3	28	5.0	I	85	100.0	1	28	78.2	ı	78	14.1		78	60.3	1
١٠١	24.8	38	0.0	128.52	54	100.0	1	88	61.2	Ι	38	10.9		38	57.3	1
1	71.6	53	0.0	177.5	28	100.0	1	55	9.99	ı	53	15.6		53	62.9	I
_	75.1 $-$	48	6.1	_	92	100.0	_	22	74.3	_	48	21.9	_	48	61.3	I
					į								Cont	Continued	on next page	t page

Table 13 – Continued from previous page

		-	SC			SC2			SC3	4		PR1			PR2			PR3	
Name	n = n	$m \mid \text{best}$	Ç.	time	best	010	time	best	gap	time	$\mathbf{best}$	0.0	time	$\mathbf{best}$	Ç.	time	best	ÇII)	time
$p79_{-}22_{-}29$	22 29	9 53	3 46.0	Ī	20	2.6	1	64	100.0	I	51	9.89	I	50	16.8	I	20	54.0	I
$p74_{-}22_{-}30$	22 30	0 43	3 27.5	I	43	0.0	56.68	59	100.0	I	44	57.5	I	43	5.0	I	43	59.9	I
$p76_{-}22_{-}30$	22 30	0 45	5 66.7	Ī	45	20.8	I	22	100.0	I	48	71.6	Ī	45	23.3	ļ	45	2.99	ı
p80_22_30	22 30	0 53	3 70.1	I	52	4.0		29	100.0		52	72.1	I	52	21.6	I	52	55.8	
p78_22_31	22 31	1 50	0 31.7		20	0.0	102.94	62	100.0	1	55	70.9		50	8.5	I	20	59.6	
$p77_{-}22_{-}37$	22 37	22 2	77.0	_	74	10.0	_	88	100.0	I	22	66.4		74	30.4	_	92	65.1	1
$p72_{-}22_{-}49$	22 49	9 104	4 83.7	Ī	101	13.6	I	110	100.0	I	102	6.07	Ī	101	34.2	I	103	82.7	I
p82_23_24	23 24	4 33	3 23.1	Ī	33	0.0	289.56	22	100.0	I	36	38.9	Ī	33	24.5	ı	33	54.5	I
p83_23_24	23 24	4 32	2 33.6	ı	32	0.0	173.52	53	100.0	I	34	9.09	Ī	32	27.6	ļ	34	62.4	I
p86_23_24	23 24	4 31	1 24.5	I	31	0.0	99.92	48	100.0	I	31	36.4	Ī	31	10.1	ļ	32	46.9	I
p84_23_26	23 26	$6 \mid 36$	9 69.2	_	39	0.0	260.88	22	100.0	Ι	40	73.3		39	50.3	_	40	52.9	1
p85_23_26	23 26	$6 \mid 33$	3 35.1	_	33	7.4	_	48	100.0	I	34	68.2		33	28.1	_	33	48.9	1
$p88_{-}23_{-}26$	23 26	6 44	4 71.8	I	43	5.5	I	28	100.0	I	49	67.2		43	30.3	T	45	63.1	ı
p89_23_27	23 27	7 52	2 75.8	1	20	0.0	269.54	80	100.0	Ι	51	2.99	I	50	53.9	-	51	63.5	1
$p87_{-}23_{-}30$	23 30	$09 \mid 0$	0 74.6	_	26	8.1	-	88	100.0	Ι	61	75.7		61	39.8	_	09	2.99	1
$p90_{-}23_{-}35$	23 3	$35 \mid 63$	3 59.6	I	63	0.0	166.26	109	100.0	I	64	8.89		69	34.0	_	99	62.2	1
p81_23_46	23 46	6   111	1 79.9	_	102	17.1	_	110	100.0	Ι	103	73.0		102	44.7	_	105	83.1	1
p92_24_26	24 26	$6 \mid 44$	476.0	Ī	42	0.0	282.26	29	100.0	I	43	62.8		43	33.8	_	45	65.6	
p97_24_26	24 26	$28 \mid 9$	9.29 2	Ī	37	0.0	89.11	65	100.0	I	44	65.5		37	22.2	-	28	61.2	
p93_24_27	24 27	7 33	3 33.2	-	33	0.0	96.79	43	100.0	_	34	59.9	Ι	33	20.4	_	36	56.9	1
p95_24_27	24 27	$7 \mid 41$	1 43.8	1	41	4.9	-	69	100.0	Ι	42	71.2	I	41	26.1	-	41	62.7	1
p96_24_27	24 27	7 43	3 67.4	Ī	42	6.9	I	49	100.0	I	48	8.02	Ī	43	60.2	ı	42	2.09	I
p99_24_27	24 27	7 45	5 75.8	Ī	43	8.3	I	80	100.0	I	45	71.3	I	43	27.3	I	43	63.3	1
p98_24_29	$ 24 \ 29 $	9   52	2 77.4	I	45	0.0	108.13	80	100.0	I	51	66.2		45	25.0	_	49	0.07	I
p94_24_31	24 31	$1 \mid 59$	9 56.8	Ī	99	7.0	1	100	100.0	I	62	75.8		22	56.8	_	99	67.9	
p91_24_33	24 33	3 67	7 79.0	_	62	7.5	_	117	100.0	I	29	73.7		62	32.1	_	63	70.5	
p100_24_34	24 34	$4 \mid 60$	0 73.3		22	5.7	I	87	100.0	I	22	73.3	ı	57	26.4		22	8.79	1

Table 14: Detailed results for Optimal Linear Arrangement on the Small data set.

time best GDLAZ 10.98	OLA4 OLA5 OLA6 OLA7 OLA7 OLA8 $[31]$ $[31]+F2$ $[31]+F3$ $[31]+F3$ gap time best gap	36         0.0         18.43         36         0.0         34.18         40         83.9         -         38         79.0         -         36         0.0         203.78         36         0.0         34.29         36         36.0	- <b>39</b> 0.0 20.63 <b>39</b> 0.0 71.29 39 78.5 - 44 87.8 - 39 13.1 - <b>39</b> 0.0 57.74 <b>39</b> 0.0	- 48 0.0 58.5 48 0.0 34.77 51 84.3 - 48 85.4 - 48 8.5 - 48 0.0 54.91 48 0.0 6	53.78 <b>70</b> 0.0 184.84 72 83.3 - 70 91.7 - 71 23.5 - <b>70</b> 0.0 167.65 70 1	23.4 - <b>32</b> 0.0 15.35 <b>32</b> 0.0 31.38 38 80.4 -   32 85.4 -   32 9.9 -   <b>32</b> 0.0 27.7   <b>32</b> 0.0 99.55	0.0 45.37 <b>29</b> 0.0 115.28 29 73.0 - 29 79.3 - 29 17.4 - <b>29</b> 0.0 109.18 <b>29</b> 0.0	27.0 - <b>37</b> 0.0 27.46 <b>37</b> 0.0 98.95 40 77.5 - <b>42</b> 88.1 - <b>37</b> 17.7 - <b>37</b> 0.0 33.35 <b>37</b> 0.0 93.18	-         40         0.0         39.51         40         0.0         99.07         44         88.6         -         44         92.2         -         40         21.3         -         40         0.0         76.64         40         0.0	20 00 00 90 00 00 00 01 8 90 01 0 90 00 0 90 00 64 8 9 90	- 39 U.O 29.38 39 U.O 08.22 39 91.0 - 39 91.0 - 59 9.9 - 39 U.O 08.38 39	40.8 - <b>39</b> 0.0 38.72 <b>39</b> 0.0 115.81 41 84.0 - 39 85.9 - 39 21.1 - <b>39</b> 0.0 157.96 39 11.6 -	-         44         0.0         23.79         44         0.0         129.13         46         84.8         -         44         91.2         -         44         18.8         -         44         0.0         54.33         44	39.8 $   40$ $0.0$ $14.76   40$ $0.0$ $32.72   45$ $90.6$ $   46$ $89.1$ $   40$ $14.4$ $   40$ $0.0$ $33.2   40$ $6.2$ $ 33.2$ $  40$ $6.2$ $   40$ $  40$	34.5  -1 <b>51</b> 0.0  32.35 <b>51</b> 0.0  140.55  51  81.5  -1  51  88.9  -1  51  15.9  -1 <b>51</b> 0.0  66.22  51  15.8  -1  51  15.9  -1  51  -1  51  15.9  -1  51  15.9  -1  51  15.9  -1  51  15.9  -1  51  15.9  -1  51  15.9  -1  51  15.9  -1  51  -1  51  15.9  -1  51  -1  51  15.9  -1  51  15.9  -1  51  15.9  -1  51  15.9  -1  51  15.9  -1  51  15.9  -1  51  15.9  -1  51  -1  51.9  -1  51  -1  51  -1  51.9  -1  51  -1  51.9  -1  51  -1  51.9  -1  -1  51.9  -1  51.9  -1  51.9  -1  51.9  -1  51.9  -1	55.9 -   <b>82</b> 0.0 45.31   <b>82</b> 0.0 96.67   82 87.8 -   82 92.7 -   82 24.1 -   <b>82</b> 0.0 103.1   82 27.6 -	34.4 - <b>35</b> 0.0 49.97 <b>35</b> 0.0 114.37 38 88.8 - 38 89.5 - 35 12.6 - <b>35</b> 0.0 117.2 <b>35</b> 0.0 254.68	17.5         -         32         0.0         84.05         32         0.0         17.6         0.0         17.6         0.0         17.6         0.0         57.8         32         0.0         57.8         32         7.4         -	38.0 <b>- 36</b> 0.0 63.19 <b>36</b> 0.0 143.47 <b>36</b> 86.1 <b>-</b> 43 91.1 <b>-</b> 36 20.9 <b>- 36</b> 0.0 162.03 <b>36</b> 0.0 169.1	51.3 - <b>46</b> 0.0 176.02 <b>46</b> 0.0 295.49 <b>47</b> 91.5 - <b>53</b> 92.4 - <b>47</b> 38.4 - <b>46</b> 15.2 - <b>46</b> 24.7 -	31.9 - <b>44</b> 0.0 107.31 44 4.0 - 48 88.5 - 47 89.4 - 44 24.0 - 44 24.0 - 44 35.9 -	-         48         0.0 201.99         48         0.0 269.52         51         90.2         -         51         96.1         -         48         32.4         -         48         17.0         -         48	-         39         0.0         24.69         39         0.0         234.74         43         83.7         -         45         91.1         -         39         15.9         -         39         0.0         64.81         39	- <b>47</b> 0.0 63.9 47 7.9 - 51 88.7 - 53 90.4 - 47 24.3 - <b>47</b> 0.0 145.38 47	-         39         0.0         95.38         39         0.0         181.25         52         91.3         -         39         88.9         -         39         18.0         -         39         0.0         34.31         39	-         93         0.0         104.24         93         11.6         -         96         90.6         -         93         94.6         -         93         94.8         -         93         7.3         -         93	- <b>36</b> 0.0 117.2 36 13.9 - 51 95.0 - 37 87.4 - 36 39.6 - 36 16.1 - 36 :	29.8	$- \begin{vmatrix} 39 & 0.0 & 78.78 \end{vmatrix} 39 \ 12.3 \qquad - \begin{vmatrix} 42 & 90.5 & -   39 & 89.7 & -   39 & 19.3 & -   39 & 0.0 \end{vmatrix}$	- <b>41</b> 0.0 210.93 <b>41</b> 0.0 207.64 <b>46</b> 90.3 - <b>44</b> 86.4 - <b>41</b> 27.2 - <b>41</b> 0.0 179.43 <b>41</b>	<b>42</b> 0.0 55.29 42 8.1 - 48 88.1 - 51 94.1 - 42 26.5 - 42 2.4 - 42	- <b>45</b> 0.0 80.94 <b>45</b> 0.0 118.77 45 88.9 - 45 91.0 - 45 26.0 - <b>45</b> 0.0 151.27 45	- <b>57</b> 0.0 106.81 57 7.7 - 61 90.2 - 57 90.5 - 57 26.4 - <b>57</b> 0.0 192.87 57	- 70 5.1 - 70 11.4 - 75 90.9 - 71 93.8 - 72 41.3 - 70 27.0 - 70 37.4	- <b>56</b> 0.0 45.27 <b>56</b> 0.0 176.79 69 94.1 - 70 94.0 - 56 24.1 - 56 2.7 - <b>56</b>	- 51 11.8 - 51 4.6 - 66 91.7 - 56 92.3 - 51 20.8 - <b>51</b> 0.0 131.45 51	-         41         0.0         83.29         41         24.7         -         47         91.5         -         52         97.3         -         43         34.5         -         41         0.0         202.16         44	- 59	_	$63.3  - \mid 54  16.9  - \mid 54  41.2  - \mid 65  90.8  - \mid 60  94.3  - \mid 55  42.1  - \mid 55  43.6  - \mid 58  44.7  - \mid 54  44.7  - \mid 64  44.7  - \mid 6$	$58.4  - \mid 50  8.0  - \mid 50  34.0  - \mid 58  96.5  - \mid 52  90.4  - \mid 50  36.8  - \mid 50  33.1  - \mid 52  40.8  - \mid 50  33.1  - \mid 50  40.8  - \mid 50  33.1  - \mid 50  40.8  - \mid 50$	59,7 - <b>51</b> 0.0 91.48 51 3.9 - <b>78</b> 97.4 - 57 91.2 - 51 30.0 - <b>51</b> 0.0 266.94 51 51.7 -	55.6 - <b>56</b> 0.0 129.12 56 21.0 - 66 92.9 - 56 94.5 - 56 35.4 - 56 23.5 - 56 27.9 -	67.9 - <b>70</b> 0.0 260.86 <b>7</b> 0 14.4 - <b>73</b> 95.4 - <b>71</b> 97.0 - <b>7</b> 0 36.9 - <b>7</b> 0 43.0 - <b>7</b> 0 24.6 -	59.0 - <b>73</b> 0.0 139.77 74 15.5 - 88 95.5 - <b>78</b> 96.2 - <b>75</b> 33.3 - <b>73</b> 22.9 - <b>74</b> 27.9 -	61.8 - <b>68</b> 0.0 136.04 68 6.9 - 84 93.5 - 85 97.7 - 68 31.2 - 68 28.6 - 68 20.3 -	53.2 - 44 9.6 - 44 27.3 - 54 94.4 - 49 98.0 - 44 46.3 - 44 30.1 - 44 58.5 -	68.8 - 45 3.3 - 45 35.2 - 55 94.5 - 54 98.2 - 47 47.6 - 45 22.1 - 45 42.2 -
time         best gap time           10.98         36         0.0         0.84           10.98         36         0.0         6.27           24.64         48         0.0         2.7           216.3         70         0.0         11.31           216.3         70         0.0         11.31           31.02         37         0.0         2.27           31.02         37         0.0         2.27           31.02         37         0.0         2.27           33.49         39         0.0         6.29           88.28         39         0.0         5.27           38.40         0.0         2.27           38.29         39         0.0         6.29           88.28         39         0.0         6.29           88.29         39         0.0         5.21           60.44         82         0.0         13.0           1104.26         32         0.0         5.21           65.08         36         0.0         2.29           65.08         44         0.0         2.29           10.2         48         0.0         2.20     <	_		95.3	92.3	95.5	97.3	- 2.96	100.0	98.3	04.0	97.8	93.0	96.9	- 2.96	- 0.66	97.3	99.5	97.0	99.2	99.1	98.5	98.4	100.0	99.5	97.2	- 8.66	- 6.66	- 8.66	-100.0	97.7	9.88	- 6.66	- 2.86	98.4	97.8	100.0	100.0	100.0	-0.001	100.0	100.0	99.4	100.0	- 9.66	100.0	100.0	100.0	100.0
	time best gap time	10.98 <b>36</b> 0.0 0.84	52.2 39 0.0 6.27	24.64 48 0.0 2.7	216.3 70 0.0 11.31	15.78 <b>32</b> 0.0 1.7	96.86 <b>29</b> 0.0 7.44	31.02 37 0.0 3.11	23.4 40 0.0 2.27	33 40 30 0 6 30	33.49 <b>39</b> 0.0 6.29	88.28 39 0.0 8.09	43.33 <b>44</b> 0.0 4.34	30.14 <b>40</b> 0.0 2.89	64.74 <b>51</b> 0.0 7.78	60.44 82 0.0 12.63	<b>35</b> 0.0 3.41	<b>32</b> 0.0 9.74	65.08 36 0.0 10.72	<b>46</b> 0.0 13.0	44 0.0 9.23	62.85 48 0.0 2.39	79.08 39 0.0 2.19	<b>47</b> 0.0 12.13	<b>39</b> 0.0 3.51	- 93 0.0 26.25	- 36 0.0 42.09	48.33 <b>37</b> 0.0 2.27	- <b>39</b> 0.0 14.7	<b>41</b> 0.0 10.36	196.56 <b>42</b> 0.0 4.86	68.42 <b>45</b> 0.0 2.56	- 57 0.0 31.66	- <b>70</b> 0.0 74.78	35.55 <b>56</b> 0.0 3.21	- <b>51</b> 0.0 24.84	189.65 41 0.0 15.49	- <b>47</b> 0.0 46.01	- <b>47</b> 0.0 16.11	- <b>54</b> 0.0 47.64	217.87 50 0.0 20.79	75.92 <b>51</b> 0.0 13.57	98.09 <b>56</b> 0.0 12.03	- 70 0.0 19.34	- 73 0.0 38.18	- 68 0.0 35.81	- 44 0.0 33.17	- <b>45</b> 0.0 17.87

Table 14 – Continued from previous page

		O	OLA1	H	OI,A2	42	L	OLA3	H	OLA4	$\vdash$	OLA5	F	OLA6	+	OLA7	OLA8	[31]		[31]+F2	[31]+F3
Name	n m	m best ga	gap time best gap time best	e pe	est gap	time	best	gap	me be	time best gap time best	me p		e pesi	gap	time be	best gap time best gap time best	best gap	ου	time bes	best gap time	time best gap time
p67_21_22 21 22		<b>40</b> 0.0	.0 125.3	.3 40		0.0 14.64	4 52	100.0	- 4	41 70.6	- 4	40 0.0 133.02	02 40	18.5	- 4	40 92.5 -	46 93.4	- 41 35.4	- 40	41.2	40 41.3 -
	21 23	53 8.2	.2	l TO	<b>53</b> 0.0	32.88	8 64	100.0	ا	54 65.1	1	53 23.1	- 53	35.9	1		65 98.2	- 54 49.9	- 53	3 21.0 -	53 40.1 -
	21 24	52 54.1		  TO	<b>51</b> 0.0	58.39	9 61	100.0	ا	52 68.5		51 0.0 296.44	_	33.0	1	55 92.7 -	67 97.3	- 52 37.4	- 51	11.8	51 30.9 -
p70_21_25	21 25	57 12.9		l JU	<b>57</b> 0.0	29.49	99 6	100.0		58 75.2		<b>57</b> 0.0 220.27	27 57	9.98	-	- 93.9 -		- 57 44.1	- 57	- 33.8 –	57 22.4 -
p68_21_27	21 27	68 8.4		9 -	0.0 89	14.49	9 81	99.2	-	72 63.2	1	68 1.5	- 68	23.8	1	83 95.0 -	68 95.9		- 68	. 5.9	70 42.1 -
p66_21_28 21 28	21 28	77 26.0	0.	_ 1	<b>77</b> 0.0		66.75 99	100.0	- 7	78 64.4	1	77 19.4	- 77	44.4	-	86 95.3 -	77 95.2	- 77 55.9	- 77		77 45.1 -
p62_21_30 21 30	21 30	91 38.2		6 -	<b>91</b> 0.0		45.17 114	6.66		91 69.7	1	91 39.8	- 91		- 1	117 96.6 -	106 98.1	- 93 52.9	- 91	- 30.9	91 55.3 -
p63_21_42	21 42	150 41.2	.2	- 14	<b>148</b> 0.0	l	5 205	217.5 205 100.0	- 1.	151 73.6	1	148 26.2	- 148	8 47.0	- 1	173 97.1 -	170 97.7	- 153 48.3	- 152	2 26.4 -	161 51.9
p75_22_25	22 25	56 19.4		10	55 0.0	0 60.27	22 2	100.0		56 78.0	1	56 18.7	- 56	31.3	-	64 95.3 -	59 96.5	- 56 41.6	- 55	- 8.6	55 28.2 -
	22 29	69 45.2		9 -	0.0 69		7 101	43.7 101 100.0	-	86 69.4		69 0.0 278.35	35 69		1				69 –		- 8.98.9
p73_22_29	22 29		.4	9 –	<b>65</b> 0.0		98 2	100.0			<u> </u>		-   65						- 65		
p79_22_29	22 29	67 28.0	0.	9 -	<b>67</b> 0.0		2 129	60.52 129 100.0	- -	68 61.2	<u> </u>	67 11.4	<u>-</u>	. 44.0	1	79 94.9 -	0.76 75	- 67 48.2	<u>-</u>	7 38.1 –	- 67 55.6 -
p74_22_30   22 30   <b>67</b>	22 30		0.0 284.17	29 21	0.0 78		4 103	9.54 103 100.0	_ e	68 75.0	-	$67  0.0 \ 183.72$	72 67	13.9	-		71 98.6		29 -	7 29.7	67 25.4 –
p76_22_30   22 30		74 30.7	7.	_ 1	<b>73</b> 0.0	93.66	9 114	93.69 114 100.0	- 7	75 68.5	-	73 15.1	- 73		-	81 95.1 -	0.86 97	- 76 44.1	- 73	8.4 –	73 40.0 -
	22 30	75 57.3		_ 7	<b>74</b> 0.0		7 122	50.17 122 100.0	-	74 66.5	1	74 12.5	- 74	46.3	1	- 6.56 86	92 97.0	- 74 38.9	- 74	43.2	74 50.7 -
	22 31	79 17.2		_ 7	<b>79</b> 0.0	0.0 65.54	1 112	112 100.0	-	82 69.4	1	79 10.8	- 79		- 1	105 97.1 -			- 79	44.4	79 47.5 -
p77_22_37	22 37 122	122 42.0		- 12	122 0.0	0.0 160.27	7 166	166 100.0	- 1	125 74.2	_ 1	122 49.9	- 122		- 1	144 97.2 -	135 97.8	- 124 55.2	- 128	8 48.5	127 69.7 -
p72_22_49	22 49 215			- 18	195 9.7		- 262	6.66	- 1.	198 81.7	_ 1	195 67.1	- 195		- 2	223 97.3 -	230 98.1	- 208 47.7	- 202	2 55.9	195 53.8 -
p82_23_24 23_24		56 17.9	6:		<b>26</b> 0.0		57.39 82	100.0		56 65.7	1	56 17.6	- 26	48.2		70 95.7 -	65 98.5	- 58 61.0	- 56	3 23.2 –	- 20.0 -
p83_23_24 23 24 49	23 24	49 12.0		- 4	<b>48</b> 0.0	33.66	98 9	33.66 89 100.0	- 4	48 67.4	1	48 10.0	- 20	33.0		76 97.4 -	60 98.3	- 54 60.6	- 48	48.1	49 59.5 -
	23 24		.1	- 4		) 23.66	-		- 4		1		- 43		-				- 43		
	23 26	53 34.4	.4	- 5	<b>52</b> 0.0	$0.0\ 223.62$	98 7	100.0	ا	55 69.7	1	52 15.7	- 52	44.0	-	62 95.2 -	54 96.3	- 52 52.3	- 53	9.68 8	52 50.3 -
	23 26			- 2	<b>20</b> 0.0		8 90	100.0	ا	50 68.0	-		- 20	46.5	1		0.96 07		- 20	55.4 -	50 51.0 -
	23 26	59 24.7	.7	_ .c	0.0 89		2 103	66.52   103   100.0	1		<u> </u>	60 20.0	09  -		-				- 28	19.1	
p89-23-27	23 27	71 47.9	6.	_ 1	<b>71</b> 0.0	$0.0\ 142.82\  \ 122\ 100.0$	2 122	100.0	- 7	72 67.5	1	71 50.7	- 71		-	91 96.7 -	83 97.6		- 71		72 68.3 -
p87_23_30 23 30 86 51.4	23 30	86 51.	4.	00	83 0.0	0.0 77.96 123 100.0	3 123	100.0	-	87 71.0	-~	89 54.8	- 83	51.2	- 1	103 97.1 -			- 85	55.6 –	
p90_23_35   23 35   105 59.1	23 35	105 59.		- 10	0.0 0.0	<b>100</b> 0.0 105.37   158 100.0	7 158	100.0	- 1	100 65.7	_ 1	100 24.9	- 100	0.54.0	_ 1	136 97.1 -	102 96.1	-   100 51.4	- 100	$100\ 42.1$ $-$	100 59.3
- 1	23 46	185 77.8		- 17	179 13.0	_	- 293	293 100.0	- 1	189 76.2	_ 1	184 37.9	- 179		- 1	- 1	196 98.5	- 1	- 179		191 61.8 -
	24 26		.2	ا ت		$0.0\ 203.88$		100.0	-	61 72.8	-	58 32.1	- 58		-	66 95.5 -	9.86 69		- 58		59 64.4 -
	24 26	٠,		- 2	<b>57</b> 0.0			123 100.0	-	59 69.6	_		- 59		-				- 28		
			0.	_ 70			81	100.0	- (¢		-		- 55		-				- 55		
p95-24-27		60 53.3	.3	- 5	<b>59</b> 0.0		2 110	79.72 110 100.0	-	59 81.8	-		- 59		-	90 97.8 -	82 97.6		- 59		62 65.4 -
p96-24-27		53 20.2	5.	   	53 0.0	0.0 178.39 73 100.0	9 73	100.0	- e	60 70.2	-	58 60.8	- 53	- 1	-	- 1			- 53	51.9	- 1
			4.	- 9	<b>62</b> 0.0	80.5		98 100.0	-		-		- 63		-				- 62		
p98-24-29	24 29	74 32.4	.4	_ 1	71 0.0	96.43	3 107	107 100.0	- 7	79 72.0	1	71 22.1	- 75	52.0	- 1	106 98.1 $-$	74 98.7	- 73 63.3	- 71	. 55.3 -	71 65.7 -
-	24 31	- 1	65	<b>x</b> 0	84 0.0	83.49		119 100.0	-	- 1	.~ 	84 19.2	- 89	- 1	- 1	114 97.0 -	91 98.7	- 1	- 90		86 70.4 -
p91_24_33	24 33 101		6:	- 5	96 3.3		- 136	136 100.0	- 1				- 89		_ 1				- 105		
p100_24_34 24 34	24 34	98 64.2	.2	- 6	<b>98</b> 0.0		7 157	97.67 157 100.0	_ 1	101 75.2	1	98 26.4	- 88	51.5	- 1	118 96.6 -	125 98.4	-10460.7	- 98	3 58.5 -	99 61.4 -