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Geometric and numerical methods in the contrast imaging problem in nuclear magnetic resonance

Bernard Bonnard · Mathieu Claeys · Olivier Cots · Pierre Martinon

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Abstract In this article, the contrast imaging problem in nuclear magnetic resonance is modeled as a Mayer problem in optimal control. The optimal solution can be found as an extremal, solution of the Maximum Principle and analyzed with the techniques of geometric control. This leads to a numerical investigation based on so-called indirect methods using the HamPath software. The results are then compared with a direct method implemented within the Bocop toolbox. Finally `lmi` techniques are used to estimate a global optimum.

Keywords Geometric optimal control · Contrast imaging in NMR · Direct method · Shooting and continuation techniques · Moment optimization.

Introduction

The control in Nuclear Magnetic Resonance (NMR) of a spin-1/2 particle is described by the *Bloch equation* [29]

$$\begin{aligned}\frac{dM_x}{d\tau} &= -M_x/T_2 + \omega_y M_z - \Delta \omega M_y \\ \frac{dM_y}{d\tau} &= -M_y/T_2 - \omega_x M_z + \Delta \omega M_x \\ \frac{dM_z}{d\tau} &= (M_0 - M_z)/T_1 + \omega_x M_y - \omega_y M_x\end{aligned}\tag{1}$$

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where the state variable is the magnetization vector $M = (M_x, M_y, M_z)$, the control is the magnetic field $\omega = (\omega_x, \omega_y, 0)$ bounded by $|\omega| \leq \omega_{\max}$, $\omega_{\max} = 2\pi \times 32.3\text{Hz}$ being the experimental intensity of the experiments [26], $\Delta\omega$ is the resonance offset and τ is the time. In order to normalize our system, we introduce: $q = (x, y, z) = (M_x, M_y, M_z)/M_0$ and q belongs to the Bloch ball $|q| \leq 1$. The time is normalized to $t = \tau \omega_{\max}$ and we introduce the control $u = \omega/\omega_{\max}$, $|u| \leq 1$. In this paper, we assume $\Delta\omega = 0$, leading to the following normalized system:

$$\begin{aligned}\frac{dx}{dt} &= -\Gamma x + u_2 z \\ \frac{dy}{dt} &= -\Gamma y - u_1 z \\ \frac{dz}{dt} &= \gamma(1-z) + u_1 y - u_2 x,\end{aligned}\tag{2}$$

where the parameters $\Gamma = 1/(\omega_{\max} T_2)$ and $\gamma = 1/(\omega_{\max} T_1)$ satisfy $2\Gamma \geq \gamma \geq 0$.

In the contrast problem, we consider two uncoupled spin-1/2 systems corresponding to different particles, each of them solution of the Bloch equation (2) with respective coefficients (γ_1, T_1) , (γ_2, T_2) , and controlled by the same magnetic field. By denoting each system by $\dot{q}_i = f(q_i, \Lambda_i, u)$, $\Lambda_i = (\gamma_i, T_i)$ and $q_i = (x_i, y_i, z_i)$, this leads to consider the system written shortly as $\dot{q} = F(q, u)$, where $q = (q_1, q_2)$ is the state variable and where \dot{q} means the derivative of q with respect to the time t . In the numerical simulations, we shall consider two cases encountered in the experiments, the *physical parameters* being the relaxation times given in seconds.

P_1 : Fluid case.

Spin 1: Cerebrospinal fluid: $T_1 = 2$, $T_2 = 0.3$;

Spin 2: Water: $T_1 = 2.5 = T_2$.

P_2 : Blood case.

Spin 1: Deoxygenated blood: $T_1 = 1.35$, $T_2 = 0.05$;

Spin 2: Oxygenated blood: $T_1 = 1.35$, $T_2 = 0.2$.

Definition 1 The *contrast problem by saturation* is the following *optimal control problem* (OCP): starting from the equilibrium point $q_0 = ((0, 0, 1), (0, 0, 1))$, reach in a given transfer time t_f the fixed state $q_1(t_f) = 0$ (corresponding to the zero magnetization of the first spin, called *saturation*) while maximising $|q_2(t_f)|^2$, the *contrast* being $|q_2(t_f)|$.

We are interested in this article in solving the contrast problem by saturation for a range of values of t_f . The contrast problem can be stated as a *Mayer problem* given by the following smooth conditions:

1. A system $\dot{q} = F(q, u)$, $q \in \mathbf{Q} \subset \mathbb{R}^n$, with

$$\mathbf{Q} = \{q = (q_1, q_2) \in \mathbb{R}^n : |q_1| \leq 1, |q_2| \leq 1\},$$

and fixed initial state $q(0) = q_0$. The control belongs to the control domain $\mathbf{U} = \{u \in \mathbb{R} : |u| \leq 1\}$.

2. A terminal manifold to reach,

$$\mathbf{Q}_f = \{q = (q_1, q_2) \in \mathbb{R}^n : q_1 = 0, |q_2| \leq 1\} \subset \mathbf{Q},$$

defined by $f(q) = 0$, where $f : \mathbb{R}^n \rightarrow \mathbb{R}^k$.

3. A cost to be minimized of the form $\min_{u(\cdot)} c(q(t_f))$ where $c : \mathbb{R}^n \rightarrow \mathbb{R}$ is a regular mapping and t_f is the final time.

The contrast problem by saturation can be summarized this way:

$$(OCP) \begin{cases} c(q(t_f)) = -|q_2(t_f)|^2 \longrightarrow \min_{u(\cdot)}, t_f \text{ fixed} \\ \dot{q} = F(q, u), \\ q(0) = q_0 \\ q_1(t_f) = 0 \end{cases} \quad (OCP)$$

In practical experiments we consider two cases:

- a) The **bi-input case** where $q = (q_1, q_2) \in \mathbb{R}^6 \cap \mathbf{Q}$ and $|u| = \sqrt{u_1^2 + u_2^2} \leq 1$.
- b) The **single-input case** where the system is restricted to $x_1 = x_2 = 0$, the control field is restricted to the real field, i.e., $u_2 = 0$, and each spin is restricted to the plane $q_i = (y_i, z_i)$.

The contrast imaging problem was analyzed in a series of recent articles using geometric optimal control [8,9] or numerical indirect methods [11], and leads to experimental work described in [12,26], but restricted mainly to the single-input case. In such studies, the contrast problem is essentially reduced to the analysis of the so-called singular trajectories of the system modeling the problem. The objective of this article is to complete the geometric and the numerical analysis of the problem. Concerning the geometric analysis, we have mainly consider in our previous works the case where the phase of the RF magnetic field is zero, and thus $u_2 = 0$. One objective of this article will be to fill the gap between the bi-input and single-input studies. From the numerical point of view, the indirect method using the HamPath software will be complemented with the Bocop toolbox [5] based on the direct approach.

A feature of the contrast problem is the existence of many locally optimal solutions which can be computed by the previously mentioned direct or indirect methods. An important question is then to assert global optimality. Hence another objective of this article is to use a moment/linear matrix inequality (LMI) technique [22,27] to compute such an estimate using the GloptiPoly toolbox [22].

This article is organized in four sections. The first section recalls and completes the geometric framework. The second section presents in details the three numerical methods. The numerical results are described and compared in the two final sections.

1 Necessary optimality conditions, geometric framework and results

The aim of this section is to recall the theoretical foundations. We use [8] as a reference in geometric control, whereas the application to the contrast problem is excerpted from [10].

1.1 Maximum principle

Proposition 1 *If u^* with corresponding trajectory q^* on $[0, t_f]$ is optimal then the following necessary optimality conditions are satisfied. Define the pseudo-Hamiltonian $H(q, p, u) = \langle p, F(q, u) \rangle$, p being the adjoint vector, there exists $p^*(\cdot)$ such that for almost every $t \in [0, t_f]$, we have*

$$(i) \quad \dot{q}^* = \frac{\partial H}{\partial p}(q^*, p^*, u^*), \quad \dot{p}^* = -\frac{\partial H}{\partial q}(q^*, p^*, u^*)$$

$$(ii) \quad H(q^*, p^*, u^*) = \max_{v \in U} H(q^*, p^*, v) \quad (\text{maximization condition})$$

and the following boundary conditions

$$(iii) \quad f(q^*(t_f)) = 0$$

$$(iv) \quad p^*(t_f) = p^0 \frac{\partial c}{\partial q}(q^*(t_f)) + \sum_{i=1}^k \sigma_i \frac{\partial f_i}{\partial q}(q^*(t_f)) \quad (\text{transversality condition}),$$

$$\sigma = (\sigma_1, \dots, \sigma_k) \in \mathbb{R}^k, \quad p^0 \leq 0$$

Definition 2 The solutions of conditions (i) and (ii) of Prop. 1 are called *extremals* and *BC-extremals* if they satisfy the boundary conditions. Note that $M(q^*, p^*) = \max_{v \in U} H(q^*, p^*, v)$ is constant and if $M(q^*, p^*) = 0$, an extremal is called *exceptional*.

1.2 Application to the contrast problem

1.2.1 State space

Since the Bloch ball is invariant for the dynamics of each spin particle, the state constraints are not active and the maximum principle can be applied.

1.2.2 Boundary conditions

In the contrast problem, $q = (q_1, q_2)$, $f = 0$ is the set $q_1 = 0$, and the cost to minimize is $c(q(t_f)) = -|q_2(t_f)|^2$. Hence, splitting the adjoint vector into $p = (p_1, p_2)$, we deduce from the transversality condition that $p_2(t_f) = -2p^0 q_2(t_f)$, $p^0 \leq 0$. If p^0 is nonzero, it can be normalized to $p^0 = -1/2$.

1.3 Parameterization of the extremal curves

1.3.1 Bi-input case

The system is written as $\dot{q} = F_0(q) + u_1 F_1(q) + u_2 F_2(q)$, $|u| \leq 1$. The maximization condition in Prop. 1 leads then to the following parameterization of the extremal controls:

$$u_1 = \frac{H_1}{\sqrt{H_1^2 + H_2^2}}, \quad u_2 = \frac{H_2}{\sqrt{H_1^2 + H_2^2}}, \quad (3)$$

where $H_i = \langle p, F_i(q) \rangle$ are Hamiltonian lifts. Define the *switching surface*:

$$\Sigma : H_1 = H_2 = 0.$$

Plugging such a u into the pseudo-Hamiltonian gives the *true Hamiltonian* $H_n = H_0 + \sqrt{H_1^2 + H_2^2}$. Outside Σ , the smooth solutions of the corresponding vector field \vec{H}_n are called *extremals of order zero*. Let (q, p, u) be a normal order zero extremal, using polar coordinates $u_1 = \cos \alpha$, $u_2 = \sin \alpha$. If $\alpha \equiv \text{constant}$ then the extremal has a *stationary phase control*. In the other case we say a non-stationary phase control.

1.3.2 Single-input case

Consider the case where $u_2 = 0$ and the system is written $\dot{q} = F_0(q) + u_1 F_1(q)$, where q belongs to a 4-dimensional space \mathbf{Q} and $|u_1| \leq 1$. The application of the maximization condition yields are two types of extremals:

- *Regular extremals*: The control is given by $u_1(t) = \text{sgn}(H_1(z(t)))$, where $z = (q, p)$ and $t \in [0, t_f]$. If the number of switchings is finite, it is called *bang-bang*.
- *Singular extremals*: The singular case is the situation where $H_1(z(t)) = 0$. The singular control can be computed as follows. If F, G are two vector fields, the *Lie bracket* is:

$$[F, G](q) = \frac{\partial F}{\partial q}(q)G(q) - \frac{\partial G}{\partial q}(q)F(q).$$

If \vec{H}_F, \vec{H}_G are two Hamiltonian vector fields the *Poisson bracket* is:

$$\{H_F, H_G\}(z) = \text{d}H_F(\vec{H}_G)(z).$$

If $H_F = \langle p, F(q) \rangle$, $H_G = \langle p, G(q) \rangle$ then we have: $\{H_F, H_G\}(z) = \langle p, [F, G](q) \rangle$. Applied to the contrast problem and differentiating twice $H_1(z(t)) = 0$ with respect to time leads to:

$$\{H_1, H_0\} = \{\{H_1, H_0\}, H_0\} + u_1 \{\{H_1, H_0\}, H_1\} = 0.$$

From the second condition, we derive when the denominator is not vanishing the corresponding singular control

$$u_{1,s} = -\frac{\{\{H_1, H_0\}, H_0\}}{\{\{H_1, H_0\}, H_1\}}. \quad (4)$$

We denote $\Sigma_1 : H_1 = 0$ and $\Sigma'_1 : H_1 = \{H_1, H_0\} = 0$. Plugging such $u_{1,s}$ into the pseudo-Hamiltonian defines the Hamiltonian vector field \vec{H}_s . Singular extremals such that $\{\{H_1, H_0\}, H_1\} \neq 0$ are called of *order two* and they are the solutions of \vec{H}_s starting at $t = 0$ from the surface Σ'_1 and satisfying $|u_{1,s}| \leq 1$.

Optimal solutions of the contrast problem are concatenations of bang and singular extremals. For the following sections, we introduce some notations. We note by BS the sequence composed by one bang arc (δ_+ or δ_-) followed by one singular arc (δ_s), both non empty, and $n\text{BS}$, $n > 1$, the concatenation of n BS-sequences, all non empty. The complexity of a sequence is measured by the number of concatenated arcs. By noticing that in our cases one has $\Gamma_i, \gamma_i \ll 1$, $i = 1, 2$, this leads to the following lemma:

Lemma 1 *The simplest BC-extremal in the contrast problem is of the form $\delta_+ \delta_s$, and so has a BS structure.*

1.4 Generalized Legendre–Clebsch condition

In the singular case the higher-order maximum principle [23] is used to complement Prop. 1 and we have:

Proposition 2 *In the singular case, the generalized Legendre–Clebsch condition*

$$\frac{\partial}{\partial u_1} \frac{d^2}{dt^2} \frac{\partial H}{\partial u_1} = \{H_1, \{H_1, H_0\}\} \leq 0 \quad (5)$$

is a necessary condition for optimality in the Mayer problem.

1.5 Saturation problem

The saturation problem consists in bringing the first spin to zero and is analyzed in details in [10, 25]. We recall briefly the results, denoting (y_1, z_1) the coordinates of the first spin. The singular trajectories are the two lines the z_1 -axis of revolution $y_1 = 0$ and the horizontal line $z_1 = \gamma_1/2(\gamma_1 - \Gamma_1)$. Along this horizontal direction, the flow is $\dot{y}_1 = -\Gamma_1 y_1 - \frac{\gamma_1^2(2\Gamma_1 - \gamma_1)}{4(\gamma_1 - \Gamma_1)^2 y_1}$. Consider the physical situation where $2\Gamma_1 > 3\gamma_1$ and the horizontal line is such that $0 > z_1 > -1$. The optimal policy to steer the north pole to zero is of the form $\delta_+ \delta_s^h \delta_+ \delta_s^v$, starting from an arc δ_+ (where $u = +1$) whereas the second arc δ_+ connects the horizontal arc δ_s^h to δ_s^v . The corresponding minimal time is denoted T_{\min} , and in the contrast by saturation one must have $t_f \geq T_{\min}$. An estimate of T_{\min} can be obtained as follows. Assuming ω_{\max} unbounded, the time to steer $y_1 = -1$ to $y_1 = 0$ along the singular horizontal line is according to the dynamics

$$\tau_1 = \int_0^1 \frac{dy_1}{\Gamma_1 y_1 + \frac{\gamma_1^2(2\Gamma_1 - \gamma_1)}{4(\gamma_1 - \Gamma_1)^2 y_1}},$$

which can be easily computed. If τ_2 is the time to steer $(0, z_1)$ to $(0, 0)$ along the vertical singular line, then $T_{\min} \simeq \tau_1 + \tau_2$.

In the limit case $t_f = T_{\min}$ in the contrast problem by saturation, the optimal policy is a 2BS structure. We have the following proposition.

Proposition 3 *The saturation solution of the first spin system can be embedded as an extremal solution of the contrast problem by saturation with $p^0 = 0$ in the transversality condition of Prop. 1.*

1.6 A geometric property

The following property is crucial:

Property 1 Consider the rotation of angle θ with respect to the z_i -axis written as $\exp(\theta R)$ and defined by

$$X_i = x_i \cos \theta + y_i \sin \theta, \quad Y_i = -x_i \sin \theta + y_i \cos \theta, \quad Z_i = z_i \quad (6)$$

where $i = 1, 2$. Then, the system is invariant up to the rotation of the control

$$v_1 = u_1 \cos \theta + u_2 \sin \theta, \quad v_2 = -u_1 \sin \theta + u_2 \cos \theta. \quad (7)$$

Clearly, the boundary conditions in the contrast problem are invariant for the rotation, and we have the following proposition (the first assertion being due to Noether theorem in Hamiltonian form)

Proposition 4 *We have:*

- i) *The Hamiltonian lift $H_R(z) = \langle p, Rq \rangle$ is a first integral along the optimal solution.*
- ii) *Starting from the point $N = ((0, 0, 1), (0, 0, 1))$, there is a one-parameter family of optimal solutions, each deduced by the θ -rotation (6), (7) respectively on the state and on the control.*

1.7 Classification of the extremal curves

The geometric control methods are efficient to stratify the set of extremals, and they are complemented by the geometric analysis of the extremal curves. This is explained next based on preliminary works [7, 16] for the first point and [9] for the second point.

1.7.1 The framework

The system is written as

$$\dot{q} = F_0(q) + u_1 F_1(q) + u_2 F_2(q)$$

and an extremal control of order zero is given by:

$$u = \frac{(H_1, H_2)}{\sqrt{H_1^2 + H_2^2}}.$$

This can be directly plugged into the Hamiltonian lift $H_0 + u_1 H_1 + u_2 H_2$ and leads to the Hamiltonian:

$$H_n = H_0 + \sqrt{H_1^2 + H_2^2},$$

whose smooth solutions are the extremals of order zero. The associated differential equation can be *regularized* using the reparameterization

$$ds = \frac{dt}{\sqrt{H_1^2 + H_2^2}}.$$

This leads to analyze a dynamical system with non isolated singularities located in the surface $\Sigma : H_1 = H_2 = 0$. This approach allows to investigate globally the extremal flow of order zero and the construction of non smooth solutions formed by connecting extremals of order zero at point of Σ , provided the Weierstrass-Erdmann conditions are satisfied:

$$p(t_+) = p(t_-), \quad H_n(t_+) = H_n(t_-),$$

where t is the time of contact with the switching surface. See [9] for the related analysis in the single-input case.

1.7.2 Spherical coordinates

Introducing for each spin system the spherical coordinates:

$$x_i = \rho_i \sin \varphi_i \cos \theta_i, \quad y_i = \rho_i \sin \varphi_i \sin \theta_i, \quad z_i = \rho_i \cos \varphi_i,$$

the system takes the form

$$\begin{aligned} \frac{d\rho_i}{dt} &= \gamma_i \cos \varphi_i - \rho_i (\delta_i \cos^2 \varphi_i + \Gamma_i) \\ \frac{d\varphi_i}{dt} &= \frac{-\gamma_i \sin \varphi_i}{\rho_i} + \delta_i \sin \varphi_i \cos \varphi_i + (-u_1 \sin \theta_i + u_2 \cos \theta_i) \\ \frac{d\theta_i}{dt} &= -\cot \varphi_i (u_1 \cos \theta_i + u_2 \sin \theta_i), \end{aligned}$$

where $\delta_i = \gamma_i - \Gamma_i$, $i = 1, 2$. Setting $\theta'_1 = \theta_1$, $\theta'_2 = \theta_1 - \theta_2$, one gets:

$$\begin{aligned} \frac{d\rho_1}{dt} &= \gamma_1 \cos \varphi_1 - \rho_1 (\delta_1 \cos^2 \varphi_1 + \Gamma_1) \\ \frac{d\varphi_1}{dt} &= \frac{-\gamma_1 \sin \varphi_1}{\rho_1} + \delta_1 \sin \varphi_1 \cos \varphi_1 + (-u_1 \sin \theta'_1 + u_2 \cos \theta'_2) \\ \frac{d\theta'_1}{dt} &= -\cot \varphi_1 (u_1 \cos \theta'_1 + u_2 \sin \theta'_1) \\ \frac{d\rho_2}{dt} &= \gamma_2 \cos \varphi_2 - \rho_2 (\delta_2 \cos^2 \varphi_2 + \Gamma_2) \\ \frac{d\varphi_2}{dt} &= \frac{-\gamma_2 \sin \varphi_2}{\rho_2} + \delta_2 \sin \varphi_2 \cos \varphi_2 - u_1 \sin(\theta'_1 - \theta'_2) + u_2 \cos(\theta'_1 - \theta'_2) \\ \frac{d\theta'_2}{dt} &= -\cot \varphi_1 (u_1 \cos \theta'_1 + u_2 \sin \theta'_1) + \cot \varphi_2 (u_1 \cos(\theta'_1 - \theta'_2) + u_2 \sin(\theta'_1 - \theta'_2)). \end{aligned}$$

Setting $v_1 = u_1 \cos \theta'_1 + u_2 \sin \theta'_1$, $v_2 = -u_1 \sin \theta'_1 + u_2 \cos \theta'_1$ the system takes the form

$$\begin{aligned}\frac{d\rho_1}{dt} &= \gamma_1 \cos \varphi_1 - \rho_1 (\delta_1 \cos^2 \varphi_1 + \Gamma_1) \\ \frac{d\varphi_1}{dt} &= \frac{-\gamma_1 \sin \varphi_1}{\rho_1} + \delta_1 \sin \varphi_1 \cos \varphi_1 + v_2 \\ \frac{d\theta'_1}{dt} &= -\cot \varphi_1 v_1 \\ \frac{d\rho_2}{dt} &= \gamma_2 \cos \varphi_2 - \rho_2 (\delta_2 \cos^2 \varphi_2 + \Gamma_2) \\ \frac{d\varphi_2}{dt} &= \frac{-\gamma_2 \sin \varphi_2}{\rho_2} + \delta_2 \sin \varphi_2 \cos \varphi_2 + v_1 \sin \theta'_2 + v_2 \cos \theta'_2 \\ \frac{d\theta'_2}{dt} &= -\cot \varphi_1 v_1 + \cot \varphi_2 (v_1 \cos \theta'_2 - v_2 \sin \theta'_2).\end{aligned}$$

Observe that the Hamiltonian H_n is invariant for a θ -rotation on the set of controls. A diffeomorphism on the state $Q = f(q)$ induces a Mathieu symplectic transformation: $Q = f(q)$, $p = \frac{\partial f}{\partial q}(q)P$. In particular, the transformation: $\theta'_1 = \theta_1$, $\theta'_2 = \theta_1 - \theta_2$ induces on the adjoint variable the transformation: $p_{\theta_1} = p_{\theta'_1} + p_{\theta'_2}$, $p_{\theta_2} = -p_{\theta'_2}$. In the spherical coordinates the Hamiltonian H_n is computed with:

$$\begin{aligned}H_1^2 + H_2^2 &= p_{\varphi_1}^2 + p_{\varphi_2}^2 + 2(p_{\varphi_1} p_{\varphi_2} + p_{\theta_1} p_{\theta_2} \cot \varphi_1 \cot \varphi_2) \cos(\theta_1 - \theta_2) + \\ &\quad p_{\theta_1}^2 \cot^2 \varphi_1 + p_{\theta_2}^2 \cot^2 \varphi_2 + 2(p_{\varphi_1} p_{\theta_2} \cot \varphi_2 - p_{\varphi_2} p_{\theta_1} \cot \varphi_1) \sin(\theta_1 - \theta_2).\end{aligned}$$

One deduces the following:

Proposition 5 θ'_1 is a cyclic variable and $p_{\theta'_1} = p_{\theta_1} + p_{\theta_2}$ is a first integral.

Computed explicitly, this gives:

$$p_{\theta_1} + p_{\theta_2} = (-p_{x_1} y_1 + p_{y_1} x_1) + (-p_{x_2} y_2 + p_{y_2} x_2) = -\langle p, Rq \rangle,$$

where R is the matrix introduced in section 1.6. Using Lie brackets, this has the following important interpretation:

$$\langle p, Rq \rangle = \langle p, [F_1, F_2](q) \rangle = \{H_1, H_2\}(q, p).$$

1.7.3 Lie bracket computations

To compute Lie brackets, one observes that the system can be lifted onto the Lie product $G \times G$, where G is the semidirect Lie product $GL(3, \mathbb{R}) \times_s \mathbb{R}^3$ acting on the q -space using the action $(A, a) = Aq + a$. The Lie bracket computation rule is $((A, a), (B, b)) = ([A, B], Ab - Ba)$. One uses the notation $F_0 = (A_0, a_0)$ with $A_0 = \text{diag}(-\Gamma_1, -\Gamma_1, -\gamma_1, -\Gamma_2, -\Gamma_2, -\gamma_2)$ and $a_0 = (0, 0, \gamma_1, 0, 0, \gamma_2)$, whereas the control fields F_1, F_2 are identified to $B_1 = \text{diag}(C_1, C_1)$ and $B_2 = \text{diag}(C_2, C_2)$, where C_1 and C_2 are the antisymmetric matrices $C_1 = E_{32} - E_{23}$, $C_2 = E_{13} - E_{31}$ with $E_{ij} = (\delta_{ij})$ (Kronecker symbol). Note that C_1 and C_2 generates the Lie algebra $so(3)$ since $[C_1, C_2] = C_3 = E_{21} - E_{12}$.

According to the Lie bracket computation rule on the semidirect Lie product, we can reduce the computations to matrix Lie brackets. We have the following results, see [9] for the details. Consider first the case of a single spin and let $A = \text{diag}(-\Gamma, -\Gamma, -\gamma)$ and denote $\delta = \gamma - \Gamma$. We have:

Lemma 2 *There are two cases*

- i) *If $\delta \neq 0$, the Lie algebra generated by $\{A, C_1, C_2\}$ is $gl(3, \mathbb{R})$.*
- ii) *If $\delta = 0$, the Lie algebra generated by $\{A, C_1, C_2\}$ is $\mathbb{R}A \oplus so(3)$.*

The computations for the coupled system give the following result.

Lemma 3 *Denoting $\delta_i = \gamma_i - \Gamma_i$, we have:*

- i) *The Lie algebra generated by $\{B_1, B_2\}$ is a Lie algebra isomorphic to $so(3)$.*
- ii) *Assume $|\delta_1|$ and $|\delta_2|$ are nonzero and distinct. Then the Lie algebra generated by $\{A_0, B_1, B_2\}$ is $\mathbb{R}A_0 \oplus sl(3, \mathbb{R}) \oplus sl(3, \mathbb{R})$.*

Next, we present in details the Lie brackets needed in our computations. Each entry is formed by a couple of 3 dimensional vectors and we use the notation omitting the indices.

– *Length 1:*

$$\begin{aligned} F_0 &= (-\Gamma x, -\Gamma y, \gamma(1-z)) \\ F_1 &= (0, -z, y) \\ F_2 &= (z, 0, -x) \end{aligned}$$

– *Length 2:*

$$\begin{aligned} [F_0, F_1] &= (0, \gamma - \delta z, -\delta y) \\ [F_0, F_2] &= (-\gamma + \delta z, 0, \delta x) \\ [F_1, F_2] &= (-y, x, 0) \end{aligned}$$

– *Length 3:*

$$\begin{aligned} [[F_1, F_2], F_0] &= 0 \\ [[F_1, F_2], F_1] &= F_2 \\ [[F_1, F_2], F_2] &= -F_1 \\ [[F_0, F_1], F_1] &= (0, -2\delta y, -\gamma + 2\delta z) \\ [[F_0, F_1], F_2] &= (\delta y, \delta x, 0) = [[F_0, F_2], F_1] \\ [[F_0, F_2], F_2] &= (-2\delta x, 0, 2\delta z - \gamma) \\ [[F_0, F_1], F_0] &= (0, -\gamma(\gamma - 2\Gamma) + \delta^2 z, -\delta^2 y) \\ [[F_0, F_2], F_0] &= (\gamma(\gamma - 2\Gamma) - \delta^2 z, 0, \delta^2 x) \end{aligned}$$

1.7.4 Stratification of the surface $\Sigma : H_1 = H_2 = 0$ and partial classification of the extremal flow near Σ

Preliminary results about this classification are coming from [7, 16]. We make a self contained presentation building on [7, 16] with additional results.

Let $z = (q, p)$ be a curve solution of $\dot{H}_0 + u_1 \dot{H}_1 + u_2 \dot{H}_2$. Differentiating H_1 and H_2 along such a solution, one gets:

$$\begin{aligned}\dot{H}_1 &= \{H_0, H_1\} - u_2 \{H_1, H_2\} \\ \dot{H}_2 &= \{H_0, H_2\} + u_1 \{H_1, H_2\}\end{aligned}\quad (8)$$

and extremals of order zero are such that the control (u_1, u_2) is defined by $u_i = \frac{H_i}{\sqrt{H_1^2 + H_2^2}}$, $i = 1, 2$.

Let $z_0 \in \Sigma_2 = \Sigma \setminus \{H_1, H_2\} = 0$ and define the control u_s by:

$$u_s(z) = \frac{(-\{H_0, H_2\}(z), \{H_0, H_1\}(z))}{\{H_1, H_2\}(z)}.\quad (9)$$

Plugging such u_s into H defines the true Hamiltonian

$$H_s(z) = H_0(z) + u_{s,1}(z)H_1(z) + u_{s,2}(z)H_2(z).$$

The behaviours of the extremals of order zero near Σ can be analyzed using a nilpotent model where all Lie brackets at $z_0 \in \Sigma_2$ of length ≥ 3 are zero. Denoting:

$$\{H_0, H_1\}(z_0) = a_1, \quad \{H_0, H_2\}(z_0) = a_2, \quad \{H_1, H_2\}(z_0) = b$$

and using polar coordinates

$$H_1 = r \cos \theta, \quad H_2 = r \sin \theta,$$

we deduce from (8):

$$\begin{aligned}\dot{r} &= a_1 \cos \theta + a_2 \sin \theta \\ \dot{\theta} &= \frac{1}{r}(b - a_1 \sin \theta + a_2 \cos \theta).\end{aligned}\quad (10)$$

To analyze this equation, we write:

$$a_1 \sin \theta - a_2 \cos \theta = A \sin(\theta + \varphi)$$

with $A \tan \varphi = -a_2/a_1$, $A = \sqrt{a_1^2 + a_2^2}$. Hence the equation $\dot{\theta} = 0$ leads to the relation

$$A \sin(\theta + \varphi) = b,$$

which has two distinct solutions on $[0, 2\pi[$ denoted θ_0, θ_1 if and only if $A > |b|$, one solution if $A = |b|$ and zero solution if $A < |b|$. Moreover $\theta_1 - \theta_0 = \pi$ if and only if $b = 0$. Plugging θ_0, θ_1 in (10), we have:

Lemma 4 *If $\sqrt{a_1^2 + a_2^2} > |b|$ and $b \neq 0$, we have a broken extremal formed by concatenating two extremals of order zero at each point z_0 of Σ_2 .*

At such a point z_0 of Σ_2 , the singular control given by (9) is such that $u_{s,1}^2 + u_{s,2}^2 = \frac{a_1^2 + a_2^2}{b^2} > 1$ and hence is not admissible.

This describes the behaviours of extremals of order zero near a generic point of z_0 . Next we analyze more degenerated situations. One needs the following concepts.

Goh condition. Higher order necessary optimality conditions along singular extremals are related to *finiteness* of the *index of the quadratic form* associated to the intrinsic second order derivative, see [8]. First we have:

$$\{H_1, H_2\} = 0 \text{ (Goh condition).} \quad (11)$$

Using $H_1 = H_2 = \{H_1, H_2\} = 0$ and (8), one gets the relations:

$$\{H_1, H_2\} = \{H_0, H_1\} = \{H_0, H_2\} = 0. \quad (12)$$

Then differentiating, we obtain:

$$\{\{H_1, H_2\}, H_0\} + u_1 \{\{H_1, H_2\}, H_1\} + u_2 \{\{H_1, H_2\}, H_2\} = 0 \quad (13)$$

$$\left. \begin{aligned} \{\{H_0, H_1\}, H_0\} + u_1 \{\{H_0, H_1\}, H_1\} + u_2 \{\{H_0, H_1\}, H_2\} &= 0 \\ \{\{H_0, H_2\}, H_0\} + u_1 \{\{H_0, H_2\}, H_1\} + u_2 \{\{H_0, H_2\}, H_2\} &= 0 \end{aligned} \right\} \quad (14)$$

This leads in general to *three* relations to compute *two* control components, see [17] for a discussion of the non genericity of such relations. However, according to Lie brackets computations, we have in our case:

Lemma 5 *If $H_1 = H_2 = 0$, one has*

$$\{\{H_1, H_2\}, H_0\} = \{\{H_1, H_2\}, H_1\} = \{\{H_1, H_2\}, H_2\} = 0$$

and (13) is satisfied.

To analyze (14), which can be written $\tilde{A} + \tilde{B}u = 0$, we use:

$$H_1 = H_2 = \{H_1, H_2\} = \{H_0, H_1\} = \{H_0, H_2\} = 0.$$

Hence p is orthogonal to $F_1, F_2, [F_1, F_2], [F_0, F_1], [F_0, F_2]$. Introducing:

$$A = \begin{pmatrix} A_1 \\ A_2 \end{pmatrix}, \quad B = \begin{pmatrix} B_1 & B_3 \\ B_2 & B_4 \end{pmatrix}, \quad C = (F_1, F_2, [F_1, F_2], [F_0, F_1], [F_0, F_2]),$$

with

$$A_1 = \det(C, [[F_0, F_1], F_0]), \quad A_2 = \det(C, [[F_0, F_2], F_0]),$$

and

$$\begin{aligned} B_1 &= \det(C, [[F_0, F_1], F_1]), & B_2 &= \det(C, [[F_0, F_2], F_1]), \\ B_3 &= \det(C, [[F_0, F_1], F_2]), & B_4 &= \det(C, [[F_0, F_2], F_2]), \end{aligned}$$

the relation (14) leads to:

$$A + Bu = 0,$$

and if $\det B \neq 0$, one gets the singular control given by the feedback:

$$u'_s = -B^{-1}A \quad (15)$$

and the associated vector field:

$$Q'_s = F_0 + u'_{s,1}F_1 + u'_{s,2}F_2.$$

Moreover, the singular control has to be admissible: $|u'_s| \leq 1$. One denotes:

$$\Sigma'_2 : H_1 = H_2 = \{H_1, H_2\} = \{H_0, H_1\} = \{H_0, H_2\} = 0 \setminus \det \tilde{B} = 0$$

and singular extremals solutions of $\vec{H}'_s = \vec{H}_0 + u'_{s,1}\vec{H}_1 + u'_{s,2}\vec{H}_2$ project onto solutions of Q'_s .

Computations of $\det B$. We give $\det B$ in the general case:

$$\det B = (x_1 y_2 - x_2 y_1)^4 (\delta_1 - \delta_2) (2\delta_1 z_1 - \gamma_1) (2\delta_2 z_2 - \gamma_2) \\ (2(\delta_1^2 \gamma_2 z_1 - \delta_2^2 \gamma_1 z_2) - \gamma_1 \gamma_2 (\delta_1 - \delta_2) - 2\delta_1 \delta_2 (\gamma_1 z_2 - \gamma_2 z_1)), \quad (16)$$

in the fluid case (P_1):

$$\det B = -(180625(x_1 y_2 - x_2 y_1)^4 (34z_1 + 3)^2) / 12573377307869184$$

and in the blood case (P_2):

$$\det B = -(244140625(x_1 y_2 - x_2 y_1)^4 (23z_2 + 2)(52z_1 + 1) \\ (13208z_1 - 2921z_2 + 162)) / 2900177174423310336.$$

Additional singular extremals can be contained in the surface:

$$\Sigma_2'' : H_1 = H_2 = \{H_1, H_2\} = \{H_0, H_1\} = \{H_0, H_2\} = \det \tilde{B} = 0.$$

In particular there are those associated to extremals such that $u_2 = 0$. Indeed, this corresponds to replace H_2 by εH_2 and to impose $\varepsilon = 0$. The remaining relations are then:

$$H_1 = \{H_0, H_1\} = 0$$

and from (14) one gets the relations:

$$\{\{H_0, H_1\}, H_0\} + u_1 \{\{H_0, H_1\}, H_1\} = 0. \quad (17)$$

Therefore this defines the singular control:

$$u_{1,s}'' = - \frac{\{\{H_0, H_1\}, H_0\}}{\{\{H_0, H_1\}, H_1\}} \quad (18)$$

and the associated Hamiltonian $H_{1,s}'' = H_0 + u_{1,s}'' H_1$, with $u_{1,s}'' = u_{1,s}$, where $u_{1,s}$ is defined section 1.3.2. In particular we have the following result:

Proposition 6 *The extremals of the single-input case are extremals of the bi-input case with the additional condition: $x_1 = p_{x_1} = x_2 = p_{x_2} = 0$.*

The classification of regular extremals near the switching surface in the single-input case is coming from [24], see also [8].

To resume our analysis, we have:

Theorem 1 *The singular extremals in the contrast problem are classified by the following stratification of vector fields:*

1. In $\Sigma_2 : H_1 = H_2 = 0 \setminus \{H_1, H_2\} = 0$, the singular control is given by (9):

$$u_s(z) = \frac{(-\{H_0, H_2\}(z), \{H_0, H_1\}(z))}{\{H_1, H_2\}(z)}.$$

2. In $\Sigma'_2 : H_1 = H_2 = \{H_1, H_2\} = \{H_0, H_1\} = \{H_0, H_2\} = 0 \setminus \det \tilde{B} = 0$, the singular control is given by the feedback (15):

$$u'_s = -B^{-1}A.$$

3. In $\Sigma''_2 : H_1 = H_2 = \{H_1, H_2\} = \{H_0, H_1\} = \{H_0, H_2\} = \det \tilde{B} = 0$, there exists singular controls such that $u_2 = 0$ and u_1 is given by (18):

$$u_{1,s} = u''_{1,s} = -\frac{\{\{H_0, H_1\}, H_0\}}{\{\{H_0, H_1\}, H_1\}}.$$

Remark 1 Observe that additional singular extremals can exist in Σ''_2 . The respective codimension are: two for Σ_2 , five for Σ'_2 and six for Σ''_2 .

2 The numerical methods

In this section we present the three numerical methods used for the resolution of the contrast problem.

2.1 Bocop

The so-called direct approach transforms the infinite dimensional optimal control problem (OCP) into a finite dimensional optimization problem (NLP). This is done by a discretization in time applied to the state and control variables, as well as the dynamics equation. These methods are usually less precise than indirect methods based on Pontryagin's Maximum Principle, but more robust with respect to the initialization. Also, they are more straightforward to apply, hence their wide use in industrial applications. We refer the reader to for instance [4] and [33] for more details on direct transcription methods and NLP algorithms.

Summary of the time discretization:

$$\begin{array}{ll} t \in [0, t_f] & \rightarrow \{t_0 = 0, \dots, t_N = t_f\} \\ z(\cdot), u(\cdot) & \rightarrow X = \{z_0, \dots, z_N, u_0, \dots, u_{N-1}, t_f\} \\ \hline \text{Criterion} & \rightarrow \min c(z_N) \\ \text{Dynamics} & \rightarrow (ex : Euler) z_{i+i} = z_i + hf(z_i, u_i) \\ \text{Admissible Controls} & \rightarrow u_i \in \mathbf{U} \\ \text{Boundary Conditions} & \rightarrow \Phi(z_0, z_N) = 0 \end{array}$$

We therefore obtain a nonlinear programming problem on the discretized state and control variables

$$(NLP) \begin{cases} \min F(X) = c(z_N) \\ LB \leq C(X) \leq UB \end{cases}$$

All tests were run using the Bocop software [5]. The discretized nonlinear optimization problem is solved by the well-known IPOPT solver [37] with MUMPS [2],

while the derivatives are computed by sparse automatic differentiation with ADOL-C [38] and COLPACK [19].

In the numerical experiments, we used a midpoint (implicit 2nd order) discretization with 1000 to 5000 time steps. Execution times on a Xeon 3.2GHz CPU were a few minutes. We recall that the costate (or adjoint state) for Pontryagin's Principle corresponds to the Lagrange multipliers for the dynamics constraints in the discretized problem.

2.2 HamPath in the single-input case

In this subsection, we recall the method used to solve the contrast problem in the **single-input case**, based on the HamPath code, see [11, 18]. The HamPath software is based upon indirect methods: simple and multiple shooting, differential continuation (or homotopy) methods and computation of the solutions of the variational equations, needed to check second order conditions of local optimality.

2.2.1 Multiple shooting method for the contrast problem in the single-input case

We introduce the λ variable such that $t_f = \lambda T_{\min}$. For a fixed $\lambda \geq 1$, we must solve the contrast problem by multiple shooting method since the optimal control is discontinuous (see 1.3.2). Shooting methods consist in finding a zero of a specific function and use Newton like algorithms. While simple shooting leads to solve a two points boundary value problem, multiple shooting takes into account intermediate conditions. This leads to the first numerical difficulty.

Difficulty 1 *Before calling the multiple shooting method, we need to know the structure of the optimal solution and we need a good approximation of the solution to make the method converge.*

Fix $t_f = \lambda T_{\min}$ with $\lambda > 1$, assume to simplify that the optimal solution $z(t) = (q(t), p(t))$, $t \in [0, t_f]$, is made of a single BS-sequence and denote t_1 , $0 < t_1 < t_f$, the switching time between the regular arc and the singular arc. The generalization to the case n BS is straightforward. By construction, $z(\cdot)$ is a concatenation of the integral curve of \vec{H} joining $z(0)$ to $z_1 = z(t_1)$ with $u_1(t) = \text{sgn}(H_1(z(t)))$, $t \in [0, t_1]$, and of the extremal (of order two) solution of \vec{H}_s starting at z_1 , where z_1 must satisfy (see subsection 1.3.2):

$$H_1(z_1) = \{H_1, H_0\}(z_1) = \{\{H_1, H_0\}, H_0\}(z_1) + u_1 \{\{H_1, H_0\}, H_1\}(z_1) = 0, \quad (19)$$

and then $z_1 \in \Sigma'_1$.

Remark 2 We use the same notation z_1 for the third component of the first spin state $q_1 = (x_1, y_1, z_1)$ and for the first switching point between bang and singular arcs. In the first case, z_1 is scalar and in the second case, $z_1 = z(t_1) = (q(t_1), p(t_1))$ lives in the cotangent space $T^*\mathbf{Q}$, thus no confusion is possible.

Let fix the notations for both bang and singular extremals. We write $z(\cdot, t_0, z_0)$ or $z(\cdot, t_0, q_0, p_0)$ the solution of $\dot{z}(\cdot) = \vec{H}(z(\cdot))$, $z(t_0) = z_0 = (q_0, p_0)$, with $q_0 = (q_{1,0}, q_{2,0})$, $p_0 = (p_{1,0}, p_{2,0})$ and $t_0 = 0$. Under these notations each intial spin state is $q_{i,0} = (y_{i,0}, z_{i,0}) = (0, 1)$, $i = 1, 2$, and the adjoint vector is given by $p_{i,0} = (p_{y_{i,0}}, p_{z_{i,0}})$. The singular extremal is denoted $z_s(\cdot, t_1, z_1)$ solution of $\dot{z}_s(\cdot) = \vec{H}_s(z_s(\cdot))$, $z_s(t_1) = z_1$, where $z_s = (q_s, p_s)$ with $q_s = (q_{1,s}, q_{2,s})$ and $p_s = (p_{1,s}, p_{2,s})$. Under these notations the boundary conditions from subsection 1.2.2 become:

$$\begin{aligned} q_{1,s}(t_f, t_1, z_1) &= (0, 0) \\ q_{2,s}(t_f, t_1, z_1) &= p_{2,s}(t_f, t_1, z_1). \end{aligned} \quad (20)$$

Hence, the bang and singular arcs $z(\cdot, t_0, z_0)$, $z_0 = (q_0, p_0)$ and $z_s(\cdot, t_1, z_1)$ are entirely defined by $(t_0, z_0, t_1, z_1, t_f)$.

Remark 3 In the contrast problem, t_0 , $t_f = \lambda T_{\min}$ and q_0 are fixed and known. For z_1 , we can either consider it as a dependant variable if we replace z_1 by the value $z(t_1, t_0, z_0)$, or as an independant variable and add the matching conditions:

$$z(t_1, t_0, z_0) = z_1, \quad (21)$$

expressing the continuity of the extremal at the switching time.

We define now *the multiple shooting function* $\bar{S}_\lambda(p_0, t_1, z_1)$ which maps (p_0, t_1, z_1) to the conditions (19), (20) and (21). See [14] for details about multiple shooting methods with application in optimal control and [31] for applications in the Bang-Singular-Bang case. The function \bar{S}_λ is given by:

$$\bar{S}_\lambda : \mathbb{R}^{3n+1} \rightarrow \mathbb{R}^{3n+2}$$

$$\begin{pmatrix} p_0 \\ t_1 \\ z_1 \end{pmatrix} \mapsto \bar{S}_\lambda(p_0, t_1, z_1) = \begin{pmatrix} H_1(z_1) \\ \{H_1, H_0\}(z_1) \\ q_{1,s}(t_f, t_1, z_1) \\ q_{2,s}(t_f, t_1, z_1) - p_{2,s}(t_f, t_1, z_1) \\ z(t_1, t_0, z_0) - z_1 \end{pmatrix}, \quad (22)$$

Remark 4 The shooting system (22) has an extra condition which is redundant and can be eliminated. See [3] for the general case where the shooting system has more equations than unknowns and where the Gauss-Newton method is used to compute a zero of the shooting function.

Lemma 6 *In the shooting system (22), the transversality condition:*

$$q_{2,s}(t_f, t_1, z_1) - p_{2,s}(t_f, t_1, z_1) = 0_{\mathbb{R}^2}$$

reduces to

$$\langle p_{2,s}(t_f, t_1, z_1), q_{2,s}(t_f, t_1, z_1) \rangle - |q_{2,s}(t_f, t_1, z_1)|^2 = 0 \quad (23)$$

and the system is square.

Proof Denote the singular extremal $z_s = (q_s, p_s)$, with $q_s = (q_{1,s}, q_{2,s})$, $p_s = (p_{1,s}, p_{2,s})$ and $q_{i,s} = (y_{i,s}, z_{i,s})$, $p_{i,s} = (p_{y_{i,s}}, p_{z_{i,s}})$, $i = 1, 2$. The condition $H_1(z_1) = 0$ implies that

$$H_1(z_s[t_f]) = 0$$

where $[t_f]$ stands for (t_f, t_1, z_1) , since $z_s(\cdot)$ is contained in Σ'_1 . Besides, the terminal condition $q_{1,s}[t_f] = 0_{\mathbb{R}^2}$ implies that

$$H_1(z_s[t_f]) = -p_{y_{2,s}}[t_f]z_{2,s}[t_f] + p_{z_{2,s}}[t_f]y_{2,s}[t_f] = \det(q_{2,s}[t_f], p_{2,s}[t_f]),$$

i.e. $q_{2,s}$ and $p_{2,s}$ are colinear at t_f . Hence we have:

$$\left\{ \begin{array}{l} H_1(z_1) = 0 \\ q_{1,s}[t_f] = 0_{\mathbb{R}^2} \\ q_{2,s}[t_f] - p_{2,s}[t_f] = 0_{\mathbb{R}^2} \end{array} \right\} \Leftrightarrow \left\{ \begin{array}{l} H_1(z_1) = 0 \\ q_{1,s}[t_f] = 0_{\mathbb{R}^2} \\ \langle p_{2,s}[t_f], q_{2,s}[t_f] \rangle - |q_{2,s}[t_f]|^2 = 0 \end{array} \right. \quad \square$$

The square system replaces the system (22) and we define *the multiple shooting function* S_λ by:

$$S_\lambda : \mathbb{R}^{3n+1} \rightarrow \mathbb{R}^{3n+1}$$

$$\begin{pmatrix} p_0 \\ t_1 \\ z_1 \end{pmatrix} \mapsto S_\lambda(p_0, t_1, z_1) = \begin{pmatrix} H_1(z_1) \\ \{H_1, H_0\}(z_1) \\ q_{1,s}[t_f] \\ \langle p_{2,s}[t_f], q_{2,s}[t_f] \rangle - |q_{2,s}[t_f]|^2 \\ z(t_1, t_0, z_0) - z_1 \end{pmatrix}. \quad (24)$$

The multiple shooting method for the contrast problem consists in finding a zero of the multiple shooting function S_λ , i.e. in solving $S_\lambda(p_0, t_1, z_1) = 0$.

Algorithmic of the HamPath code The fortran hybrid Newton method `hybrj` (from the `minpack` library [32]) is used to solve the nonlinear system $S_\lambda(p_0, t_1, z_1) = 0$. The `hybrj` code implements the Powell hybrid algorithm [35] based upon Newton-Raphson method combined with Levenberg-Marquardt algorithm. The Jacobian of S_λ must be provided to `hybrj` and must be invertible to get convergence. In [3], the authors analyze the convergence of the shooting algorithm and the invertibility of the shooting function for optimal control problems with singular arcs. Define the function

$$E(t_0, t_1, t_f, z_0, z_1, ez_0, ez_1) : \mathbb{R}^{3+4 \times 2n} \rightarrow \mathbb{R}^{3n+1}$$

by

$$S_\lambda(p_0, t_1, z_1) = E(t_0, t_1, t_f, (q_0, p_0), z_1, z(t_1, t_0, z_0), z_s(t_f, t_1, z_1)),$$

where $z_0 = (q_0, p_0)$, $ez_0 = z(t_1, t_0, z_0)$ and $ez_1 = z_s(t_f, t_1, z_1)$.

Remark 5 The user must only provide the function E (S_λ is not needed) and the two ordered true-Hamiltonians H and H_s (the regular and singular controls must be computed), i.e. H for the first arc and H_s for the second arc. Then, the code assembles automatically the multiple shooting function and its Jacobian which are given to `hybrj`.

We detail how $S'_\lambda(p_0, t_1, z_1)$ is computed. The Jacobian is given by:

$$\begin{aligned} \frac{\partial S_\lambda}{\partial p_0} &= \left(\frac{\partial E}{\partial z_0} + \frac{\partial E}{\partial e z_0} \cdot \frac{\partial z}{\partial z_0}(t_1, t_0, z_0) \right) \begin{bmatrix} 0 \\ I_n \end{bmatrix} \\ \frac{\partial S_\lambda}{\partial t_1} &= \frac{\partial E}{\partial t_1} + \frac{\partial E}{\partial e z_0} \cdot \frac{\partial z}{\partial t_f}(t_1, t_0, z_0) + \frac{\partial E}{\partial e z_1} \cdot \frac{\partial z_s}{\partial t_0}(t_f, t_1, z_1) \\ \frac{\partial S_\lambda}{\partial z_1} &= \frac{\partial E}{\partial z_1} + \frac{\partial E}{\partial e z_1} \cdot \frac{\partial z_s}{\partial z_0}(t_f, t_1, z_1), \end{aligned} \quad (25)$$

where $\frac{\partial}{\partial t_0}$, $\frac{\partial}{\partial t_f}$ and $\frac{\partial}{\partial z_0}$ mean respectively the partial derivative with respect to the initial time, the final time and the initial condition. All the partial derivatives of E are computed by Automatic Differentiation (AD) with the `tape` software [20]. The derivative $\partial_{z_0} z(t_1, t_0, z_0)$ is the solution at t_1 of the variational equation:

$$\delta \dot{z}(t) = d\vec{H}(z(t))\delta z(t), \quad \delta z(t_0) = I_{2n}, \quad z(t_0) = z_0,$$

whereas $\partial_{z_0 z_s}(t_f, t_1, z_1)$ is the solution at t_f of the variational equation:

$$\delta \dot{z}(t) = d\vec{H}_s(z_s(t))\delta z(t), \quad \delta z(t_1) = I_{2n}, \quad z_s(t_1) = z_1.$$

Then $\partial_{t_f} z(t_1, t_0, z_0)$ is simply equal to $\vec{H}(z(t_1, t_0, z_0))$ while $\partial_{t_0 z_s}(t_f, t_1, z_1)$ is the solution at t_f of:

$$\delta \dot{z}(t) = d\vec{H}_s(z_s(t))\delta z(t), \quad \delta z(t_1) = -\vec{H}_s(z_1), \quad z_s(t_1) = z_1.$$

HamPath uses again AD to compute \vec{H} , $d\vec{H}$ and $d\vec{H}_s$.

2.2.2 Homotopy method on the final time

Continuation techniques or homotopic methods are well known and widely used: see for example [1] for theoretical and numerical details. We just point out some facets encountered in optimal control, especially for the contrast problem.

In the contrast problem, natural parameters are the relaxation times and the final time t_f . In this article, our goal is to give the optimal policy with respect to t_f . Thus we define the homotopic function $h: \mathbb{R}^N \times \mathbb{R} \rightarrow \mathbb{R}$ by $h(x, \lambda) = S_\lambda(x)$, $\lambda \geq 1$, where S_λ is the multiple shooting function (24) and $x = (p_0, t_1, z_1)$ in the BS case.

The classical difficulties about homotopic methods consist in assuring that a curve in $h^{-1}(0)$ exists, is sufficiently smooth and will intersect a fixed target homotopic level in a finite length. Suppose h is continuously differentiable and that we know x_0 such that $h(x_0, \lambda_0) = 0$ and

$$\text{rank} \left(\frac{\partial h}{\partial x}(x_0, \lambda_0) \right) = N.$$

Suppose also that 0 is a regular value of h . Then a continuously differentiable curve starting from (x_0, λ_0) exists and is either diffeomorphic to a circle or the real line. The curves in $h^{-1}(0)$ are disjoint, and we call each branch of $h^{-1}(0)$ a path of zeros.

Remark 6 For a 2BS structure, we must introduce two others arcs and the variable x is $x = (p_0, t_1, z_1, t_2, t_2, z_3)$. Hence, in the BS and 2BS cases, the paths of zeros we compare are not defined in the same spaces.

Besides, it is possible that a 2BS solution is continuously deformed in a way that a BS or a 3BS structure appeared. The continuation process would stop at the change of structure. A BS-sequence must be removed if a bang arc tends to disappear, or added if a singular arc tends to saturate the constraint $|u| = 1$. Finally, the following difficulty is crucial.

Difficulty 2 *An important issue in the contrast problem is to deal with the many local solutions.*

For a given value $\bar{\lambda}$, we must compare the cost associated to each component of $h^{-1}(0) \cap \{\lambda = \bar{\lambda}\}$. This global aspect is responsible for a possible loss of regularity on the value function $\lambda \mapsto c(q(t_f))$, $t_f = \lambda T_{\min}$ and on the optimal path of zeros.

Algorithmic of the *HamPath* code Unlike well-known prediction-correction methods, see [1], we merely follow the path of zeros by integrating the differential system with a high order Runge-Kutta scheme, without any correction. The Jacobian of the homotopic function is computed using variational equations as in subsection 2.2.1. See [11, 15] for details about the algorithmic.

2.3 lmi

The direct and indirect methods provide local optimal solutions. By comparing the different paths of zeros, one obtains a strong candidate solution whose global optimality must be asserted. This can be done by the moment/lmi techniques described below.

The moment approach is a global optimization technique that transforms a non-linear, possibly infinite-dimensional optimization problem into convex and finite-dimensional relaxations in the form of Linear Matrix Inequalities (lmi). We follow [28] for the specific case of optimal control with bounded controls and [27] for the main steps of the method.

An overview of the method is given in Fig. 1. The first step consists in linearizing the problem by casting it as a Linear Program (LP) on a measure space, a problem often referred to as a *generalized moment problem*. This can be performed by the use of so-called *occupation measures*, encoding admissible trajectories. The second step is to exploit the problem's structure, here given by its polynomial data, to manipulate the measures by their *moment sequences*. This leads to a Semi-Definite Program (SDP) with countably many decision variables, one for each moment. The third and last step is to truncate this last problem to a finite set of those moments, leading to a relaxation in the form of Linear Matrix Inequalities (lmi). Those relaxations can be solved by off-the-shelf software.

In the sequel, we show $J \geq J_{\text{LP}} \geq J_{\text{SDP}} \geq J_{\text{LMI}}^r$, which is the relation of interest if the method is used to yield upper bounds on the contrast. We also point to

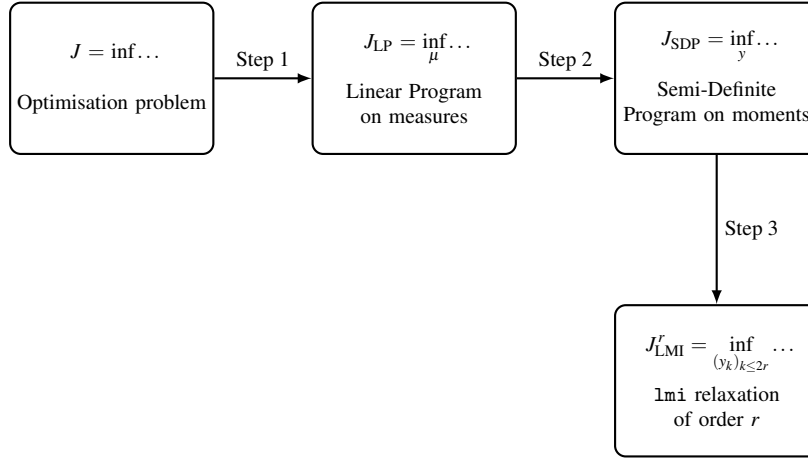


Fig. 1 Overview of the moment approach. Step 1: the initial optimization problem is cast as a Linear Program on a measure space. Step 2: the latter is itself recast as a Semi-Definite Program on moment sequences. Step 3: truncating the sequences to moments of degree smaller than $2r$ leads to the Linear Matrix Inequality relaxation of order r .

relevant theorems in the literature showing that for the problem at hand, the cost of the lmi relaxations asymptotically converge to that of the original problem, i.e. $\lim_{r \rightarrow \infty} J_{\text{LMI}}^r \rightarrow J$.

2.3.1 Step 1: formulation as a measure LP

The first step is to embed problem (OCP) into a linear program on measures by the use of occupation measures. We first set up the notations. For $z \in \mathbf{Z} \subset \mathbb{R}^n$, $\mathbb{R}[z]$ denotes the ring of polynomials in the variables z . $\mathcal{M}^+(\mathbf{Z})$ is the set of finite, positive Borel measures supported on compact set \mathbf{Z} and $\int_{\mathbf{Z}} v(z) d\mu(z)$ denotes the integration of a continuous function $v \in C(\mathbf{Z})$ with respect to $\mu \in \mathcal{M}^+(\mathbf{Z})$. We also write simply $\int v d\mu$ should no ambiguity arise.

For concise notations, define compact set $\mathbf{K} = [0, t_f] \times \mathbf{Q} \times \mathbf{U}$. Consider then the following *linear* program on measures, an instance of the generalized moment problem:

$$\begin{aligned}
 J_{\text{LP}} &= \inf_{\mu, \varphi} \int -|q_2|^2 d\varphi \\
 \text{s.t. } & \int v(t_f, \cdot) d\varphi - v(0, 0) = \int \left(\frac{\partial v}{\partial t} + \frac{\partial v}{\partial q} F(q, u) \right) d\mu, \quad \forall v \in \mathbb{R}[t, q], \quad (\text{LP}) \\
 & \mu \in \mathcal{M}^+(\mathbf{K}), \\
 & \varphi \in \mathcal{M}^+(\mathbf{Q}_f).
 \end{aligned}$$

Proposition 7 (Measure embedding) *To every pair $(u(t), q(t))$ admissible for (OCP) corresponds a pair (μ, φ) admissible for (LP) achieving the same cost, hence*

$$J \geq J_{\text{LP}}.$$

Proof For each admissible pair $(u(t), q(t))$, define its corresponding *time occupation measure* $\mu \in \mathcal{M}^+(\mathbf{K})$ by:

$$\mu(\mathbf{A}, \mathbf{B}, \mathbf{C}) := \int_{[0, t_f] \cap \mathbf{A}} \delta_{q(t)}(\mathbf{B}) \delta_{u(t)}(\mathbf{C}) dt.$$

Here, δ_x is the Dirac measure supported at x , and \mathbf{A} , \mathbf{B} and \mathbf{C} are Borel subsets of resp. $[0, t_f]$, \mathbf{Q} and \mathbf{U} . That is, μ measures the time “spent” by the admissible triplet $(t, u(t), x(t))$ on Borel subsets of \mathbf{K} . Similarly, we define the *final state occupation measure* $\varphi \in \mathcal{M}^+(\mathbf{Q}_f)$ for the same admissible pair simply as $\varphi := \delta_{q(t_f)}$.

Then, evaluating each polynomial test function v along the admissible trajectory yields, by the chain rule:

$$\begin{aligned} v(t_f, q(t_f)) - v(0, q(0)) &= \int_0^{t_f} dv(t, q(t)) \\ &= \int_0^{t_f} \left(\frac{\partial v}{\partial t}(t, q(t)) + \frac{\partial v}{\partial q}(t, q(t)) F(q(t), u(t)) \right) dt. \end{aligned}$$

For the constructed occupation measures, this last temporal integration becomes the weak dynamics of (LP). The proposition follows. \square

Note that the set of admissible vector fields for dynamics F is convex for any $q \in \mathbf{Q}$, such that theorem 3.6 (ii) of [28] holds and $J = J_{\text{LP}}$.

In [21], an alternative formulation as a measure LP is given for switched systems. For these systems, controls are modeled by measures, instead of the above construction defining occupation measures *supported on* the control space. The alternative formulation is believed to be more computationally effective for the moment approach, as it involves measures defined on Euclidean spaces of lower dimension.

Observe that in the single input case, problem (OCP) is bilinear, with the control taking its values inside the polytope defined by $\mathbf{U} = \text{conv}\{-1, +1\}$. The control problem can then be cast as a switched system, the first mode being driving the system with $u(t) = +1$, and the second one by $u(t) = -1$. Following [21], this leads to:

$$\begin{aligned} J_{\text{LP}'} &= \inf_{\mu_1, \mu_2, \varphi} \int -|q_2|^2 d\varphi \\ \text{s.t. } \forall v \in \mathbb{R}[t, q] : & \int v(t_f, \cdot) d\mu_f - v(0, 0) = \\ & \int \left(\frac{\partial v}{\partial t} + \frac{\partial v}{\partial q}(F_0 + F_1) \right) d\mu_1 + \int \left(\frac{\partial v}{\partial t} + \frac{\partial v}{\partial q}(F_0 - F_1) \right) d\mu_2, \quad (\text{LP}') \\ & \mu_1, \mu_2 \in \mathcal{M}^+([0, t_f] \times \mathbf{Q}), \\ & \varphi \in \mathcal{M}^+(\mathbf{Q}_f). \end{aligned}$$

In the following, both measure formulations will be tested on the contrast problem.

2.3.2 Step 2: recasting as a moment SDP

Unfortunately, there is no generic tractable method to solve problems (LP) or (LP'), and additional structure on problem data is required. For optimal control problem (OCP), this structure is provided by the polynomial cost and dynamics, as well as the basic semi-algebraic characterization of the compact sets \mathbf{K} and \mathbf{Q}_f . It is then possible to manipulate measures by their moments in a given polynomial basis, which yields a semi-definite program on countably many moments, with cost $J_{\text{SDP}} = J_{\text{LP}}$. In the following, we concentrate on (LP) in the single-input case, as the discussion is straightforward to adapt for the bi-input case or for alternative formulation (LP').

We first set up the notations. Define the moment of order $k \in \mathbb{N}^n$ of a measure μ supported on $\mathbf{Z} \subset \mathbb{R}^n$ by using the multi-index notation

$$y_k^\mu = \int_{\mathbf{Z}} z_1^{k_1} \cdots z_n^{k_n} d\mu(z) := \int_{\mathbf{Z}} z^k d\mu(z). \quad (26)$$

Conversely, μ is said to be a *representing measure* for an arbitrary sequence of reals y_k^μ if μ satisfies (26) for all $k \in \mathbb{N}^n$. The degree of monomial z^k is denoted by $\deg z^k = |k|_1 = \sum_{i=1}^n k_i$. \mathbb{N}_d^n denotes the set $\{k \in \mathbb{N}^n : |k|_1 \leq d\}$.

Then, with a multi-indexed sequence of reals $y = (y_k)$ with $k \in \mathbb{N}^n$, let $L_y : \mathbb{R}[z] \rightarrow \mathbb{R}$ be the (Riesz) linear functional of $f = \sum_k f_k z^k$ defined by

$$f \mapsto L_y(f) = \sum_k f_k y_k, \quad f \in \mathbb{R}[z].$$

Note that for ease of presentation, we represent the array of coefficients of polynomial $f(z)$ by the same letter f . When confusion may arise, we write the polynomial explicitly by $f(z)$. Also observe that when the sequence y is generated by a measure such as in (26), $L_y(f) = \int f d\mu$ by linearity. Define the moment matrix of order $d \in \mathbb{N}$ associated with an arbitrary sequence of reals y as the real symmetric matrix $M_d(y)$ whose (multi-indexed) (i, j) th entry reads

$$M_d(y)[i, j] = L_y(z^{i+j}) = y_{i+j}, \quad \forall i, j \in \mathbb{N}_d^n. \quad (27)$$

Similarly, define the localizing matrix of order d associated with y and $g \in \mathbb{R}[z]$ as the real symmetric matrix $M_d(g * y)$ whose (i, j) th entry reads

$$M_d(g(z) * y)[i, j] = L_y(g(z) z^{i+j}) = \sum_k g_k y_{i+j+k}, \quad \forall i, j \in \mathbb{N}_d^n. \quad (28)$$

These constructions are central for the following well-known fact:

Proposition 8 *Let \mathbf{Z} be a basic, semi-algebraic set defined by $\mathbf{Z} := \{z \in \mathbb{R}^n : g_i(z) \geq 0, i = 1 \dots n_{\mathbf{Z}}\}$. Then, a necessary condition for a sequence of reals y^μ to have a representing measure $\mu \in \mathcal{M}^+(\mathbf{Z})$ is:*

$$M_d(y^\mu) \succeq 0, \quad M_d(g_i * y^\mu) \succeq 0, \forall d \in \mathbb{N}.$$

Proof Take an arbitrary polynomial $p(z)$ of degree d . Then for a positive measure μ supported on \mathbf{Z} , we have necessarily $0 \leq \int p^2(z) d\mu = p' M_d(y) p$ and also $0 \leq \int p^2(z) g_i(z) d\mu = p' M_d(g_i(z) * y) p$. Since this holds for any $p(x)$, the result follows. \square

Returning back to (LP), notice that \mathbf{K} can be represented by the following *basic, semi-algebraic* representation

$$\mathbf{K} = \left\{ \begin{array}{l} t \in \mathbb{R}, q \in \mathbb{R}^4, u \in \mathbb{R} : \\ g_1(t, q, u) := t(t_f - t) \geq 0 \\ g_2(t, q, u) := 1 - q_{11}^2 - q_{12}^2 \geq 0 \\ g_3(t, q, u) := 1 - q_{21}^2 - q_{22}^2 \geq 0 \\ g_4(t, q, u) := 1 - u^2 \geq 0 \end{array} \right\}, \quad (29)$$

and similarly, for \mathbf{Q}_f :

$$\mathbf{Q}_f = \left\{ \begin{array}{l} q \in \mathbb{R}^4 : \\ g_1^f(q) := q_{11} = 0 \\ g_2^f(q) := q_{12} = 0 \\ g_3^f(q) := 1 - q_{21}^2 - q_{22}^2 \geq 0 \end{array} \right\}. \quad (30)$$

Then, consider the following problem posed on real sequences y^μ and y^φ :

$$\begin{aligned} J_{\text{SDP}} &= \inf_{y^\mu, y^\varphi} L_{y^\varphi}(-|q_2|^2) \\ \text{s.t. } L_{y^\varphi}(v(t_f, \cdot)) - v(0, 0) &= L_{y^\mu} \left(\frac{\partial v}{\partial t} + \frac{\partial v}{\partial q} F(q, u) \right), \quad \forall v \in \mathbb{R}[t, q], \\ M_d(y^\mu) \succeq 0, \quad M_d(g_i * y^\mu) &\succeq 0, \quad \forall d \in \mathbb{N}, \quad i = 1 \dots n_{\mathbf{K}}, \\ M_d(y^\varphi) \succeq 0, \quad M_d(g_i^f * y^\varphi) &\succeq 0, \quad \forall d \in \mathbb{N}, \quad i = 1 \dots n_{\mathbf{Q}_f}. \end{aligned} \quad (\text{SDP})$$

As a simple consequence of Prop. 8, we have

Proposition 9 *Problem (SDP) is a relaxation of (LP), i.e.*

$$J_{\text{LP}} \geq J_{\text{SDP}}.$$

Note that sets \mathbf{K} and \mathbf{Q}_f satisfy the assumptions of [27, Th. 3.8], such that $J_{\text{LP}} = J_{\text{SDP}}$.

2.3.3 Step 3: truncation of moment sequences

The last step is certainly the most obvious one. Problem (SDP) has countably many decision variables, and truncating those to a finite set leads directly to a convex and finite-dimensional program in the form of linear matrix inequalities.

Given that all polynomial data are quadratic, consider the following lmi problems for $r \geq 1$:

$$\begin{aligned} J_{\text{LMI}}^r &= \inf_{(y_k^\mu)_{|k| \leq 2r}, (y_k^\varphi)_{|k| \leq 2r}} L_{y^\varphi}(-|q_2|^2) \\ \text{s.t. } \quad \forall v \in \mathbb{R}[t, q] : \\ L_{y^\varphi}(v(t_f, \cdot)) - v(0, 0) &= L_{y^\mu} \left(\frac{\partial v}{\partial t} + \frac{\partial v}{\partial q} F(q, u) \right), \quad (\text{LMI}) \\ M_r(y^\mu) \succeq 0, \quad M_{r-s_i}(g_i * y^\mu) &\succeq 0, \quad i = 1 \dots n_{\mathbf{K}}, \\ M_r(y^\varphi) \succeq 0, \quad M_{r-s_i^f}(g_i^f * y^\varphi) &\succeq 0, \quad i = 1 \dots n_{\mathbf{Q}_f}. \end{aligned}$$

where $s_i = \deg(g_i)/2$ if $\deg(g_i)$ is even and $(\deg(g_i) + 1)/2$ otherwise. Similarly, $s_i^f = \deg(g_i^f)/2$ if $\deg(g_i^f)$ is even and $(\deg(g_i^f) + 1)/2$ otherwise. Note that since $M_{r+1} \succeq 0$ implies $M_r \succeq 0$, only the highest order moment matrices and localizing matrices are necessary. In addition, as only additional constraints are added at each higher relaxation order, we have the following result:

Proposition 10 (Lasserre’s relaxation hierarchy)

$$J_{\text{SDP}} \geq \dots \geq J_{\text{LMI}}^{r+1} \geq J_{\text{LMI}}^r \geq \dots \geq J_{\text{LMI}}^2 \geq J_{\text{LMI}}^1.$$

It is also shown in [28] that the costs of the `lmi` relaxations actually converge to that of the cost of (SDP) when $r \rightarrow \infty$.

2.3.4 Example: construction of the first relaxation

We conclude the presentation of the method by explicitly constructing the first relaxation of (OCP) for the single input case, under measure formulation (LP). Define the indexing of moments in the monomial basis by

$$y_{ijklmn}^\mu := \int t^i q_{11}^j q_{12}^k q_{21}^\ell q_{22}^m u^n d\mu, \quad y_{jklm}^\varphi := \int q_{11}^j q_{12}^k q_{21}^\ell q_{22}^m d\varphi.$$

Then, the cost of (LMI) is explicit by

$$J_{\text{LMI}}^1 = \inf L_{y^\varphi}(-|q_2|^2) = -y_{0020}^\varphi - y_{0002}^\varphi,$$

where the decision variables are members of the finite sets $\{y_{ijklmn}^\mu : i + j + k + \ell + m + n \leq 2\}$ and $\{y_{jklm}^\varphi : j + k + \ell + m \leq 2\}$. For the weak dynamics of (LMI), all polynomial test functions of degree 1 or lower will lead to linear constraints involving moments of order two or less. Plugging $v = 1, t, q_{11}, \dots, q_{22}$ into (LMI) leads to

$$\begin{aligned} y_{0000}^\varphi - 1 &= 0, \\ t_f - 0 &= y_{000000}^\mu, \\ y_{1000}^\varphi - 0 &= -\Gamma_1 y_{010000}^\mu - y_{001001}^\mu, \\ y_{0100}^\varphi - 1 &= \gamma_1 y_{000000}^\mu - \gamma_1 y_{001000}^\mu + y_{010001}^\mu, \\ y_{0010}^\varphi - 0 &= -\Gamma_2 y_{000100}^\mu - y_{000011}^\mu, \\ y_{0001}^\varphi - 1 &= \gamma_2 y_{000000}^\mu - \gamma_2 y_{000010}^\mu + y_{000101}^\mu. \end{aligned}$$

The semi-definite constraints for the moment matrices are, applying (27):

$$\begin{bmatrix} y_{000000}^\mu & y_{100000}^\mu & \cdots & y_{000001}^\mu \\ y_{100000}^\mu & y_{200000}^\mu & \cdots & y_{100001}^\mu \\ \vdots & \vdots & \ddots & \vdots \\ y_{000001}^\mu & y_{100001}^\mu & \cdots & y_{000002}^\mu \end{bmatrix} \succeq 0, \quad \begin{bmatrix} y_{0000}^\varphi & y_{1000}^\varphi & \cdots & y_{0001}^\varphi \\ y_{1000}^\varphi & y_{2000}^\varphi & \cdots & y_{1001}^\varphi \\ \vdots & \vdots & \ddots & \vdots \\ y_{0001}^\varphi & y_{1001}^\varphi & \cdots & y_{0002}^\varphi \end{bmatrix} \succeq 0.$$

All inequalities defining \mathbf{K} and \mathbf{Q}_f in (29) and (30) are quadratic, hence their corresponding localizing moment matrix given by (28) is a scalar at the first relaxation, leading to

$$\begin{aligned} M_0(g_1 * y^\mu) &= t_f y_{100000}^\mu - y_{200000}^\mu \geq 0, \\ M_0(g_2 * y^\mu) &= y_{000000}^\mu - y_{020000}^\mu - y_{002000}^\mu \geq 0, \\ M_0(g_3 * y^\mu) &= y_{000000}^\mu - y_{000200}^\mu - y_{000020}^\mu \geq 0, \\ M_0(g_4 * y^\mu) &= y_{000000}^\mu - y_{000002}^\mu \geq 0, \\ M_0(g_3^f * y^\varphi) &= y_{0000}^\varphi - y_{0020}^\varphi - y_{0002}^\varphi \geq 0. \end{aligned}$$

Finally, the equalities $g_1(q) = 0$ and $g_2(q) = 0$ defining \mathbf{Q}_f can be restated as the following linear equalities:

$$\begin{aligned} y_{1000}^\varphi &= y_{2000}^\varphi = y_{1100}^\varphi = y_{1010}^\varphi = y_{1001}^\varphi = 0, \\ y_{0100}^\varphi &= y_{1100}^\varphi = y_{0200}^\varphi = y_{0110}^\varphi = y_{0101}^\varphi = 0. \end{aligned}$$

2.3.5 Summary of the LMI method

The moment/LMI method approach for optimization consist in reformulating an optimization problem as a linear program on measures. When the data is polynomial, a hierarchy of LMI relaxations can be constructed, whose cost converge to that of the original problem.

The strong feature of the method is that those LMIs generate lower bounds on the true cost, and can therefore be used as certificates of global optimality. On the other hand, the weak points of the method are its poor algorithmic complexity for unstructured problem, as well as for the special case of optimal control, the unavailability of a generic method to recover controls.

Note that the passage to a given LMI relaxation starting from measure problem (LP) or (LP') can be fully automated with high-level commands using the GLOP-TIPOLY toolbox [22].

3 Numerical simulations, single-input case

We present here the results about the single-input case (see subsection 1.3.2) of the problem (OCP). From the experimental point of view we are interested in the following cases, the parameters being the relaxation times given in seconds and the minimal time to steer the first spin from the north pole to the center of the Bloch ball.

P_1 : Fluid case.

Spin 1: Cerebrospinal fluid: $T_1 = 2$, $T_2 = 0.3$;

Spin 2: Water: $T_1 = 2.5 = T_2$.

$T_{\min} = 26.17040$.

P_2 : Blood case.

Spin 1: Deoxygenated blood: $T_1 = 1.35$, $T_2 = 0.05$;

Spin 2: Oxygenated blood: $T_1 = 1.35$, $T_2 = 0.2$.

$T_{\min} = 6.7981$.

Recalling difficulty 1, we need to know the control structure (meaning the number of Bang-Singular sequences) before calling the multiple shooting method. A possible strategy is to use continuation (or homotopy) techniques introducing for example Tychonov type regularization, in order to detect the n BS sequence and find a smooth approximation of the non-smooth solution. In [11, 18] this kind of strategy is applied. Here, we use the `Bocop` software based upon direct methods (detailed in subsection 2.1) to obtain approximate optimal solutions used to initialize indirect shooting. In both cases P_1 and P_2 , the contrast problem has many local solutions, see difficulty 2, possibly with different control structures. Besides, the structure of the best policy can change depending on the final time, as detailed below in 3.5 and 3.6, see also [18] for full details.

In this section, we first detail in four steps how we can obtain a potential local optimal solution for a fixed t_f chosen in the $[T_{\min}, 3T_{\min}]$ range. In subsection 3.1, optimization by the direct method provides first approximations, and in 3.2 the control structure is given to initialize indirect shooting in 3.3 and to check second order necessary conditions in 3.4. Then, we are interested in the influence of the final time on the best policy in subsection 3.5. We have to monitor crossing between value functions, change of structure along one same path and second order necessary conditions. The simulations from subsection 3.1 to subsection 3.5 are detailed only in the fluid case. In subsection 3.6, we give for the fluid and blood cases, the best sub-optimal syntheses we have and finally we compare these sub-optimal syntheses with estimates of global optima obtained from `lmi` techniques in 3.7. These comparisons are used to assert the global optimality of the solutions obtained from direct and indirect approaches.

Before presenting the results, we explain how we introduce the λ variable. To do that, we change the parameterization of our Mayer problem introducing the time τ such that $\lambda T_{\min} \tau = t$. Using the notations from the introduction, the new problem becomes: $\min_{u(\cdot)} c(q(\tau_f))$, $\dot{q} = \lambda T_{\min} F(q, u)$, $q(\tau_0) = q_0$, $f(q(\tau_f)) = 0$, $\tau_0 = 0$ and $\tau_f = 1$. Then in the BS case, $h(x, \lambda) = S_\lambda(x)$, $x = (p_0, \tau_1, z_1)$ where

$$S_\lambda : \mathbb{R}^{3n+1} \rightarrow \mathbb{R}^{3n+1}$$

$$\begin{pmatrix} p_0 \\ \tau_1 \\ z_1 \end{pmatrix} \mapsto S_\lambda(p_0, \tau_1, z_1) = \begin{pmatrix} H_1(z_1) \\ \{H_1, H_0\}(z_1) \\ q_{1,s}([\tau_f]) \\ \langle p_{2,s}([\tau_f]), q_{2,s}([\tau_f]) \rangle - |q_{2,s}([\tau_f])|^2 \\ z(\tau_1, t_0, z_0, \lambda) - z_1 \end{pmatrix}, \quad (31)$$

where $[\tau_f]$ stands for $(\tau_f, \tau_1, z_1, \lambda)$.

3.1 Step 1: direct method

We present here the results for the direct approach. The only a priori information is the value of the minimum time transfer T_{\min} from [18], used to set the final time t_f in the $[T_{\min}, 3T_{\min}]$ range. We note $t_f = \lambda T_{\min}$ with λ in $[1, 3]$. The state variables are initialized as constant functions, with the values $y_1(\cdot) = 0$, $z_1(\cdot) = 0.5$, $y_2(\cdot) = 0$,

$z_2(\cdot) = 1$. For the control variables we also use a constant function, with four different initializations $u_1(\cdot) \in \{0.05, 0.1, 0.25, 0.5\}$. The discretization method used is implicit midpoint (2nd order) with 500 to 1000 time steps depending on the problem. In order to improve convergence, we add a small regularization term to the objective to be minimized, $\varepsilon \int_0^{t_f} |u(t)|^2 dt$, with $\varepsilon = 10^{-5}$.

We repeat the four optimizations (with the different control initializations) for λ in $\{1.1, 1.5, 1.8, 2.0, 3.0\}$. Bocop converges for all initializations except when $\lambda = 3$, where only one optimization out of four converges. Table 1 groups together the results from all the optimizations. For each solution, we give the contrast and the corresponding rank between each different initializations for a same value of λ . We also indicate the norm of the approximate initial adjoint vector $p(0)$, taken from the multipliers for the discretized dynamics in the (NLP) problem. For both $\lambda = 1.8$ and $\lambda = 2.0$, three different initializations lead to the same solution while for $\lambda = 1.1$ and $\lambda = 1.5$, the four initializations converge to four different solutions. Note that solutions 11b and 11c seem to be identical, and similarly solutions 20a and 20b do not differ a lot, as shown on Figs. 2 and 3. This illustrates Difficulty 2 about the many local solutions, due in particular to symmetry reasons.

Table 1 Fluid case, step 1: Direct method. Results of optimizations from direct methods. The final time $t_f = \lambda T_{\min}$ is taken such as $\lambda \in \{1.1, 1.5, 1.8, 2.0, 3.0\}$. The control is initialized by a constant in $\{0.05, 0.1, 0.25, 0.5\}$. For each solution, the contrast and the norm of the adjoint vector (coming from the multipliers for the discretized dynamics in the (NLP) problem) are given. For a fixed λ we present the rank of the solutions based on the contrast level. Note that if two ranks are equal, the two optimizations have converged to the same solution. Finally a name is given for each different solution.

λ	$u_1(\cdot)$ init.	Contrast	Rank	$ p(0) $	Name
1.1	0.05	0.6460	1	0.7229	11a
1.1	0.10	0.6444	2	0.7213	11b
1.1	0.25	0.6441	3	0.7212	11c
1.1	0.50	0.6414	4	0.7212	11d
1.5	0.05	0.6899	2	0.6185	15a
1.5	0.10	0.6872	4	0.6187	15b
1.5	0.25	0.6930	1	0.6186	15c
1.5	0.50	0.6877	3	0.6196	15d
1.8	0.05	0.6915	2	0.5596	18a
1.8	0.10	0.7025	1	0.5596	18b
1.8	0.25	0.7025	1	0.5596	18b
1.8	0.50	0.7024	1	0.5595	18b
2.0	0.05	0.7050	1	0.5239	20a
2.0	0.10	0.7017	2	0.5239	20b
2.0	0.25	0.7051	1	0.5239	20a
2.0	0.50	0.7051	1	0.5240	20a
3.0	0.05	0.7079	1	0.3787	30a

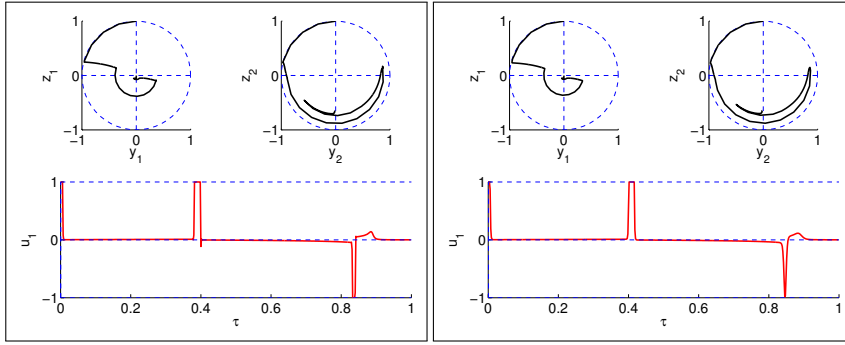


Fig. 2 Fluid case, step 1: Direct method. Solutions 11b (left subplot) and 11c (right subplot) from Table 1 obtained with Bocop. Trajectories for spin 1 and 2 in the (y,z) -plane are portrayed in the first two subgraphs of each subplot. The corresponding control is drawn in the bottom subgraph. Note that the first singular arcs, for each control subgraph, do not end at the same times.

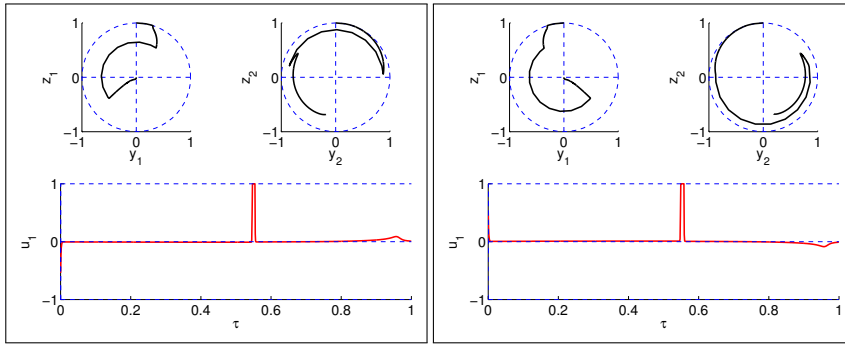


Fig. 3 Fluid case, step 1: Direct method. Solutions 20a (left subplot) and 20b (right subplot) from Table 1 obtained with Bocop. Trajectories for spin 1 and 2 in the (y,z) -plane are portrayed in the first two subgraphs of each subplot. The corresponding control is drawn in the bottom subgraph. The two bang arcs have the same sign for solution 20a, whereas for solution 20b, the two bang arcs are of opposite sign.

3.2 Step 2: determination of the structure

The structure is obtained by examination of the control plots. This gives the normalized switching times τ_i and the state-costate $z_i = z(\tau_i)$ associated, $i = 1, \dots, m-1$, or similarly t_i since $t_i = \lambda T_{\min} \tau_i$, where m is the number of bang and singular arcs (a 2BS structure has $m = 4$ arcs). The variables τ_i and $z(\tau_i)$, $i = 1, \dots, m-1$, with the initial adjoint vector $p_0 = p(0)$ are required to initialize the multiple shooting method, see the definitions of the shooting function in the BS case at eqs. (24) (with time t) and (31) (with normalized time τ). Table 2 sums up the different structures for all the distinct solutions found in Table 1. We can already notice that the best structure found by the direct approach is 3BS for $\lambda = 1.1$ and then 2BS for greater values of λ .

Table 2 Fluid case, step 2: determination of the structure. Same as Table 1 but with only the distinct solutions and reorganized. For each solution, a name and the contrast are given. For a fixed λ we present the rank of the solutions based on the contrast level. The structure is denoted by the signs of the bang arcs, and we normalize the first bang arc to be positive.

λ	Name	Contrast	Rank	Structure
1.1	11a	0.6460	1/4	1 -1 -1
1.1	11b	0.6444	2/4	1 1 -1
1.1	11c	0.6441	3/4	1 1 -1
1.1	11d	0.6414	4/4	1 1
1.5	15c	0.6930	1/4	1 -1
1.5	15a	0.6899	2/4	1 1
1.5	15d	0.6877	3/4	1 -1 -1
1.5	15b	0.6872	4/4	1 -1 1
1.8	18b	0.7025	1/2	1 -1
1.8	18a	0.6915	2/2	1 -1 1
2.0	20a	0.7050	1/2	1 -1
2.0	20b	0.7017	2/2	1 1
3.0	30a	0.7079	1/1	1 -1

3.3 Step 3: multiple shooting method

Thanks to steps 1 and 2, we have good approximations of the solutions in order to initialize the multiple shooting method described at 2.2.1, which solve the following shooting equation (see eq. (31)):

$$S_\lambda(p_0, \tau_1, z_1, \dots, \tau_{m-1}, z_{m-1}) = 0,$$

where m is the number of arcs, $\tau_0 = 0$ and $\tau_f = 1$, and the structure is $\frac{m}{2}$ BS.

However, since indirect shooting methods are very sensitive to the initial point, we perform for each of the 13 different solutions from Table 2 not one but many shoots. Note that one call to the method is about a few seconds. To do so we add a random small perturbation $\varepsilon_i \in [-0.1, 0.1]$ to τ_i , $i = 1, \dots, m-1$, before each call to the method. The approximate new state-costate $z_{\varepsilon_i} = z(\tau_{\varepsilon_i})$, $\tau_{\varepsilon_i} = \tau_i + \varepsilon_i$ is obtained thanks to the discretized solution from step 1. We finally solve the shooting equation

$$S_\lambda(p_0, \tau_{\varepsilon_1}, z_{\varepsilon_1}, \dots, \tau_{\varepsilon_{m-1}}, z_{\varepsilon_{m-1}}) = 0 \quad (32)$$

about a hundred times, with different random perturbations.

Notice that with this algorithm, one initialization from Table 2 can provide several solutions. Table 3 groups together the distinct solutions obtained after convergence of the multiple shooting method. Four initializations (11b, 11c, 11d and 15b) from Table 2 never made the method converge, whereas for instance, the two initializations 20a and 20b gave 12 different solutions. Note that for a given λ , the best direct optimization from Table 2 always provides the best solution after shooting.

Remark 7 We keep every solution from Table 3 because of difficulty 2.

Table 3 Fluid case, step 3: multiple shooting. Results after many calls to the multiple shooting method. The shooting equation solved is (32). This table gives, the value of λ , the initial name, the contrast and rank from Table 2 obtained by direct optimizations. The new contrast and rank after shooting is also provided with the structure of the solutions and the norm of the shooting function after convergence. Note that for a given λ , the best direct optimization from Table 2 always provides the best solution after shooting.

λ	Init. Name	Init. Contrast	Init. rank	New Contrast	New Rank	Structure	$ S_\lambda $
1.1	11a	0.6460	1/4	0.6452	1/2	1 -1 -1	1.12e-13
1.1	11a	0.6460	1/4	0.6361	2/2	1 -1 -1	6.02e-14
1.5	15c	0.6930	1/4	0.6919	1/7	1 -1	5.08e-14
1.5	15a	0.6899	2/4	0.6888	2/7	1 1	2.03e-14
1.5	15d	0.6877	3/4	0.6860	3/7	1 -1 -1	2.73e-13
1.5	15c	0.6930	1/4	0.6837	4/7	1 -1	1.01e-12
1.5	15c	0.6930	1/4	0.6759	5/7	1 -1	2.76e-14
1.5	15a	0.6899	2/4	0.6741	6/7	1 1	3.16e-14
1.5	15a	0.6899	2/4	0.6664	7/7	1 1	3.43e-12
1.8	18b	0.7025	1/2	0.7014	1/6	1 -1	1.64e-13
1.8	18a	0.6915	2/2	0.6980	2/6	1 -1 1	1.21e-10
1.8	18b	0.7025	1/2	0.6927	3/6	1 -1	3.50e-13
1.8	18a	0.6915	2/2	0.6894	4/6	1 -1 1	2.36e-12
1.8	18b	0.7025	1/2	0.6844	5/6	1 -1	1.38e-13
1.8	18b	0.7025	1/2	0.6764	6/6	1 -1	3.02e-13
2.0	20a	0.7050	1/2	0.7040	1/12	1 -1	2.23e-14
2.0	20b	0.7017	2/2	0.7005	2/12	1 1	2.56e-14
2.0	20a	0.7050	1/2	0.6977	3/12	1 -1	5.25e-14
2.0	20a	0.7050	1/2	0.6951	4/12	1 -1	3.40e-13
2.0	20b	0.7017	2/2	0.6918	5/12	1 1	1.72e-13
2.0	20a	0.7050	1/2	0.6912	6/12	1 -1	7.88-07
2.0	20b	0.7017	2/2	0.6879	7/12	1 1	8.75e-07
2.0	20a	0.7050	1/2	0.6865	8/12	1 -1	2.47e-13
2.0	20b	0.7017	2/2	0.6833	9/12	1 1	2.43e-11
2.0	20a	0.7050	1/2	0.6829	10/12	1 -1	1.69e-13
2.0	20a	0.7050	1/2	0.6783	11/12	1 -1	2.13e-13
2.0	20b	0.7017	2/2	0.6751	12/12	1 1	1.10e-12
3.0	30a	0.7079	1/1	0.7013	1/2	1 -1	7.18e-14
3.0	30a	0.7079	1/1	0.6923	2/2	1 -1	2.23e-13

Fig. 4 groups together solutions 1/12 and 6/12 for $\lambda = 2.0$ from Table 3. The switching times (vertical dashed lines) from direct optimization 20a are added on the control subplot to compare the initialization 20a with the solutions obtained after convergence of the multiple shooting method.

3.4 Step 4: second order conditions

According to proposition 3.2 from [11], the non-existence of conjugate points on each singular arc of a candidate solution is a necessary condition of local optimality. See [11] for details about conjugate points in the contrast problem. Here, we compute for each singular arc of all the solutions from Table 3, the first conjugate point along

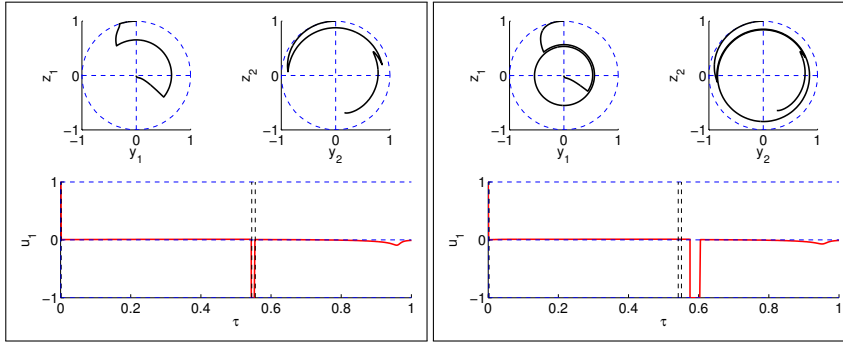


Fig. 4 Fluid case, step 3: multiple shooting. Solutions 1/12 (left subplot) and 6/12 (right subplot) for $\lambda = 2.0$ from Table 3, with the switching times (vertical dashed lines) from direct optimization 20a. Trajectories for spin 1 and 2 in the (y,z) -plane are portrayed in the first two subgraphs of each subplot. The corresponding control is drawn in the bottom subgraph.

the arc, applying the algorithm presented in subsection 4.3 from [11]. None of the solutions has a conjugate point on a singular arc. Hence all the solutions satisfy the second order necessary condition of local optimality. Fig. 5 represents the computations of the two conjugate points (since the structure is 2BS) of solution 1/12 with $\lambda = 2.0$ from Table 3.

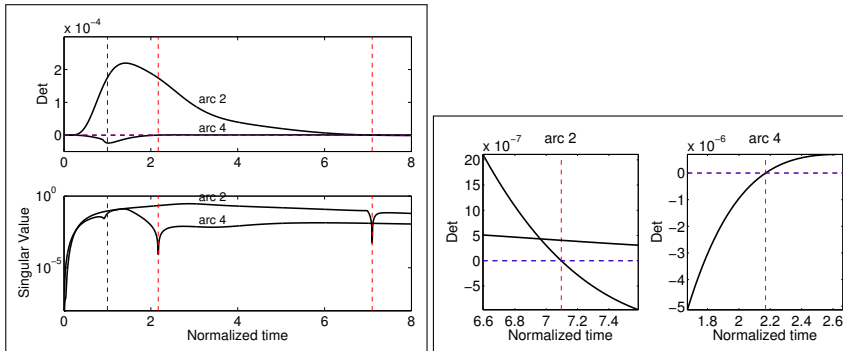


Fig. 5 Fluid case, step 4: second order conditions. Second order necessary condition check on solution 1/12 with $\lambda = 2.0$ from Table 3. The rank condition from the algorithm presented in subsection 4.3 from [11] is evaluated along the two singular arcs. See [6] for details on the concept of conjugate times. On the left subplot, for each singular arc, the curve is reparameterized so that the final time corresponds to the abscissa 1 (vertical blue dashed line); the determinant associated with the rank condition is plotted (top subgraph), so there is a conjugate time whenever it vanishes (vertical red dashed lines). One observes that conjugate times on each arc are located after the (normalized to 1) final time, satisfying necessary condition of local optimality of the trajectory. At the bottom, the smallest singular value of the matrix whose rank we test is plotted, extracting only the relevant information to detect the rank drops. On the right subplot is presented a zoom of top-left subgraph near the two conjugate times.

3.5 Step 5: influence of the final time (homotopy method)

Given that the initial point (the North pole) is a stationary point, the contrast is an increasing function of t_f acting as a parameter. Indeed, applying a zero control at $t = 0$ leaves the system in its initial state so there is an inclusion of admissible controls between problems when the final time is increased (and the bigger the set of controls, the larger the maximum contrast). Having increasing bounded (by one, which is the maximum possible contrast given the final condition on spin no. 1) functions, it is natural to expect asymptotes on each branch.

For all solutions from Table 3, provided by multiple shooting, a first homotopy on λ is made in the range $[1, 3]$. Fig. 6 shows the path of zeros in the left subgraph with the value function and the norm of the shooting function, for solution 2/12, $\lambda = 2$, from Table 3. The right subgraph presents the value functions of solutions 5/12, 9/12 and 12/12 after the homotopies, showing the branches of different local solutions.

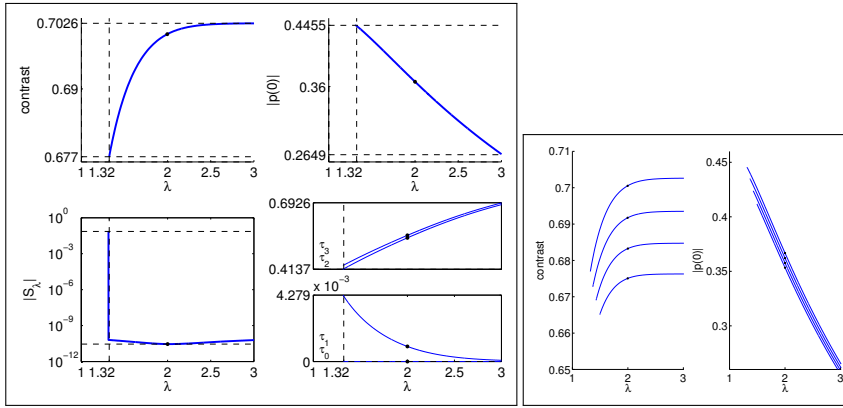


Fig. 6 Fluid case, step 5: influence of the final time. On the left subgraph: homotopy on solution 2/12, $\lambda = 2.0$ from Table 3. The blue color represents 2BS solutions. The value function, the norm of the initial adjoint vector, the norm of the shooting function and the switching times along the path are given. A first homotopy from $\lambda = 2$ to $\lambda = 3$ is made. A second from $\lambda = 2$ to $\lambda = 1$ stops around $\lambda = 1.32$ since the norm of the shooting function becomes greater than a threshold fixed to 10^{-3} . This threshold is an option given to the homotopic method. The right subgraph displays the value functions after homotopies on solutions 5/12, 9/12 and 12/12 for $\lambda = 2.0$ from Table 3. All four homotopies stop before reaching $\lambda = 1$. These four path of zeros of local solutions have a distinctive feature. For a fixed λ , the time interval of the second bang arc of the best solution among the four path, is included in the time interval of the second bang arc of the second best solution, and so on.

The possible change of structure along a path of zeros is emphasized in Fig. 7. In the right subgraph of this figure, the path of zeros from Fig. 6 is extended, after the detection of a saturating singular arc (see left subgraph). Note that there is no solution from Table 3 on this extended path. Hence a new branch has been found by this detection. Note also that the 2BS solution are represented in blue, the 3BS in red and the 4BS in green. Then for each solution of each branch the second order necessary condition is checked as in subsection 3.4: the first conjugate point of each singular extremal is computed. There is no failure in this test, hence all the solutions

satisfy the necessary second order condition of local optimality. Fig. 8 presents the simulations for solution 2/12, $\lambda = 2$, from Table 3. Finally, we detect some crossing between value functions of different path of zeros as we can see in Fig. 9.

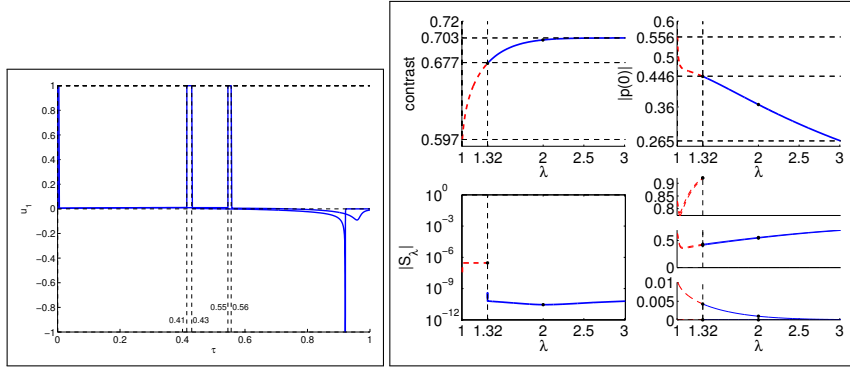


Fig. 7 Fluid case, step 5: influence of the final time. On the left subgraph are shown the control laws of solutions at $\lambda = 2$ and $\lambda = 1.32$ from path from Fig. 6. For $\lambda = 1.32$, we can see the saturating singular arc around $\tau = 0.92$. The 2BS solution at $\lambda = 1.32$ is used to initialize a multiple shooting with a 3BS structure and then to perform a new homotopy from $\lambda = 1.32$ to $\lambda = 1$. On the right subgraph: complete homotopy on solution 2/12, $\lambda = 2.0$ from Table 3 is portrayed. Compare to Fig. 6. The value function, the norm of the initial adjoint vector, the norm of the shooting function and the switching times along the path are given. The blue color represents 2BS solutions while the red color is for 3BS structures. The dashed red lines come from the extended path after the change of structure detected around $\lambda = 1.32$. Note that there is no solution from Table 3 on the 3BS part of the extended path. Hence a new branch has been found.

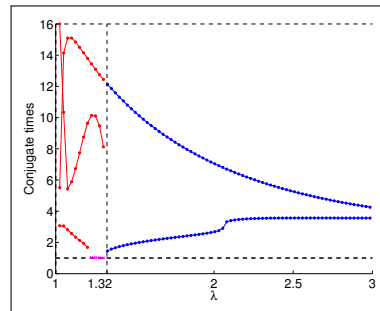


Fig. 8 Fluid case, step 5: influence of the final time. Second order necessary condition checked along the extended path from Fig. 7. For all solutions from $\lambda = 1$ to $\lambda = 3$ are computed the first conjugate times along each singular arc. For $\lambda \in [1, 1.32]$, the structure is 3BS and there are 3 singular arcs. For $\lambda \in [1.32, 3]$, there are 2 singular arcs. Each singular interval is normalized in such a way the initial time is 0 and the final time is 1. The lower dashed horizontal line represents the final time 1. There is no conjugate time before the normalized final time 1 which means that all solutions satisfy the second order necessary condition of local optimality. This is true for all extended path of zeros coming from solutions from Table 3. Note that the magenta crosses, plotted just before $\lambda = 1.32$, give the time when a singular arc saturates the constraint $|u| = 1$.

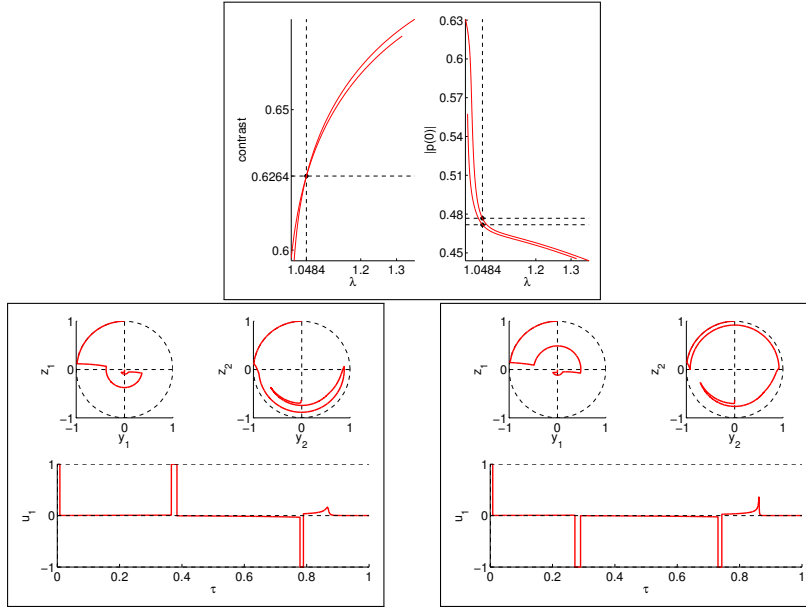


Fig. 9 Fluid case, step 5: influence of the final time. Crossing between branches coming from 3BS solution 1/2 with $\lambda = 1.1$ and 2BS solution 2/12 with $\lambda = 2$, after change of structure, from Table 3. Note that the 3BS solution 1/2 with $\lambda = 1.1$ and all the 2BS solutions 1/7 with $\lambda = 1.5$, 1/6 with $\lambda = 1.8$ and 1/12 with $\lambda = 2$ give the same extended path after a change of structure. The crossing is around $\lambda = 1.0484$. Thus for $\lambda \leq 1.0484$, the best solution has a 3BS structure of the form $\delta_+ \delta_s \delta_+ \delta_s \delta_- \delta_s$ (bottom-left subgraph) while for $\lambda \in [1.0484, 1.351]$ the best solution is of the form $\delta_+ \delta_s \delta_- \delta_s \delta_- \delta_s$ (bottom-right subgraph). On the two bottom subgraphs, the trajectories for spin 1 and 2 in the (y, z) -plane are portrayed with the corresponding control, both for $\lambda = 1.0484$.

3.6 Sub-optimal syntheses in fluid and blood cases

We give the syntheses of locally optimal solutions obtained in the blood and fluid cases. Note that in the special case $t_f = T_{\min}$, for both cases the solution is 2BS and of the form $\delta_+ \delta_s \delta_+ \delta_s$.

For the fluid case, the left subplot of Fig. 10 represents all the different branches obtained in step 5 by homotopy on λ . The greatest two value functions intersect around $t_f = 1.048T_{\min}$. The right subplot shows the sub-optimal synthesis. The best policy is:

$$\begin{aligned}
 & \delta_+ \delta_s \delta_+ \delta_s && \text{for } \lambda \in [1.000, 1.006], \\
 & \delta_+ \delta_s \delta_+ \delta_s \delta_- \delta_s && \text{for } \lambda \in [1.006, 1.048], \\
 & \delta_+ \delta_s \delta_- \delta_s \delta_- \delta_s && \text{for } \lambda \in [1.048, 1.351], \\
 & \delta_+ \delta_s \delta_- \delta_s && \text{for } \lambda \in [1.351, 3.000].
 \end{aligned} \tag{33}$$

For the blood case, the results are excerpted from [18]. The left subplot of Fig. 11 shows the contrast for five different components of $\{h = 0\}$, for final times $t_f \in [1, 2]T_{\min}$. The three black branches are made only of BS solutions whereas the two others are made of 2BS and 3BS solutions. To maximise the contrast, the best policy,

drawn as solid lines, is:

$$\begin{aligned}
 & \delta_+ \delta_s \delta_+ \delta_s && \text{for } \lambda = 1.000, \\
 & \delta_+ \delta_s && \text{for } \lambda \in (1.000, 1.294], \\
 & \delta_+ \delta_s \delta_- \delta_s \delta_- \delta_s && \text{for } \lambda \in [1.294, 2.000].
 \end{aligned} \tag{34}$$

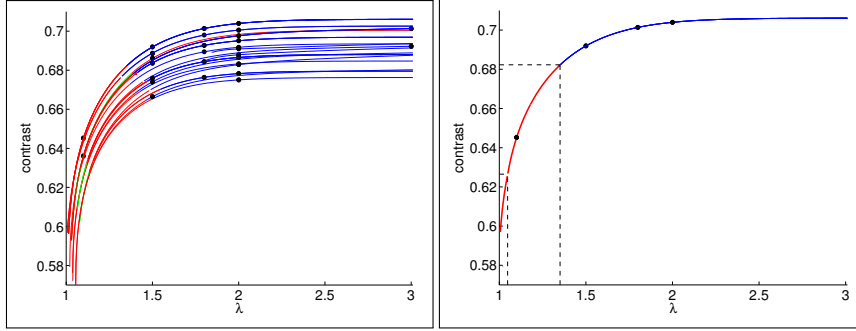


Fig. 10 Fluid case, sub-optimal synthesis. Illustration on the left subplot, of local solutions (each branch corresponds to a control structure). The suboptimal synthesis is plotted on right subplot. The colors are blue for 2BS structure, red for 3BS and green for 4BS. The best policy is $\delta_+ \delta_s \delta_+ \delta_s$ for $\lambda \leq 1.0484$, and $\delta_+ \delta_s \delta_- \delta_s \delta_- \delta_s$ for $\lambda \in [1.0484, 1.351]$. Then, for $\lambda \in [1.351, 3]$, the best policy is 2BS and of the form $\delta_+ \delta_s \delta_- \delta_s$.

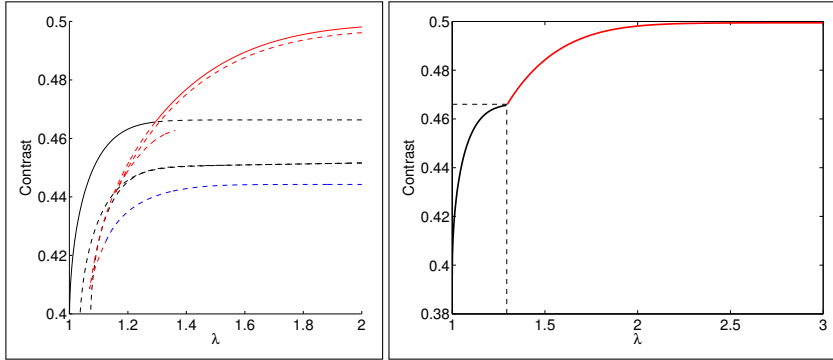


Fig. 11 Blood case, sub-optimal synthesis. Illustration on the left subplot, of local solutions (each branch corresponds to a control structure). Best policy as solid lines, local solutions as dashed lines. The suboptimal synthesis is plotted on right subplot. The colors are black for BS structure, blue for 2BS and red for 3BS. The best policy is BS for $t_f \in (1, 1.294)T_{\min}$ and 3BS of the form $\delta_+ \delta_s \delta_- \delta_s \delta_- \delta_s$ for $t_f \in (1.294, 2]T_{\min}$. In the special case $t_f = T_{\min}$, the solution is 2BS and of the form $\delta_+ \delta_s \delta_+ \delta_s$.

3.7 Step 6: sub-optimal syntheses compared to global results (lmi method)

We now apply the lmi method to the contrast problem, in order to obtain upper bounds on the true contrast. Comparing these bounds to the contrast of our solutions then gives an insight about their global optimality.

Table 4 shows the evolution of the upper bound on the contrast in function of LMI relaxation order, for the fluid case with $t_f = T_{\min}$. Both formulations (LP) and (LP') are compared. As expected, the method yields a monotonically non-increasing sequence of sharper bounds. Relaxations of orders 4 and 5 yield very similar bounds, but this should not be interpreted as a termination criterion for the lmi method. Formulation (LP') allows for faster computation times at high relaxation orders, which was the principal motivation for its introduction. One can also notice that (LP') leads to sharper bounds than (LP). This is explained by the higher number of linear constraints admitted by the former at a given relaxation order. Indeed, $F(q, u)$ in (LP) is bilinear in its arguments whereas $F_0(q) \pm F_1(q)$ in (LP') is simply linear. This last formulation therefore admits test functions v of one extra degree at any given relaxation order.

r	Formulation (LP)			Formulation (LP')		
	$\sqrt{-J_M^r}$	N_r	t_r	$\sqrt{-J_M^r}$	N_r	t_r
1	1.000	49	0.2	0.8474	63	0.7
2	0.8301	336	1	0.7552	378	3
3	0.6928	1386	8	0.6226	1386	14
4	0.6086	4290	857	0.6069	3861	332
5	0.6007	11011	30800	0.6040	9009	8400

Table 4 Comparison of formulations (LP) and (LP') for the fluid case with $t_f = T_{\min}$: upper bounds on contrast $\sqrt{-J_M^r}$, numbers of moments N_r and CPU times t_r in function of relaxation order r .

Fig. 12 compares the evolution of the upper bounds for different values of $t_f \in [T_{\min}, 3T_{\min}]$, for the blood and fluid cases respectively. For the whole end-time interval, (LP') does produce sharper bounds than (LP), although this is not guaranteed.

Finally, Fig. 13 compares the tightest upper bounds found by the lmi method against the best candidate solutions found by Bocop and HamPath, in both the blood and fluid cases. The figures also represent the relative gap between the methods defined as $(C_{LMI} - C_H)/C_H$, where C_{LMI} is the lmi upper bound and C_H is the contrast found with HamPath. As such, this measure characterizes the optimality gap between the methods. It does not, however, specify which of the method(s) could be further improved.

At the fifth relaxation, the average gap is around 11% in the blood case, which, given the application, is satisfactory on the experimental level. For the fluid case, the average gap on the contrast is about 2% at the fifth relaxation, which strongly suggest that the solution is actually a global optimum. The gap is even below the 1% mark for $t_f \leq 2T_{\min}$.

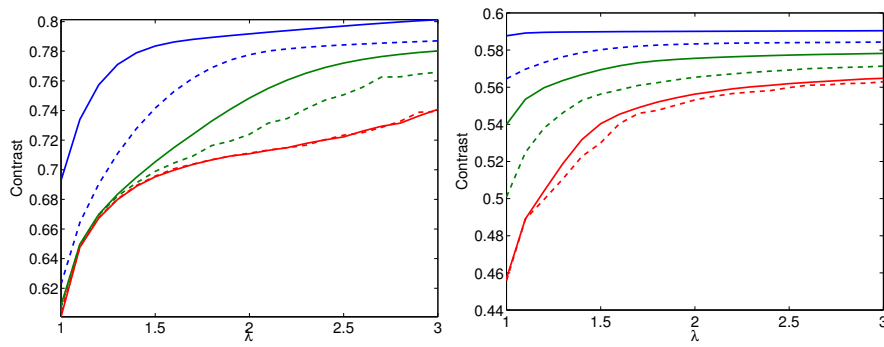


Fig. 12 Step 6: LMI. Upper bounds on contrast, for **fluid case** on left subgraph and **blood case** on right subgraph, in function of final time for formulations (LP) (straight lines) and (LP') (dashed) for relaxation orders 3 to 5.

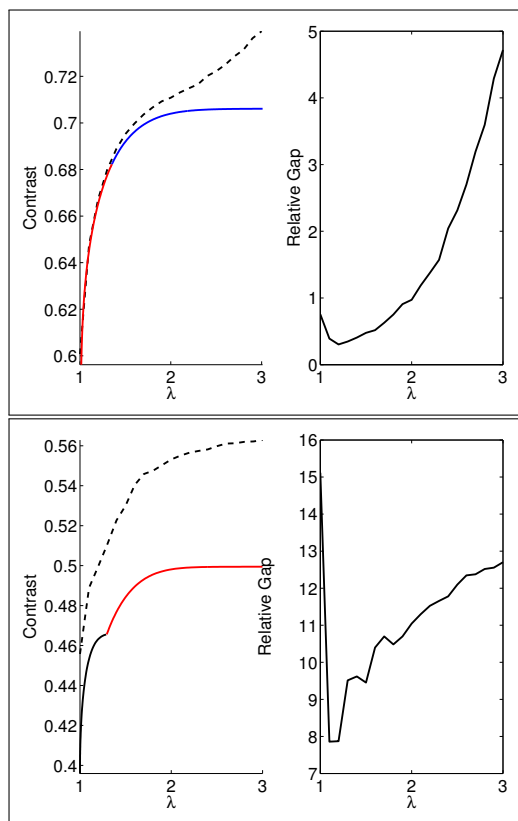


Fig. 13 Step 6: LMI. Best upper bounds (dotted line) by the 1mi method compared with best solutions by HamPath (straight), and relative gap between the two, for **fluid case** on top subgraph and **blood case** on bottom subgraph.

4 Open problems

4.1 The bi-input case in the contrast problem by saturation

We present here some preliminary results on the bi-input problem in the fluid case, with the direct method `Bocop`. We use the same constant initialization for the state variables, and for the control variables u_x and u_y we test the constant initializations -0.5 , -0.1 , 0.1 and 0.5 . We recall that the control must satisfy the constraint $|u| \leq 1$ at all times. We use the same regularisation as in the mono-input case, namely adding a term $\varepsilon \int_0^{t_f} |u(t)|^2 dt$ to the cost function. The discretization is the 2nd order implicit midpoint with 500 to 1000 time steps.

Unlike the many local solutions we found for the mono-input problem (cf Table. 1), here the first batch of optimizations seems to reveal only one branch of solutions, with a 2BS structure. We present in more details the solution for $t_f = 2T_{\min}$, which gives a contrast of 0.7053. The control and the trajectories of the two spins are drawn on Fig. 14. We observe that during the first BS sequence, both spins stay in the same plane, and the phase of the control stays constant as well. Then during the second bang arc, the phase of the control changes and the spins move into separate planes, before rejoining again at the end of the bang arc. Finally, the second singular arc has again a constant phase for the control, with both spins staying in a plane until the final time. Figs. 15 and 16 show the phase of the control and spins, with the norm of the control plotted to indicate the 2BS structure.

Classification of the singular arcs. On this solution, the singular arcs correspond to the Σ_2'' case from Th.1. We numerically check that $x_1 y_2 - y_1 x_2 = 0$ over the two singular arcs, meaning that both spins remain in the same plane. We also check that the phase of the control is constant at these times, and is orthogonal to the plane of the spins, which indeed leads to $\dot{\theta} = 0$ when expressing the dynamics in spherical coordinates (see 1.7.2). The singular arcs in this bi-input solution are actually similar to the singular arcs in the mono-input case. Indeed, if we observe closely the spin trajectories, we find that this bi-input solution is similar to the mono-input solution 20a from Fig. 3. The contrast values confirm this similarity, with 0.7050 for the mono-input and 0.7053 for the bi-input.

When applied to the bi-entry problem, only formulation (LP) is available for the moment/LMI approach, as the quadratic constraint on the controls prevents the use of formulation (LP'). In addition to the increase in the state and control space sizes, this makes only lower relaxations order available for the bi-entry case. In practice, the method is limited to the third relaxation order, for which the upper bounds are essentially identical to those of the mono-entry problem, in both the blood and fluid case. This strongly limits the possible improvements of controlling the problem with two inputs, if any at all.

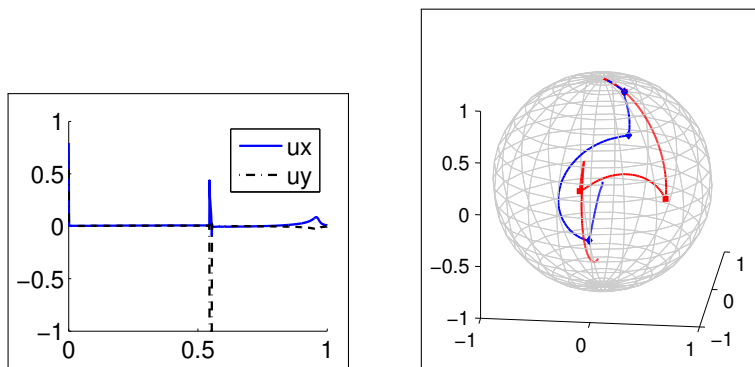


Fig. 14 Bi-input case: Controls u_x and u_y for the 2BS bi-input solution for $t_f = 2T_{\min}$ on the left subgraph. On the right subgraph, trajectories for both spins on the Bloch sphere for the 2BS bi-input solution for $t_f = 2T_{\min}$. The three switching times between bang and singular arcs are indicated by blue diamonds for the first spin and red squares for the second spin. Note that the first square and diamond overlap on the graph.

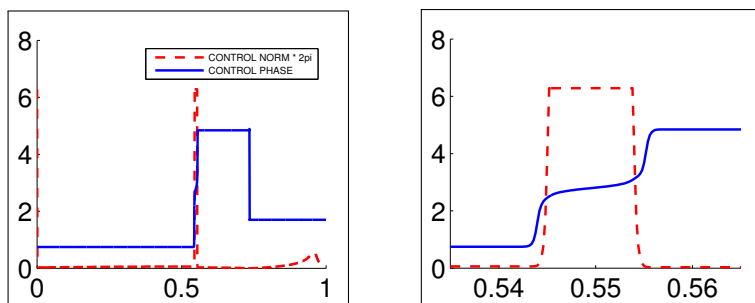


Fig. 15 Bi-input case: Control phase and norm for the 2BS bi-input solution for $t_f = 2T_{\min}$. The control phase is constant on the first BS sequence, then varies during the second bang arc (see zoom on the right subgraph). The control phase is piecewise constant on the second singular arc, with a jump of π when the control crosses 0, from northwest to southeast quadrant.

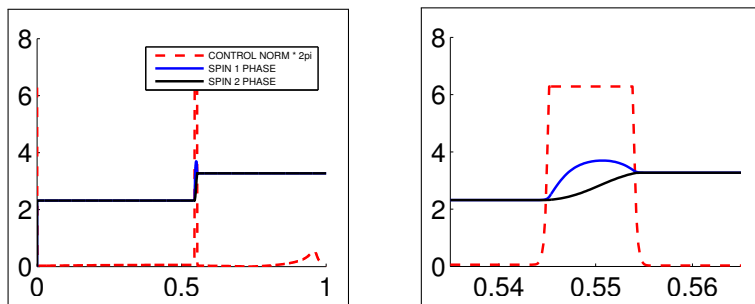


Fig. 16 Bi-input case: Spins phase for the 2BS bi-input solution for $t_f = 2T_{\min}$. Both spins phase are constant and equal on the first BS sequence, then drift away from each other during the second bang arc, before meeting again at the end of the bang arc (see zoom on the right subgraph). Both spins phase remain constant and equal during the second singular arc until the final time.

4.2 Application to the homogeneity problem in Magnetic Resonance Imaging

In our study, we have restricted the analysis to the maximum achievable contrast by saturation for a single voxel of the image but in MRI, the quality of the contrast is affected by B_0 and B_1 (Rf-field) inhomogeneity so that the spins in the sample in different spatial positions experience different magnetic fields.

This is clear from Bloch equation written in the fixed laboratory frame as:

$$\frac{dM}{dt} = \gamma M \wedge B - R(M)$$

where M is the magnetization vector, γ is the gyromagnetic ratio, B is the magnetic field which decomposes into $B_0 + B_1(t)$ where B_0 is the strong magnetic polarizing field in the z-direction and $B_1(t) = (B_x(t), B_y(t))$ is the applied Rf-field in the orthogonal direction, while $R(M)$ is the dissipation of the form:

$$\left(\frac{M_x}{T_2}, \frac{M_y}{T_2}, \frac{(M_z - M_0)}{T_1} \right),$$

due to the relaxation parameters.

denoting $\omega_0 = -\gamma B_0$, $u(t) = -\gamma B_y(t)$, $v(t) = -\gamma B_x(t)$, and normalizing M to $q = (x, y, z) = (M_x, M_y, M_z)/M_0$, the Bloch equation takes the form:

$$\frac{dq}{dt} = Aq - R(q),$$

with:

$$A = \begin{bmatrix} 0 & -\omega_0 & u \\ \omega_0 & 0 & -v \\ -u & v & 0 \end{bmatrix}, \quad R(q) = \begin{bmatrix} x/T_2 \\ y/T_2 \\ (z-1)/T_1 \end{bmatrix}.$$

Expressing (x, y, z) in a moving reference frame:

$$x = x' \cos \omega_0 t - y' \sin \omega_0 t, \quad y = x' \sin \omega_0 t + y' \cos \omega_0 t, \quad z = z',$$

while the control Rf-field is written in the resonant form:

$$u = u_1 \cos \omega_0 t + v_1 \sin \omega_0 t, \quad v = -u_1 \sin \omega_0 t + v_1 \cos \omega_0 t,$$

the Bloch equation becomes:

$$\frac{dq'}{dt} = A'q' - R(q'), \quad A' = \begin{bmatrix} 0 & 0 & u_1 \\ 0 & 0 & -v_1 \\ -u_1 & v_1 & 0 \end{bmatrix}.$$

In general, taking into account B_0 and B_1 inhomogeneity, one obtains in MRI, an ensemble of spin systems [30]:

$$\frac{dq'(t, s)}{dt} = A_s q'(t, s) - R(q'(t, s)), \quad A_s = \begin{bmatrix} 0 & -\omega_s & \varepsilon_s u_1 \\ \omega_s & 0 & -\varepsilon_s v_1 \\ -\varepsilon_s u_1 & \varepsilon_s v_1 & 0 \end{bmatrix},$$

where $\omega_s \in [-B, B]$ represents the resonance offset due to B_0 inhomogeneity and ε_s represents the Rf-inhomogeneity and both are determined experimentally according to spatial position of the spin in the sample.

In particular, in the contrast problem, each vortex corresponds to one of the two spins with different relaxation parameters $\Lambda_i = (1/T_1^i, 1/T_2^i)$, $i = 1, 2$. For a simple vortex, one has $\omega_s = 0$ while ε_s can be normalized to 1, and the maximum achievable contrast by saturation in a given transfer time t_f can be numerically computed by the methods presented in this article, direct method (Bocop) vs indirect method (HamPath) or both.

A second step in the analysis is to use a combination of both techniques to improve the homogeneity quality of the image versus the maximum contrast. This leads to introduce an additional optimization problem concerning the ensemble of spin systems:

$$\min |q'(t_f, s) - q'_d(t_f, s)|$$

where $|\cdot|$ represents an adequate norm distance between the response of the system and the desired contrast. For instance, considering the single-input case and two voxels, one can take $q'_d(t, s) = (0, c(t_f))$ where $c(t_f)$ is the minimum of the two contrast by saturation of the voxels.

5 Conclusion

In this paper, we investigate several methods in optimal control to tackle successfully the contrast problem by saturation in nuclear magnetic resonance.

First of all, the application of geometric control techniques allows for an in-depth classification of the structures of the many local optima. As a result, the solutions in the single input are identified to be concatenations of bang-singular arcs. Those solutions are also valid for the bi-entry case, although additional structures, which we partly characterize, also satisfy first order conditions. The fine characterization of the candidate solutions is the basis for the first numerical method considered, an indirect approach by multiple shooting implemented through the HamPath software. When combined with homotopy techniques, this allows finding a family of solutions in function of the problems relaxation time.

The second numerical method used in the paper is a direct approach implemented by the Bocop software. Several initializations are proposed, as they often lead to different locally optimal solutions. The method often finds quality solutions, in a more straightforward way than the indirect method. In addition, those solutions provide an interesting alternative to regularization techniques for initializing the indirect multiple shootings, to obtain numerical solutions with high accuracy. The candidate trajectories are also continued via homotopy by the indirect method, to identify whole new branches of potential solutions.

The last method considered is a moment optimization technique implemented by the GLOptiPoly toolbox, leading to convex semi-definite relaxations of the optimal control problem in the form of Linear Matrix Inequalities. The lower bounds provided

by the method are compared against the upper bound given by the local synthesis. We report close agreement between those bounds in the single input case, which validates the candidate solutions as globally optimal.

We also present some preliminary simulations on the bi-input case. They seem to indicate little difference with respect to the single input case, both in terms of control structure and objective value. Complete investigation of the bi-input case remains an open problem.

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