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Industrial Application of a Second Order Sliding Mode Observer for Speed and Flux Estimation in Sensorless Induction Motor

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1. Introduction

Recently, considerable research efforts are focused on the sensorless Induction Motors (*IM*) control problem. We refer the reader to Holtz (2006) for a tutorial account on the topic. Indeed, industries concerned by sensorless *IM* drives are continuously seeking for cost reductions in their products. The main drawback of *IM* is the mechanical sensor. The use of such direct speed sensor induces additional electronics, extra wiring, extra space, frequent maintenance, careful mounting and default probability. Moreover, the sensor is vulnerable for electromagnetic noise in hostile environments and has a limited temperature range.

To avoid mechanical sensor (speed, position and load torque) of *IM*, several approaches for the so-called "sensorless control" have attracted a great deal of attention recently (see for example Schauder (1992), Kubota et al. (1993), Vas (1998), Leppänen (2003), Hilaiet et al. (2009), Khalil et al. (2009), Dib et al. (2011), Ghanes & Zheng (2009), Aurora & Ferrara (2007), Ghanes et al. (2010), Maiti et al. (2012)). These methods can be classified into three main strategies.

- Artificial intelligence strategies Vas (1998), Maiti et al. (2012).
- Strategies based on *IM* spatial saliency methods with fundamental excitation and high frequency signal injection Leppänen (2003), Holtz (2006).
- Fundamental motor model strategies: adaptive observer Schauder (1992), Luenberger observe Kubota et al. (1993), Kalman filter observer Hilaiet et al. (2009), high gain observer Khalil et al. (2009), Dib et al. (2011), sliding mode observer Ghanes & Zheng (2009), Aurora & Ferrara (2007), interconnected high gain observer Ghanes et al. (2010).

This chapter belongs to the third strategy using mainly observer methods.

First and second strategies have been a subject of growing interest in recent years. For example the second strategy based on *IM* spatial saliency with extra converters is a robust and physical method. But artificial intelligence and spatial saliency algorithms are quite heavy for basic microprocessors.

The third strategy that is a powerful observer that can estimate simultaneously variables and parameters of a large class of nonlinear systems doesn't require a very high performance processor for real time implementation but they are often tested at high speed in sensorless *IM* whereas the main difficulties are mainly at very low frequencies Ghanes & Zheng (2009), Ghanes et al. (2010).

However for our best of knowledge, examination of the literature on the third strategy shows that the real time computation constraints with a cheapest microprocessors or microprocessors not specially allowed to this task¹ are not taken into account to deal with industrial applications of sensorless *IM* including very low frequencies drives.

Meanwhile, compared with other observers, sliding mode technic Perruquetti & Barbot (2002) have attractive advantages of robustness against matching disturbances and, insensitivity to some specific variation of parameters in sliding mode behavior. However, the chattering effect (that is inherent to standard first sliding mode technic) is often an obstacle for practical applications. Higher-Order Sliding Modes (see for example Bartolini et al. (1998), Levant (2003) and Davila et al. (2005)) are one of the solutions which does not compromise robustness and avoid filtering of estimated variables as considered by other methods.

In this chapter, a second order sliding mode observer for the *IM* without mechanical sensor is presented for the open problem of sensorless *IM* drives at very low frequency. This observer converges in finite time and is robust to the variation of parameters. To illustrate the proposed observer, firstly a very simple case is presented in order to exemplified the tuning parameters. Then, to highlight the technological interest of the proposed method and also show the difficulties due to real time computation constraints when a basic microprocessors are used, an industrial application is proposed.

This paper is organized as follows: the section 2 recalls both *IM* model and unobservability phenomena of *IM*. In section 3 the super twisting algorithm (second sliding mode observer) is first presented in a simple case and then applied for sensorless *IM*. After that the section 4 proposes a discrete version of the super twisting observer. In section 5 the experimental results of the proposed observer carried out in an industrial framework are presented. Some conclusions and remarks are drawn in section VII.

2. Technical background

2.1 *IM* model

In Chiasson (2005) the following *IM* model is proposed, in the fixed (α, β) frame:

$$\begin{cases} \dot{i}_{s\alpha} &= -\frac{R_s L_r^2 + R_r M_{sr}^2}{\sigma L_s L_r^2} i_{s\alpha} + \frac{M_{sr}}{\sigma L_s L_r} \left(\frac{R_r}{L_r} \phi_{r\alpha} + p \Omega \phi_{r\beta} \right) + \frac{1}{\sigma L_s} v_{s\alpha} \\ \dot{i}_{s\beta} &= -\frac{R_s L_r^2 + R_r M_{sr}^2}{\sigma L_s L_r^2} i_{s\beta} + \frac{M_{sr}}{\sigma L_s L_r} \left(\frac{R_r}{L_r} \phi_{r\beta} - p \Omega \phi_{r\alpha} \right) + \frac{1}{\sigma L_s} v_{s\beta} \\ \dot{\phi}_{r\alpha} &= \frac{M_{sr} R_r}{L_r} i_{s\alpha} - \frac{R_r}{L_r} \phi_{r\alpha} - p \Omega \phi_{r\beta} \\ \dot{\phi}_{r\beta} &= \frac{M_{sr} R_r}{L_r} i_{s\beta} - \frac{R_r}{L_r} \phi_{r\beta} + p \Omega \phi_{r\alpha} \\ \dot{\Omega} &= \frac{p M_{sr}}{J L_r} (\phi_{r\alpha} i_{s\beta} - \phi_{r\beta} i_{s\alpha}) - \frac{f}{J} \Omega - \frac{1}{J} T_l \end{cases} \quad (1)$$

As the mechanical position and magnetic variables are unknown, $d - q$ frame is well appropriate for sensorless observer based control design.

***IM* parameters:**

- R_s : Stator resistance (*Ohms*).
- R_r : Rotor resistance (*Ohms*).

¹ The microprocessors may be dedicated to many process tasks as supervision process, communication process in addition to the considered task

- L_S : Stator inductance (*Ohms*).
- L_R : Rotor inductance (*H*).
- L_M : Mutual inductance (*H*).
- p : number of pole pairs.
- f : viscous friction coefficient (*Nm.s/rad*).
- J : inertia (*Kg.m²*).

IM variables :

- $v_{s\alpha,\beta}$: Stator voltage (*V*).
- $i_{s\alpha,\beta}$: Stator current (*A*).
- $\phi_{r\alpha,\beta}$: Rotor flux (*Wb*).
- Ω : Mechanical speed (*rad/s*).
- T_l : Load torque (*Nm*).

In order to construct the proposed observer for an industrial application, we work with a per unit model, under the following equations :

$$\begin{cases} \dot{x}_1 = -\gamma x_1 + \theta (b x_3 + c x_5 x_4) + \xi v_1 \\ \dot{x}_2 = -\gamma x_2 + \theta (b x_4 - c x_5 x_3) + \xi v_2 \\ \dot{x}_3 = a x_1 - b x_3 - c x_5 x_4 \\ \dot{x}_4 = a x_2 - b x_4 + c x_5 x_3 \\ \dot{x}_5 = h (x_3 x_2 - x_4 x_1) - d x_5 - e T_l \end{cases} \quad (2)$$

With the following parameters:

$$\begin{aligned} x_1 &= \frac{i_{s\alpha}}{I_{ref}} & x_2 &= \frac{i_{s\beta}}{I_{ref}} & x_3 &= \frac{\omega_{ref} \phi_{r\alpha}}{V_{ref}} & x_4 &= \frac{\omega_{ref} \phi_{r\beta}}{V_{ref}} & x_5 &= \frac{p \Omega}{\omega_{ref}} \\ a &= \frac{M_{sr} I_{ref} \omega_{ref}}{T_r V_{ref}} & b &= \frac{1}{\tau_r} & c &= \omega_{ref} & d &= \frac{f \bar{v}}{J} \\ e &= \frac{p}{J \omega_{ref}} & h &= \frac{p^2 M_{sr} I_{ref} V_{ref}}{J \omega_{ref}^2 L_r} & \theta &= \frac{K V_{ref}}{I_{ref} \omega_{ref}} & \xi &= \frac{V_{ref}}{\sigma L_s I_{ref}} \\ \sigma &= 1 - \frac{M_{sr}^2}{L_s L_r} & \gamma &= \frac{R_s L_r^2 + R_r M_{sr}^2}{\sigma L_s L_r^2} & \tau_r &= \frac{L_r}{R_r} & K &= \frac{M_{sr}}{\sigma L_s L_r} \end{aligned}$$

Thus for the sake of homogeneity, hereafter experimental results will be given in per-unit (p.u.).

2.2 Observability

The IM observability has been studied by several authors (see for example Canudas De Wit et al. (2000), Ibarra-Rojas et al. (2004), Ghanes et al. (2006)). In Ghanes et al. (2006), it is proved that the IM observability cannot be established in the particular case when fluxes $\Phi_{r\alpha}$, $\Phi_{r\beta}$ and speed Ω are constant, even if we use the higher derivatives of currents. This is a sufficient and necessary condition for loss of observability.

This operating case match to the following physically interpretation:

Constant fluxes ($\dot{\phi}_{r\alpha} = \dot{\phi}_{r\beta} = 0$)

With ω_s the stator voltage pulsation and T_{em} the electromagnetic torque.

$$\omega_s = p\Omega + \frac{R_r T_{em}}{p\Phi_{rd}^2} = 0 \quad (3)$$

where $\Phi_{rd}^2 = \phi_{r\alpha}^2 + \phi_{r\beta}^2$ is the square of the direct flux in (d, q) frame.

Constant speed ($\dot{\Omega} = 0$)

$$T_{em} = f\Omega + T_l \quad (4)$$

Thanks to previous equations, we obtain:

$$T_l = - \left(f + \frac{p^2 \Phi_{rd}^2}{R_r} \right) \Omega \quad (5)$$

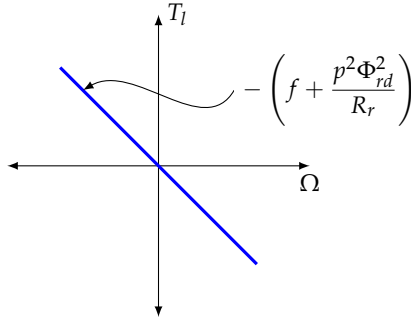


Fig. 1. Inobservability curve

The unobservability curve in the map (T_l, Ω) is shown in figure (1).

Obviously, the observability is lost gradually when we approach this curve Ghanes et al. (2006).

3. Second order sliding mode observer

3.1 Super twisting algorithm: An academic example

Sliding modes were used at first, as a control technique, but in the recent years it presented as a very good tool for observer design Levant (1998), Levant (1998), Davila et al. (2005).

Considering the following system:

$$\begin{cases} \dot{x}_1 = x_2 \\ \dot{x}_2 = f(x, t) \\ y = h(x) = x_1 \end{cases} \quad (6)$$

With $f(x, t)$ a bounded function.

For system (6), a second order sliding mode observer is designed in the following way:

$$\begin{cases} \dot{\hat{x}}_1 = \hat{x}_2 + \lambda |e_1|^{\frac{1}{2}} \text{sign}(e_1) \\ \dot{\hat{x}}_2 = a \text{sign}(e_1) \end{cases} \quad (7)$$

With $\lambda, \alpha > 0$ and $e_1 = x_1 - \hat{x}_1$.

The efficiency of this strategy depends on coefficients α and λ . For second order system (6) we show convergence of estimated variables (\hat{x}_1, \hat{x}_2) to (x_1, x_2) by studying dynamics errors \dot{e}_1 and \dot{e}_2 .

Thus

$$\begin{cases} \dot{e}_1 = \dot{x}_1 - \dot{\hat{x}}_1 = e_2 - \lambda|x_1 - \hat{x}_1|^{\frac{1}{2}}\text{sign}(x_1 - \hat{x}_1) \\ \dot{e}_2 = \dot{x}_2 - \dot{\hat{x}}_2 = f(x, t) - \alpha\text{sign}(x_1 - \hat{x}_1) \end{cases} \quad (8)$$

With

$$f(x, t) \in [-f^+, f^+], \quad e_2 = x_2 - \hat{x}_2$$

And

$$\ddot{e}_1 = f(x, t) - \alpha\text{sign}(e_1) - \frac{1}{2}\lambda|e_1|^{-\frac{1}{2}}\dot{e}_1$$

Thus

$$\ddot{e}_1 \in [-f^+, f^+] - \alpha\text{sign}(e_1) - \frac{1}{2}\lambda|e_1|^{-\frac{1}{2}}\dot{e}_1$$

Where

$$f^+ = \max\{|f(x, t)|\}$$

Conditions on λ and α that permit a convergence in finite time of (\dot{e}_1, e_1) to $(0, 0)$ are derived hereafter according to figure 2.

Proposition: For any initial conditions $x(0), \hat{x}(0)$, there exists a choice of λ and α such that the error dynamics \dot{e}_1 and \dot{e}_2 converge to zero in finite time and by consequence $\hat{x}_1 \mapsto x_1$ and $\hat{x}_2 \mapsto x_2$.

Proof: Consider system (6). To show the convergence of (\hat{x}_1, \hat{x}_2) to (x_1, x_2) (ie., $(e_1, e_2) \rightarrow (0, 0)$), we need to show that

$$\frac{|\dot{e}_1(T_2)|}{|\dot{e}_1(0)|} < 1 \quad (9)$$

of figure 2, where $\dot{e}_1(T_2) = C$ and $\dot{e}_1(0) = A$.

Figure 2 illustrates the finite time convergence behavior of the proposed observer for system 6. In what follows we will give the error trajectory for each quadrant in the worst cases.

Let consider the system's dynamic \ddot{e}_1

$$\ddot{e}_1 = f(x, t) - \alpha\text{sign}(e_1) - \frac{\lambda}{2}|e_1|^{-\frac{1}{2}}\dot{e}_1 \quad (10)$$

with $\frac{d|x|}{dt} = \dot{x}\text{sign}(x)$.

Equation (10) leads to

$$\ddot{e}_1 \in [-f^+, f^+] - \alpha\text{sign}(e_1) - \frac{\lambda}{2}|e_1|^{-\frac{1}{2}}\dot{e}_1 \quad (11)$$

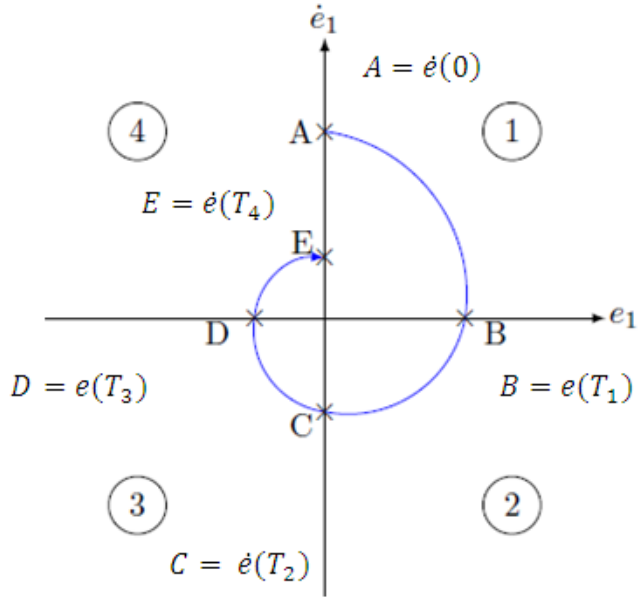


Fig. 2. Upper bound of finite time convergence curve.

where

$$f^+ = \max(|f(t, x)|),$$

First quadrant: $e_1 > 0$ and $\dot{e}_1 > 0$

Starting from point A of figure 2 the trajectory of $\dot{e}_1 = f(e_1)$ is in the first quadrant $e_1 \geq 0$ and $\dot{e}_1 \geq 0$. The rising trajectory is given by $\ddot{e}_1 = -(\alpha - f^+)$.

By choosing

$$\alpha > f^+ \quad (12)$$

we ensure that $\ddot{e}_1 < 0$ and hence \dot{e}_1 decreases and tends towards the y-axis, corresponding to $\dot{e}_1 = 0$ (point B in figure 2).

Computing of $e_1(T_1)$

From (10), we have

$$\ddot{e}_1 = -(\alpha - f^+)$$

Which implies that

$$\dot{e}_1(t) = -(\alpha - f^+)t + \dot{e}_1(0) \quad (13)$$

And

$$e_1(t) = -(\alpha - f^+) \frac{t^2}{2} + \dot{e}_1(0)t$$

From (13), since $\dot{e}_1(T_1) = 0$, we obtain the necessary time for going from A to B with $B = e_1(T_1)$.

$$T_1 = \frac{\dot{e}_1(0)}{(\alpha - f^+)} \quad (14)$$

Then we can compute $e(T_1)$ as follows

$$\begin{aligned} e_1(T_1) &= -(\alpha - f^+) \frac{\dot{e}_1^2(0)}{2(\alpha - f^+)} + \frac{\ddot{e}_1^2(0)}{(\alpha - f^+)} \\ &= \frac{\dot{e}_1^2(0)}{2(\alpha - f^+)} \end{aligned} \quad (15)$$

Second quadrant: $e_1 > 0$ and $\dot{e}_1 < 0$

In this case, $\ddot{e}_1 = -f^+ - \text{asign}(e_1) - \frac{\lambda}{2}|e_1|^{-\frac{1}{2}}\dot{e}_1$

becomes negative ($\ddot{e}_1 < 0$) on making a good choice of α which leads to

$$(\alpha + f_1^+) > -\frac{\lambda_1}{2}|e_1|^{-\frac{1}{2}}\dot{e}_1 \quad (16)$$

Since \dot{e}_1 is negative, then

$$|\dot{e}_1(t)| \leq \frac{2(\alpha + f_1^+)}{\lambda} |e_1(t)|^{\frac{1}{2}} \quad (17)$$

Considering by the sake of simplicity (17), $e_1 > 0$ and $\dot{e}_1 < 0$.

Integrating (17) with $e_1(0) = 0$ gives

$$\sqrt{e_1(t)} = \frac{(\alpha + f^+)}{\lambda} t \quad (18)$$

At $t = T_2$, we should make the inverse of function (18) from point B to C in figure 2. This leads to

$$e_1(T_2) = e_1(T_1). \quad (19)$$

Then (18) becomes

$$\sqrt{e_1(T_1)} = \frac{(\alpha + f^+)}{\lambda} T_2 \quad (20)$$

By replacing $e_1(T_1)$ coming from (15) in equation (20), we get the necessary time for going from B to C

$$T_2 = \frac{\lambda}{(\alpha + f^+)} \frac{\dot{e}_1(0)}{\sqrt{2}(\alpha - f^+)} \quad (21)$$

After that, by using the argument of (19) in equation (17) evaluated at $t = T_2$ in the worth case, we get

$$|\dot{e}_1(T_2)| = \frac{2(\alpha + f_1^+)}{\lambda} |e_1(T_1)|^{\frac{1}{2}} \quad (22)$$

By replacing $e_1(T_1)$ by its expression given by (15) in (22), we get

$$|\dot{e}_1(T_2)| = \frac{2(\alpha + f_1^+)}{\lambda} \frac{|\dot{e}_1(0)|}{\sqrt{2}\sqrt{(\alpha - f^+)}} \quad (23)$$

Thus, by satisfying inequality (9) in equation (23) λ should be chosen as

$$\lambda > (\alpha + f_1^+) \sqrt{\frac{2}{(\alpha - f^+)}} \quad (24)$$

Finally, conditions (12) and (24) of the observer parameters are sufficient conditions guaranteeing the state convergence (i.e. the states (e_1, \dot{e}_1) tend towards $e_1 = \dot{e}_1 = 0$ (Figure 2).

This ends the proof.

Moreover the convergence is in finite time, because from (14) and 21 we obtain

$$T_\infty \leq \left(\sum_{i=0}^{+\infty} \left(\frac{\sqrt{2}(\alpha + f^+)}{\lambda\sqrt{\alpha - f^+}} \right)^i \right) \left(\frac{\lambda}{\sqrt{2}(\alpha + f^+)} + 1 \right) \frac{\dot{e}_1(0)}{(\alpha - f^+)}$$

as

$$\left| \frac{\sqrt{2}(\alpha + f^+)}{\lambda\sqrt{\alpha - f^+}} \right| < 1$$

we obtain a bounded limit

$$T_\infty \leq \left(\frac{1}{1 - \frac{\sqrt{2}(\alpha + f^+)}{\lambda\sqrt{\alpha - f^+}}} \right) \left(\frac{\lambda}{\sqrt{2}(\alpha + f^+)} + 1 \right) \frac{\dot{e}_1(0)}{(\alpha - f^+)}$$

Here we give simulations of a very simple example. The function $f(t, x)$ in system (6) is set equal to $\sin(t)$ with $f^+ = \max\{\sin(t)\} = 1$. We get

$$\begin{cases} \dot{x}_1 &= x_2 \\ \dot{x}_2 &= \sin(t) \\ y &= x_1 \end{cases} \quad (25)$$

The associated observer is:

$$\begin{cases} \dot{\hat{x}}_1 &= \hat{x}_2 + \lambda |e_1|^{\frac{1}{2}} \text{sign}(e_1) \\ \dot{\hat{x}}_2 &= \alpha \text{sign}(e_1) \end{cases} \quad (26)$$

The simulation results are shown in figure 3. It can be seen that figure (3) spotlight *two* steps into Super Twisting Algorithm, which are convergence step in finite time, and sliding mode. Indeed observer is working on $t = 1$ s with $\hat{x}_1(0) = 1$ and $\hat{x}_2(0) = 1$. \hat{x}_1 converges under 1s to x_1 , and then slides along x_1 path, and equal to \tilde{x}_2 .

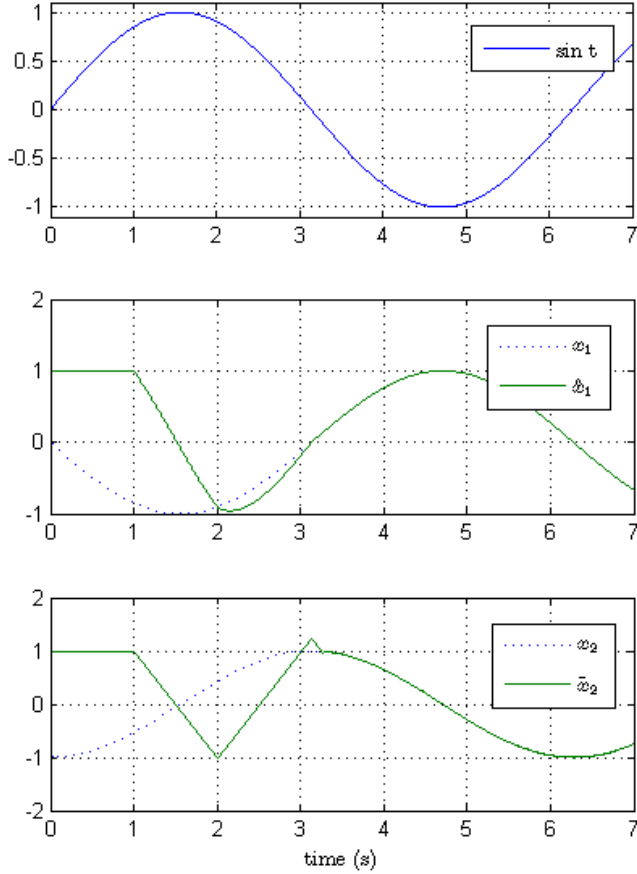


Fig. 3. Super Twisting Algorithm example.

3.2 Application to *Induction Motor*

At first, due to the nonlinearity of flux and speed product, the *IM* model (2) is not written in a suitable form allowing to apply the super twisting algorithm presented in previous section. To overcome this difficulty, we make the following change of variables in order to rewrite the *IM* model (2) (without \dot{x}_5 equation) into a form 6:

$$\left\{ \begin{array}{l} z_1 = x_1 \\ z_2 = x_2 \\ z_3 = b x_3 + c x_5 x_4 \\ z_4 = b x_4 - c x_5 x_3 \\ z_5 = \dot{z}_3 \\ z_6 = \dot{z}_4 \end{array} \right. \quad (27)$$

Equation 27 is not a diffeomorphism, not an homeomorphism but only an immersion, because the dimension of x is 5 and the dimension of z is 6. Nevertheless, this immersion is used in order to avoid some singularities in a speed estimation as this will be pointed out in the next. From the IM model (2) and (27), we obtain a new dynamical system as following:

$$\begin{cases} \dot{z}_1 = -z_1 + \theta z_3 + \zeta v_1 \\ \dot{z}_2 = -\gamma z_2 + \theta z_4 + \zeta v_2 \\ \dot{z}_3 = z_5 \\ \dot{z}_4 = z_6 \end{cases} \quad (28)$$

Thus, we can propose a new observer structure for dynamical system (28):

$$\begin{cases} \dot{\hat{z}}_1 = \theta \tilde{z}_3 - \gamma z_1 + \zeta v_1 + \lambda_1 |e_1|^{\frac{1}{2}} \text{sign}(e_1) \\ \dot{\hat{z}}_3 = \alpha_1 \text{sign}(e_1) \\ \dot{\hat{z}}_2 = \theta \tilde{z}_4 - \gamma z_2 + \zeta v_2 + \lambda_2 |e_2|^{\frac{1}{2}} \text{sign}(e_2) \\ \dot{\hat{z}}_4 = \alpha_2 \text{sign}(e_2) \\ \dot{\hat{z}}_3 = E_1 E_2 (\tilde{z}_5 + \lambda_3 |e_3|^{\frac{1}{2}} \text{sign}(e_3)) \\ \dot{\hat{z}}_5 = E_1 E_2 \alpha_3 \text{sign}(e_3) \\ \dot{\hat{z}}_4 = E_1 E_2 (\tilde{z}_6 + \lambda_4 |e_4|^{\frac{1}{2}} \text{sign}(e_4)) \\ \dot{\hat{z}}_6 = E_1 E_2 \alpha_4 \text{sign}(e_4) \end{cases} \quad (29)$$

$$\text{with } E_i \begin{cases} 1 \text{ if } e_i = z_i - \hat{z}_i = 0, i = 1, 2 \\ 0 \text{ if not} \end{cases} \quad (30)$$

This observer structure depends on Super Twisting Algorithm presented in previous section and Step by Step proficiencies Floquet & Barbot (2007). We propose to put in multiples-series observers with functions (E_i).

The functions E_i ensure that the next steps errors do not escape too far before one has the convergent of the last step error.

The gains α_i, λ_i are chosen which respect to the reachability condition of the Super Twisting algorithm as stated in inequalities (12) and (24) of previous section. By choosing

$$\alpha_1 > \max(|\theta z_3|), \quad \lambda_1 > (\max(|\theta z_3|) + \alpha_1) \sqrt{\frac{2}{\alpha_1 - \max(|\theta z_3|)}} \quad (31)$$

$$\alpha_2 > \max(|\theta z_4|), \quad \lambda_2 > (\max(|\theta z_4|) + \alpha_2) \sqrt{\frac{2}{\alpha_2 - \max(|\theta z_4|)}} \quad (32)$$

$$\alpha_3 > \max(|z_5|), \quad \lambda_3 > (\max(|z_5|) + \alpha_3) \sqrt{\frac{2}{\alpha_3 - \max(|z_5|)}} \quad (33)$$

$$\alpha_4 > \max(|z_6|), \quad \lambda_4 > (\max(|z_6|) + \alpha_4) \sqrt{\frac{2}{\alpha_4 - \max(|z_6|)}} \quad (34)$$

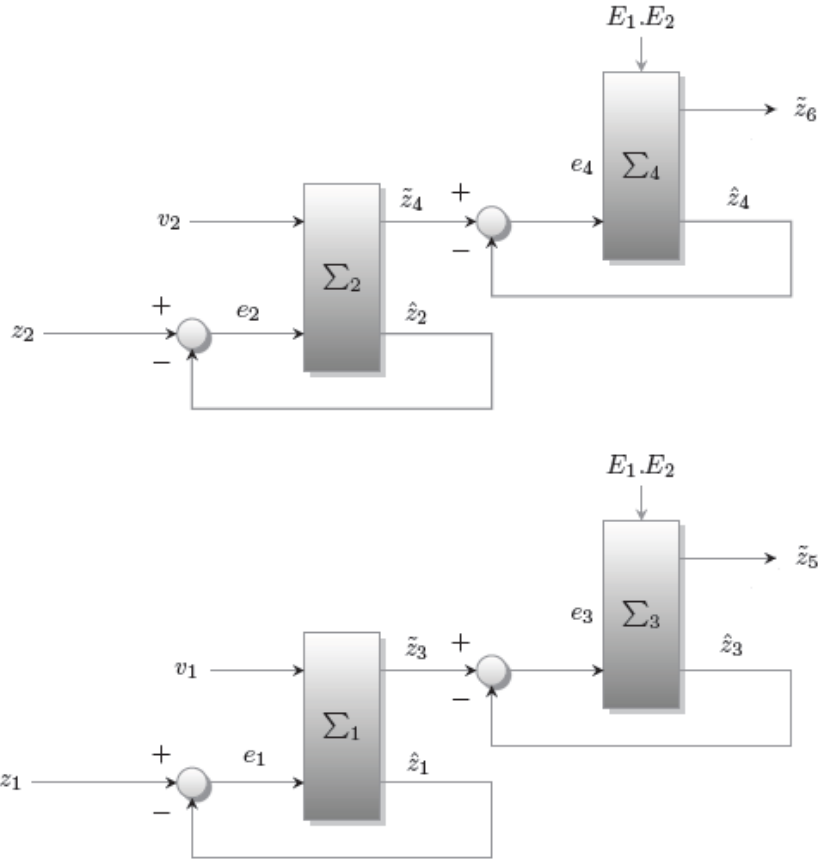


Fig. 4. General *IM* Observer Structure.

and we get

$$e_1 = e_2 = e_3 = e_4 = 0$$

i.e.

$$\begin{aligned} \hat{z}_1 &= z_1, & \hat{z}_2 &= z_2 \\ \hat{z}_3 &= \tilde{z}_3, & \hat{z}_4 &= \tilde{z}_4 \\ \tilde{z}_5 &= z_5, & \tilde{z}_6 &= z_6 \end{aligned}$$

Consequently all variables $z_1, z_2, \hat{z}_3, \hat{z}_4, \tilde{z}_5, \tilde{z}_6$ are available and then we can deduce *IM* variables.

We propose to treat this problem in two different cases: $\dot{x}_5 \neq 0$, and $\dot{x}_5 = 0$

CASE A : $\dot{x}_5 \neq 0$

Firstly we propose to express fluxes x_3 and x_4 , from equation (27) we obtain:

$$\begin{aligned}\hat{z}_3 &= bx_3 + cx_5x_4 \\ \hat{z}_4 &= bx_4 - cx_5x_3\end{aligned}$$

We deduce

$$x_3 = \frac{\hat{z}_3 - cx_5x_4}{b} \quad (35)$$

$$x_4 = \frac{\hat{z}_4 + cx_5x_3}{b} \quad (36)$$

By substituting x_4 by its expression in (35) and x_3 in (36) we have:

$$\begin{aligned}x_3 &= \frac{\hat{z}_4 + \frac{c}{b} z_3 x_5}{b + \frac{c^2 x_5^2}{b}} \\ x_4 &= \frac{\hat{z}_3 - \frac{c}{b} z_4 x_5}{b + \frac{c^2 x_5^2}{b}}\end{aligned} \quad (37)$$

Now let us express x_5 . From (2) we know

$$\begin{aligned}\dot{x}_3 &= ax_1 - bx_3 - cx_5x_4 \\ \dot{x}_4 &= ax_2 - bx_4 + cx_5x_3\end{aligned} \quad (38)$$

Firstly we propose to write \dot{x}_3 and \dot{x}_4 as a function of variables z . By using (27) in (38), we get:

$$\begin{aligned}\dot{x}_3 &= az_1 - \hat{z}_3 \\ \dot{x}_4 &= az_2 - \hat{z}_4\end{aligned} \quad (39)$$

By Replacing (39) in (38) and using the two first equations in (27), it follows

$$\hat{z}_3 = bx_3 + cx_5x_4 \quad (40)$$

$$\hat{z}_4 = bx_4 - cx_5x_3 \quad (41)$$

Taking the time derivative of (41) and using third-fourth equations in (27) yields to

$$\dot{z}_3 = \dot{\tilde{z}}_5 = b\dot{x}_3 + c\dot{x}_5x_4 + c\dot{x}_4x_5 \quad (42)$$

$$\dot{z}_4 = \dot{\tilde{z}}_6 = b\dot{x}_4 - c\dot{x}_5x_3 - c\dot{x}_3x_5 \quad (43)$$

From (42) we have:

$$\dot{x}_5 = \frac{\tilde{z}_5 - b\dot{x}_3 - cx_5\dot{x}_4}{cx_4} \quad (44)$$

By substituting (44) in (43), we get

$$\tilde{z}_6 = b\dot{x}_4 - cx_5\dot{x}_3 - x_3 \frac{\tilde{z}_5 - b\dot{x}_3 - cx_5\dot{x}_4}{x_4} \quad (45)$$

Then we can deduce the motor speed x_5 by replacing in (45) expressions of x_3 - x_4 and \dot{x}_3 - \dot{x}_4 coming from (37) and (39), respectively.

After a straightforward computations, we obtain a second order expression of x_5 :

$$\pi_1 x_5^2 + \pi_2 x_5 + \pi_3 = 0 \quad (46)$$

where

$$\begin{aligned} \pi_1 &= \frac{c}{b} [(az_2 - \hat{z}_4)\hat{z}_3 - (az_1 - \hat{z}_3)\hat{z}_4] \\ \pi_2 &= \frac{c}{b} [b(az_1 - \hat{z}_3)\hat{z}_3 - b(az_2 - \hat{z}_4)\hat{z}_4 - \tilde{z}_5\hat{z}_3 + \hat{z}_4\tilde{z}_6] \\ \pi_3 &= \hat{z}_3 [-\tilde{z}_6 + b(az_2 - \hat{z}_4)] - \hat{z}_4 [\tilde{z}_5 - b(az_1 - \hat{z}_3)] \end{aligned}$$

CASE B : $\dot{x}_5 = 0$

We propose this hypothesis because of dynamical gap evolution between electrical and mechanical variables, in fact speed evolves much more slowly than currents or fluxes.

Thus with this hypothesis we simplify (42) and (43), and obtain two expressions of x_5 :

$$x_5 = \frac{\tilde{z}_5 - b\dot{x}_3}{c\dot{x}_4} \quad (47)$$

or

$$x_5 = \frac{b\dot{x}_4 - \tilde{z}_6}{c\dot{x}_3} \quad (48)$$

we change \dot{x}_3 by expression (35) and \dot{x}_4 by expression(36)

$$x_5 = \frac{\tilde{z}_5 - baz_1 + b\hat{z}_3}{caz_2 - c\hat{z}_4} \quad (49)$$

or

$$x_5 = \frac{\tilde{z}_6 + baz_2 - b\hat{z}_4}{caz_1 - c\hat{z}_3} \quad (50)$$

Equations (49) and (50) are true only if :

$$caz_2 - c\hat{z}_4 \neq 0 \text{ for (49) and } caz_1 - c\hat{z}_3 \neq 0 \text{ for (50)}$$

Speed estimation

In order to avoid singularities of speed estimation in (49) and (50), we use the fact that (49) and (50) are in quadrature and thus we get the estimation of speed x_5 as follows :

$$x_5 = \frac{(\tilde{z}_5 - baz_1 + b\hat{z}_3)(caz_2 - c\hat{z}_4) + (\tilde{z}_6 + baz_2 - b\hat{z}_4)(caz_1 - c\hat{z}_3)}{(caz_2 - c\hat{z}_4)^2 + (caz_1 - c\hat{z}_3)^2} \quad (51)$$

Flux estimation

The rotor flux are obtained by replacing the estimation speed (51) in (37)

Flux position estimation

Having the rotor flux estimation (37), we can obtain rotor flux position ρ

$$\rho = atan\left(\frac{x_4}{x_3}\right) \quad (52)$$

4. Discrete time implementation

4.1 Explicit Euler method

For the industrial application in real time, the discrete time observer is designed. The explicit Euler's method is chosen to transform continuous observer to discrete observer. This is due to the simplicity of computation. Considering a differential equation :

$$\dot{x} = f(x)$$

The explicit Euler's method with a sampling time T_e gives:

$$x(k) = x(k-1) + T_e f(x(k-1))$$

the data acquisition period T_e is also the computation period.

Applying the explicit Euler's method for the second order sliding mode observer, the discrete observer is obtained:

$$\left\{ \begin{array}{l} \hat{z}_1(k) = \hat{z}_1(k-1) + T_e \left[\theta \tilde{z}_3(k-1) - \gamma z_1(k-1) + \xi v_1(k-1) \right. \\ \quad \left. + \lambda_1 |e_1(k-1)|^{\frac{1}{2}} \text{sign}(e_1(k-1)) \right] \\ \tilde{z}_3(k) = \tilde{z}_3(k-1) + T_e \alpha_1 \text{sign}(e_1(k-1)) \\ \hat{z}_2(k) = \hat{z}_2(k-1) + T_e \left[\theta \tilde{z}_4(k-1) - \gamma z_2(k-1) + \xi v_2(k-1) \right. \\ \quad \left. + \lambda_2 |e_2(k-1)|^{\frac{1}{2}} \text{sign}(e_2(k-1)) \right] \\ \tilde{z}_4(k) = \tilde{z}_4(k-1) + T_e \alpha_2 \text{sign}(e_2(k-1)) \\ \hat{z}_3(k) = \tilde{z}_3(k-1) + T_e E_1 E_2 \left[\tilde{z}_5(k-1) + \lambda_3 |e_3(k-1)|^{\frac{1}{2}} \text{sign}(e_3(k-1)) \right] \\ \tilde{z}_5(k) = \tilde{z}_5(k-1) + T_e E_1 E_2 \alpha_3 \text{sign}(e_3(k-1)) \\ \hat{z}_4(k) = \tilde{z}_4(k-1) + T_e E_1 E_2 \left[\tilde{z}_6(k-1) + \lambda_4 |e_4(k-1)|^{\frac{1}{2}} \text{sign}(e_4(k-1)) \right] \\ \tilde{z}_6(k) = \tilde{z}_6(k-1) + T_e E_1 E_2 \alpha_4 \text{sign}(e_4(k-1)) \end{array} \right. \quad (53)$$

4.2 Oversampling

To achieve good accuracy, a small sample period and fast DSP are needed. In the industrial application, the DSP clock frequency is only 150MHz, which does not allow a small enough sample period. So in experimentation an over-sample technique is proposed. In the following paragraphs we show that, under a few low restrictive conditions, it is possible to reduce the error of Euler's method, seen in the previous subsection (4.1).

Hereafter we first present the oversampling method in a very simple use, where $f \in C^\infty$. Assume a continuous autonomous system of the form:

$$\dot{x} = f(x); \quad x(t_0) = x_0 \quad (54)$$

Assume in addition that the system is discretized at a sampling time T_e . Then the system ((54)) can be approximated by the explicit Euler's method:

$$x(t_{k+1}) = x(t_k) + T_e \dot{x}(t_k) + O(T_e^2) \quad (55)$$

For small values of T_e , $O(T_e^3)$ is neglected and the truncation error is approximately proportional to T_e^2 .

Suppose now that the system (54) is discretized at two different sample rates resulting in two discrete time systems: H_1 sampled at frequency $f_{s1} = \frac{1}{T_e}$ and H_2 sampled at frequency $f_{s2} = \frac{N}{T_e}$; and let us compare the truncation error of each one after T_e seconds for N large enough. The discrete time is given by $t_{H1} = nT_e$ for H_1 and $t_{H2} = k\frac{T_e}{N}$ for H_2 , with $n, k \in \mathbb{N}$. Assume that the initial times and the initial conditions are the same for both of them, that is: $nT_e = k\frac{T_e}{N} = t_0$ and $x(nT_e) = x\left(k\frac{T_e}{N}\right) = x(t_0) = x_0$. The dynamics of the discrete time system H_1 can be written as:

$$x((n+1)T_e) = x(nT_e) + T_e f(x(nT_e)) + O(T_e^2) \quad (56)$$

H_2 , sampled at $f_{s2} = \frac{N}{T_e}$, evolves as follows:

$$\begin{aligned} x\left(\left(k+1\right)\frac{T_e}{N}\right) &= x\left(k\frac{T_e}{N}\right) + \frac{T_e}{N} f\left(x\left(k\frac{T_e}{N}\right)\right) + O\left(\frac{T_e}{N}\right)^2 \\ x\left(\left(k+2\right)\frac{T_e}{N}\right) &= x\left(\left(k+1\right)\frac{T_e}{N}\right) + \frac{T_e}{N} f\left(x\left(\left(k+1\right)\frac{T_e}{N}\right)\right) + O\left(\frac{T_e}{N}\right)^2 \\ &= x\left(k\frac{T_e}{N}\right) + \frac{T_e}{N} f\left(x\left(k\frac{T_e}{N}\right)\right) \\ &\quad + \frac{T_e}{N} f\left(x\left(k\frac{T_e}{N}\right) + \frac{T_e}{N} f\left(x\left(k\frac{T_e}{N}\right)\right) + O\left(\frac{T_e}{N}\right)^2\right) + 2O\left(\frac{T_e}{N}\right)^2 \end{aligned} \quad (57)$$

For N large enough we can consider the influence of the error term $O\left(\frac{T_e}{N}\right)^2$ over the function $\frac{T_e}{N}f(\cdot)$ as a term in $O\left(\frac{T_e}{N}\right)^3$, then:

$$\begin{aligned} x\left(\left(k+2\right)\frac{T_e}{N}\right) &\approx x\left(k\frac{T_e}{N}\right) + \frac{T_e}{N} f\left(x\left(k\frac{T_e}{N}\right)\right) + \frac{T_e}{N} f\left\{x\left(k\frac{T_e}{N}\right) + \frac{T_e}{N} f\left(x\left(k\frac{T_e}{N}\right)\right)\right\} \\ &\quad + 2O\left(\frac{T_e}{N}\right)^2 \\ &= x\left(k\frac{T_e}{N}\right) + \frac{T_e}{N} f\left(x\left(k\frac{T_e}{N}\right)\right) + \frac{T_e}{N} f\left(x\left(\left(k+1\right)\frac{T_e}{N}\right)\right) + 2O\left(\frac{T_e}{N}\right)^2 \end{aligned} \quad (58)$$

So, in a general way, we have:

$$x\left(\left(k+N\right)\frac{T_e}{N}\right) \approx x\left(k\frac{T_e}{N}\right) + \frac{T_e}{N} \sum_{i=k}^{k+N-1} f\left(x\left(i\frac{T_e}{N}\right)\right) + NO\left(\frac{T_e}{N}\right)^2 \quad (59)$$

As we can see from (56) and (59), the truncation errors of the discrete systems H_1 and H_2 are

$$\varepsilon_1 = O\left(T_e^2\right) \quad (60)$$

and

$$\varepsilon_2 = NO \left(\left(\frac{T_e}{N} \right)^2 \right) \quad (61)$$

The truncation errors ε_1 and ε_2 , given by (60) and (61) respectively give

$$NO \left(\left(\frac{T_e}{N} \right)^2 \right) \approx \frac{O(T_e^2)}{N} \quad (62)$$

$$\varepsilon_2 \approx \frac{\varepsilon_1}{N} \quad (63)$$

Then the oversampled system H_2 reduces the truncation error about N times.

In practice, to achieve the benefits of oversampling, we emulate this technique based on the assumption that between two consecutive samples of an input signal, its derivative is nearly constant. In this way the new "samples" are obtained by linear interpolation between consecutive "measured" samples. This technique is shown in figure 5. On the top the "classical

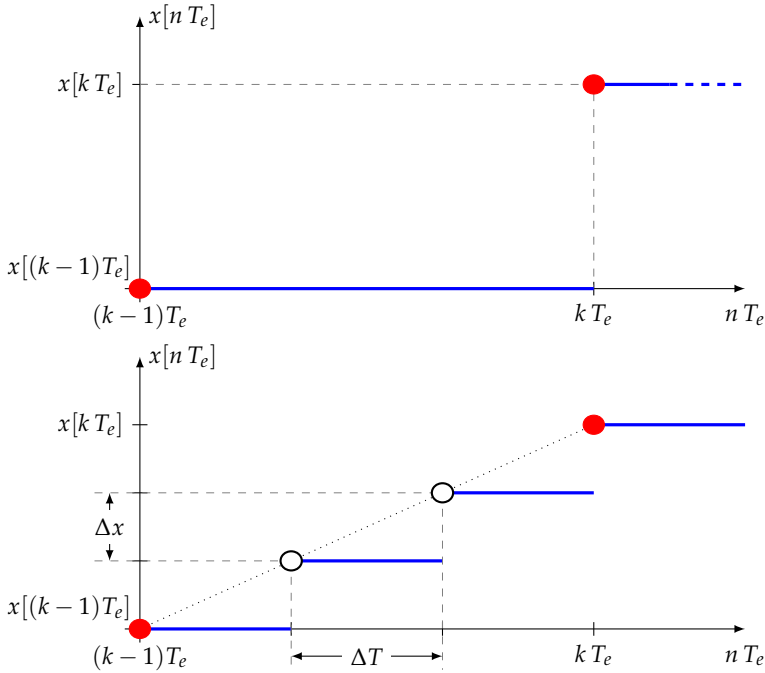


Fig. 5. Comparison between sampling and oversampling implementation.

sampling" is shown and on the bottom, the oversampling technique is depicted. As we can see, the sample period is reduced three times its original value, that is, $\frac{T_e}{N} = \frac{T_e}{3}$. This technique reduces the truncation error, inherent to Euler's method, three times. The benefits of this technique are exposed and validated by experimental tests.

5. Experimentations

5.1 Test bench

P_N	rated power	1.5KW
V_N	rated voltage	230V
I_N	rated current	3.2A
F_N	rated frequency	50Hz
N_N	rated speed	2998tr/min
p	number of pair of poles	1
R_S	stator resistance	4.2Ω
R_R	rotor resistance	2.8Ω
L_S	stator inductance	0.522 H
L_R	rotor inductance	0.537 H
M_{SR}	mutual inductance	0.502 H
f	viscous coefficient	1N.s/rad
α_1, λ_1	tunning parameters	$\alpha_1 = 1500, \lambda_1 = 2500$
α_2, λ_2	tunning parameters	$\alpha_2 = \alpha_1, \lambda_2 = \lambda_1$
α_3, λ_3	tunning parameters	$\alpha_3 = 1500, \lambda_3 = 2000$
α_4, λ_4	tunning parameters	$\alpha_4 = \alpha_3, \lambda_4 = \lambda_3$

Table 1. Induction machine and observer parameters.

Table (1) presents all electrical and mechanical parameters of Induction machine used in practice, and in Table (2) main VAR-CNTRL card features are presented.

The tunning parameters $\alpha_i, \lambda_i, i = 1, \dots, 4$ of the proposed observer are chosen according to inequalities (31), 32, 33 and 34 to satisfy convergence conditions.



Fig. 6. VAR-CNTRL card a product of GS Maintenance.

VAR-CNTRL is a electronic card designed by **GS Maintenance** and dedicated to motor control (Synchronous, Induction machine, Brushless, and DC motor). Equipped with a **DSP**

TMS320F2812 from **Texas Instrument**, this component is a fixed point; data are represented under 32 bits.

Practicals tests have been done under the following configurations:

- F_e , Sampling frequency of 8KHZ.
- F_{cyc} , **DSP** clock frequency of 150MHZ.
- 1024 points encoder, as speed sensor.
- **ADC's** (Analog-to-Digital Coder) of 12 bits provide bus voltage (V_{DC}), and phase currents (I_A, I_B) frames under 12 bits.

In addition to the **VAR-CNTRL**, a **MMI** (Man Machine Interface) permits to visualize **DSP** data registers in representation format 8.8 that means possible variations are from [-127.996 to 128].

To summarize our Bed Test description, we have :

- An **IM**.
- A two-level **VSI** (Voltage Source Inverter).
- A control card , **VAR-CNTRL**.
- A **MMI**.
- A speed sensor, a voltage sensor, and two current sensors.

5.2 Results

In this section we propose some experimentation results, that allow the following points:

- Validate Super Twisting Algorithm convergence.
- Evaluate Oversampling method efficiency.
- Evaluate Motor variables estimation.

In section 4.1 we introduced Euler Explicit Sampling Method to discretize a continuous system. Some technical limits about sampling frequency F_e lead us to introduce Oversampling strategy (c.f. section 4.2) . At first glance we propose to validate Super Twisting Observer strategy (c.f. system 7), we will take account of subsystem Σ_1 in figure 4 with the following entries : (v_1, z_1), and outputs : (\hat{z}_1, \hat{z}_3).

1	Analog Input/Output connectors. (3 Inputs /3 Outputs)
2	Communication port. (1 RS232)
3	Logical Output connector. (6 Outputs)
4	QEP connector. (A-B-Z)
5	Logical Input connector. (8 Isolated Inputs)
6	Supply voltage connector. (3.3V- 5V - ($\pm 15V$) - 24V)
7	Measurements connector. (V_{DC}, I_A, I_B)
8	DSP TMS320F2812
9	PWM connector. (6 Output signals).

Table 2. VAR-CNTRL card main elements.

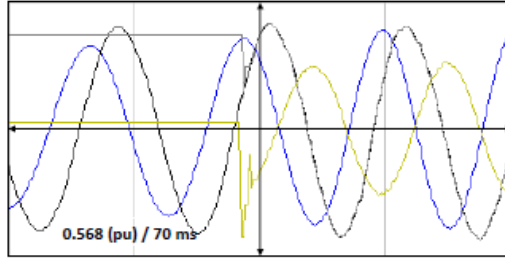


Fig. 7. MMI capture : (z_1, v_1) and (\hat{z}_1, \hat{z}_3) on convergence phase.

On figure 7 we validate the convergence of Σ_1 in figure 4, we can see that under some initials values \hat{z}_1 converge to z_1 in a finite time.

Figures 8 and 9 permit to assume that oversampling method is efficient, in fact we see that signals estimated by the observer (53) of the subsystem Σ_1 in figure 4 are much more better with an oversampling than without.

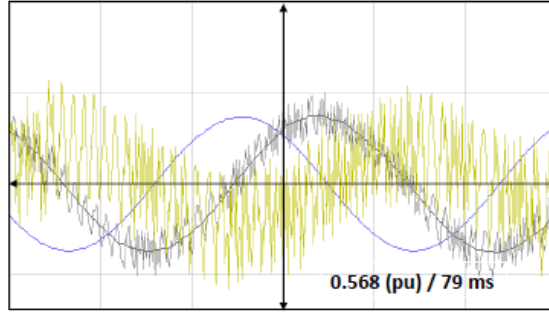


Fig. 8. MMI capture : (z_1, v_1) and (\hat{z}_1, \hat{z}_3) without oversampling method.

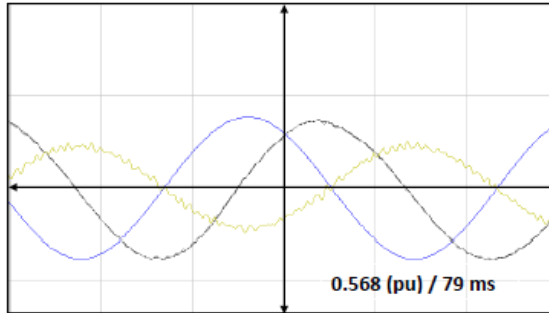


Fig. 9. MMI capture : (z_1, v_1) and (\hat{z}_1, \hat{z}_3) with oversampling method. ($N = 10$.)

Thus at the same operating point, we assume that with oversampling method we improve efficiency of the algorithm. With this validated data we can now abort estimation of *IM* magnetic (x_3, x_4) and mechanical (x_5) variables including the rotor position flux ρ given in equations 51, (35-36) and (52) respectively.

The main objective of this work is to provide a motor speed estimation without any mechanical sensor, and then drive it. Note that the speed sensor is only used in comparison of esti-

mated speed with its measure. To validate our strategy we propose some tests into different conditions.

Figures 12 and 13 permit to validate accuracy of estimated speed compare to measured speed in high variation range. However, it is admit that at low and very low speed, estimated speed damages more and more, as we can see on figures 14 and 15.

Now we propose some dynamical test results. During acceleration and deceleration phases (c.f. 16) , estimated speed is steel working although there is small delay between x_5 and \hat{x}_5 .

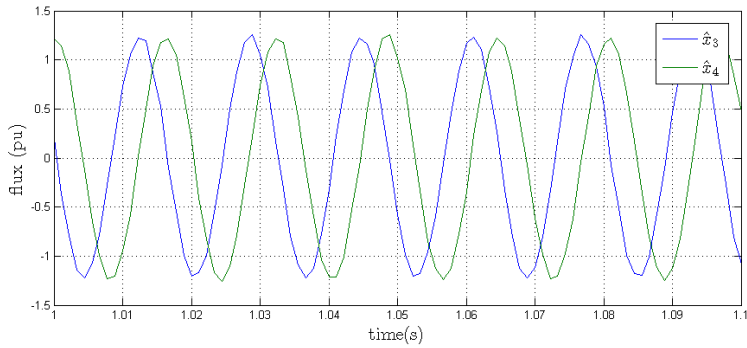


Fig. 10. Flux Estimation: x_3 and x_4 during static phase.

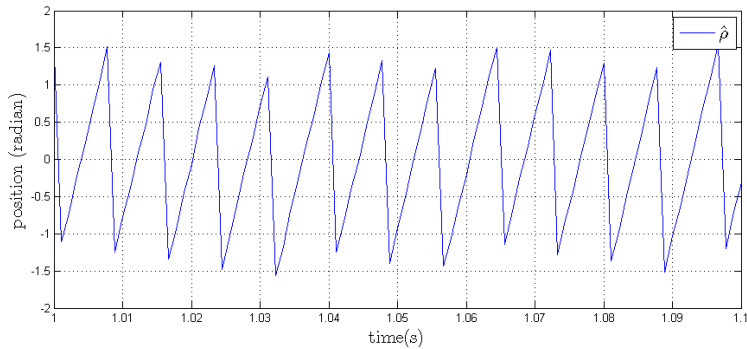


Fig. 11. Estimated of rotor flux position: ρ .

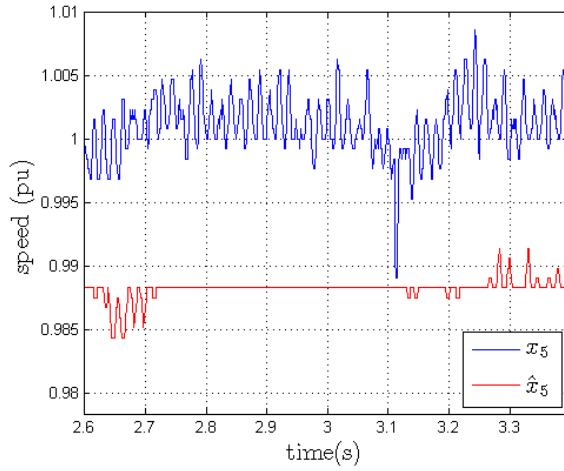


Fig. 12. Measure and estimate of speed during static phase: x_5 and \hat{x}_5

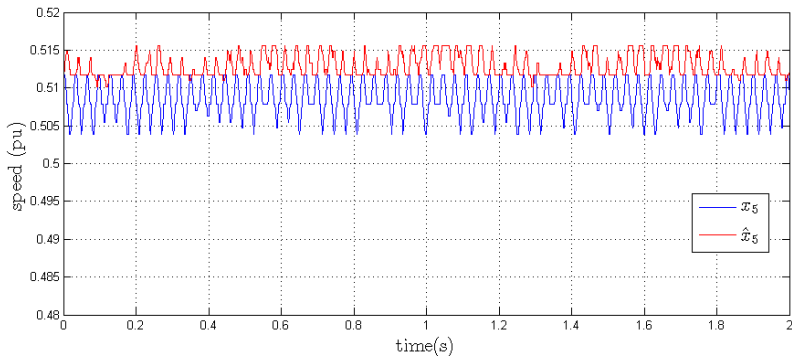


Fig. 13. Measure and estimate of speed during static phase: x_5 and \hat{x}_5

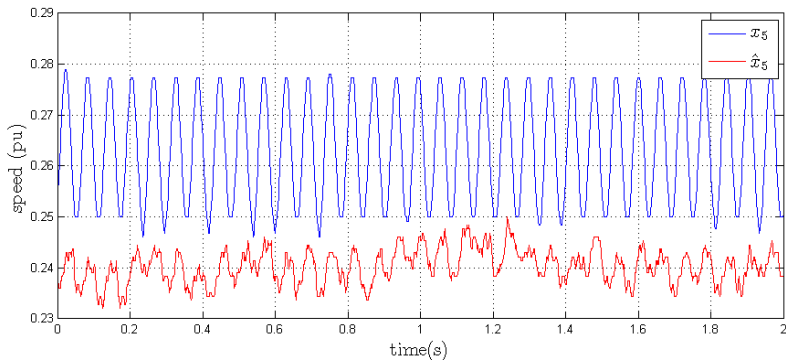


Fig. 14. Measure and estimate of speed during static phase: x_5 and \hat{x}_5

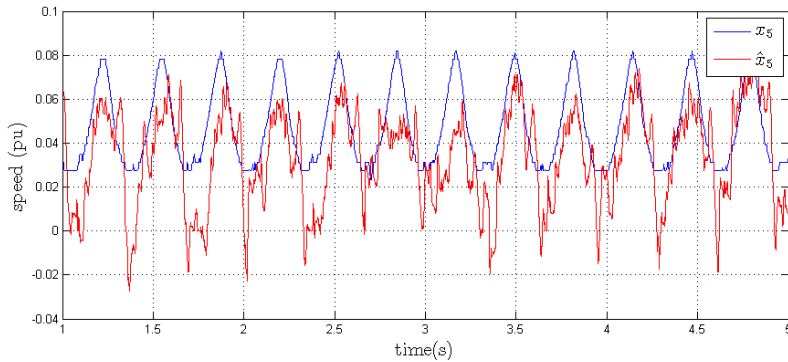


Fig. 15. Measure and estimate of speed during static phase: x_5 and \hat{x}_5

During static phase operation we saw that at low and very low speed, speed observation does not work very well. However on figures (17) and (18) we cross 0 speed, we denote a small divergence as small as the time to cross it; in fact this phenomenon underlines that speed is non observable with low current dynamic.

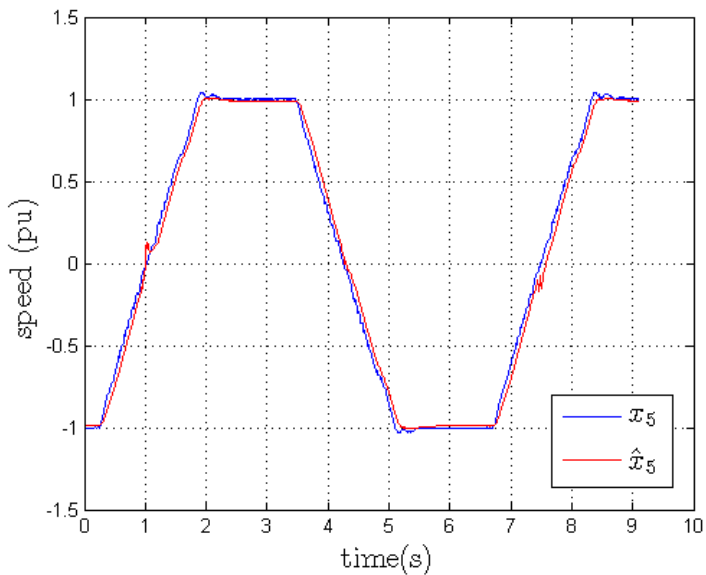


Fig. 16. Measure and estimate of speed during variable phase: x_5 and \hat{x}_5

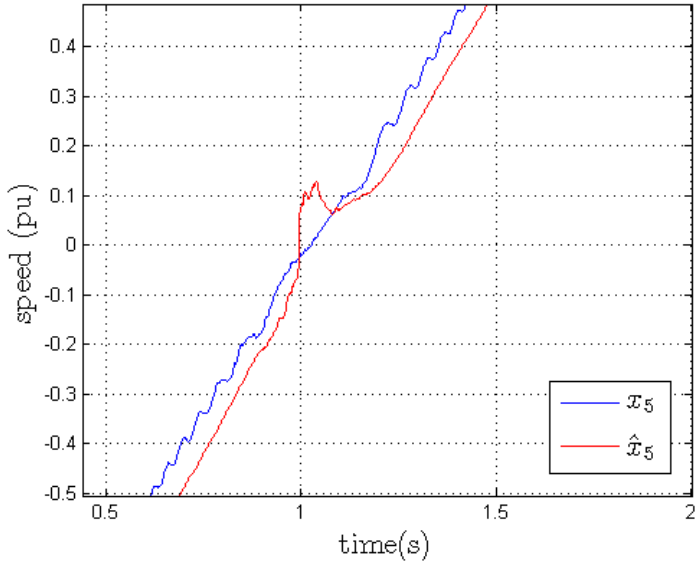


Fig. 17. Measure and estimate of speed during acceleration phase: x_5 and \hat{x}_5

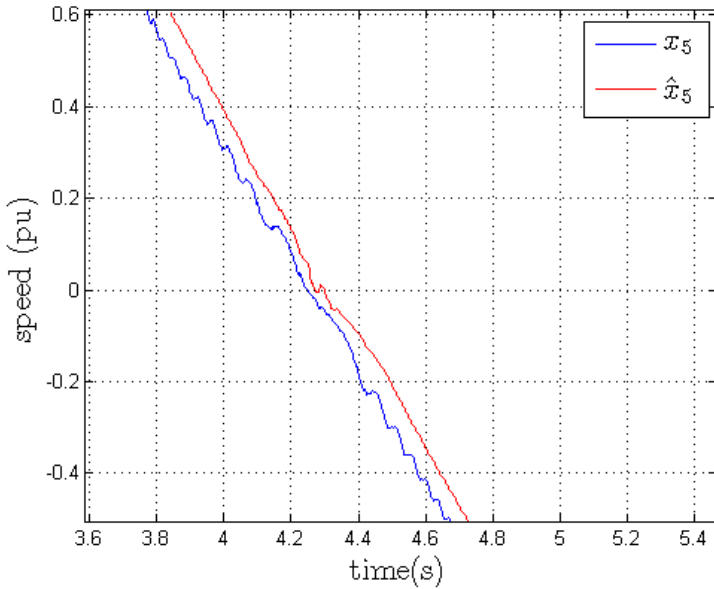


Fig. 18. Measure and estimate of speed during deceleration phase: x_5 and \hat{x}_5
 Figures 12 and 13 at high speed, show that speed approximation proposed in equation (51) work and permit to obtain magnitude and speed sign. This efficiency is also proved during dynamical phases as we can see on figure 16.

About this bad results, we have 2 arguments:

- Parameters error, mainly on stator and rotor resistance (R_S, R_R).
- Poor current dynamic, combined to digitizing error at low frequency working.

To overcome all this features, we propose to use an on-line resistor measurement of stator threw temperature.

6. Conclusion

Through this chapter an original method of observation without mechanical sensors for induction machine was introduced.

Designed for a embedded system (VAR-CNTRL) equipped with a fixed point DSP, we carried out various tests of validation.

We used concept of Sliding Mode through Super Twisting Algorithm, and oversampling method being based on the explicit Euler development. The contribution of this paper is mainly based on the applicability of the proposed observer for sensorless induction motor when a basic microprocessors are used in an industrial context.

At the time of the setting works of our strategy some technical constraints brought us to introduce a news strategy.

Thus the practical results permit us to do a first assessment:

- we validate our oversampling method introduced to overcome low speed data acquisition.
- we validate speed estimation during static and dynamic steps.
- we obtained an image of rotor flux(x_3 , and x_4), and also rotor position.

Compared with mechanical sensor the precision provides by the observer on the size speed offer a precision inferior or equal to 5% in the operating speed range from: 25% to 100%.

In term of prospects, it possible to improve the threshold of operation in low mode (25% to 5%) by adaptation oversampling number to stator frequency value, indeed a larger sample number could improve approximation of the continuous system .

In next step some tests will done to validate:

- Validation of hardness to load variation.
- Validation in closed loop.

About Observability loose at very low speed a first solution could be to switch with a speed estimator.

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